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**INVERSE MODELLING FOR SOURCE CHARACTERIZATION IN COMPLEX INDUSTRIAL  
SITES: DEVELOPMENT OF THE ADJOINT STATE METHOD APPLIED TO A  
LAGRANGIAN STOCHASTIC DISPERSION MODEL**

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**Abstract:** In this paper, a new application of the adjoint state method, to a Lagrangian stochastic (LS) model, in the context of atmospheric dispersion of pollutants, is presented. This method allows to solve the minimization problem with an efficient computation of the objective function gradient, reducing computation cost. The technique is applied to a LS model as it accurately models turbulent dispersion in a complex environment while still providing reasonable computational cost. In a first part, the adjoint method is presented, highlighting its benefits. Then the method is extended to a LS model, described as a Markovian explicit iterative model with least-square misfit. Finally, test cases are discussed.

**Key words:** *Inverse problem, Adjoint method, Pollutant source characterization, Lagrangian models*

## INTRODUCTION

The characterization of atmospheric pollutant sources in industrial sites is a major concern to improve on-site safety and to evaluate environmental impact. However, some of these sources are leaks and diffuse emissions difficult to identify and quantify, especially in real-time. Inverse modelling is a widespread method used to cope with this issue. It relies on sensor measurements downstream of the plume coupled with an inversion algorithm, allowing to retrieve source term characteristics, i.e., emission rate and position. In the literature, one can find different approaches to obtain these characteristics, as grid search “brute force” methods (Ben Salem *et al.*, 2014), consisting in testing a possible source position at every grid point and picking the one that best fits the data. Alternatively, one can solve a minimization problem with optimization methods classically computing the whole Jacobian matrix of the functional (Gill *et al.*, 1981).

Yet, all these techniques are time-consuming, reducing their applicability when time to solution prevails. To address this issue, the adjoint method was developed for the inverse problem theory (Chavent, 1974) to efficiently compute the cost function gradient, allowing for fast local optimization techniques (Keats *et al.*, 2007). Indeed, it avoids computing the whole Jacobian besides being independent of the optimization parameter number. Since then, it has been widely used, including in the atmospheric dispersion field, to find source term characteristics. A literature review highlights applications to Gaussian and Eulerian models (Pudykiewicz, 1998; Giering, 2000) but, to our knowledge, not on a forward LS model, despite being suitable for modelling turbulent dispersion in complex environment while providing reasonable computational cost. Consequently, this study aims at presenting a new application of this method, to a LS model for atmospheric dispersion of pollutants, and its use on some dataset configurations.

In the first section, the adjoint method is introduced, focusing on its benefits compared to other approaches. In the second part, it is extended to a LS model described as a Markovian explicit iterative model with least-square misfit. At last, some numerical verification results obtained by this application are discussed.

## ADJOINT STATE METHOD FOR INVERSE PROBLEM SOLVING

### Forward model definition

A forward model  $F_s$ , depending on model parameters  $m_s$  and giving the state (output) variable  $u_s$ , defines the generally implicit state equation (Plessix, 2006):

$$\underbrace{F_s}_{n_F \times 1} \left( \underbrace{u_s}_{n_u \times 1}, \underbrace{m_s}_{n_m \times 1} \right) = \underbrace{0}_{n_F \times 1} \quad (1)$$

$F_s$ ,  $u_s$  and  $m_s$  are respectively of size  $n_F$ ,  $n_u$  and  $n_m$  with  $n_F = n_u$  there being as many outputs as equations. If an explicit relationship  $f_s$  exists between  $u_s$  and  $m_s$ ,  $F_s$  will stand as  $F_s(u_s, m_s) = u_s - f_s(m_s) = 0$ . In the atmospheric dispersion context,  $F_s$  is a forward transport and dispersion model of pollutants originating from a source  $s$ , with  $u_s$  a concentration vector (e.g. pollutant species concentrations) provided as the forward model output and  $m_s$  a source parameter vector, i.e. source position and strength ( $n_m = 4$ ).

### Methodology for inverse problem solving

Generally, as an explicit analytical inversion of equation (1) does not exist, the inverse problem must be considered as a minimization one. The goal is to minimize the difference between the observation data  $d$ , i.e. the concentration observations in this context, and the output data  $u_s$  provided by the forward model (modelled concentrations). It amounts to minimize a cost function  $J$ , depending on model parameters  $m_s$ :

$$\underbrace{J}_{1 \times 1} \left( \underbrace{m_s}_{n_m \times 1} \right) = \underbrace{E}_{1 \times 1} \left( \underbrace{u_s}_{n_u \times 1}, \underbrace{m_s}_{n_m \times 1} \right) \quad (2)$$

with  $E$  the error functional of the differences between the model data  $u_s$  and the observations  $d$ . To find the values of  $m_s$  minimizing the cost function  $J$ , its gradient must be computed. The minimization problem is then solved iteratively in practise, updating the  $m_s$  values at each iteration of the optimization algorithm.

### Introduction of the adjoint state equation to compute the gradient

Classically, the computation of  $\nabla J$  requires the whole Jacobian matrix, i.e. the matrix of the derivatives relatively to model parameters  $m_s$ . Providing the full expression of the gradient:

$$\underbrace{\nabla J}_{n_m \times 1} := \left( \frac{dJ}{dm_s} \right)^T = \left( \frac{\partial E}{\partial u_s} \frac{du_s}{dm_s} + \frac{\partial E}{\partial m_s} \right)^T = \underbrace{\left( \frac{du_s}{dm_s} \right)^T}_{n_m \times n_u} \underbrace{\left( \frac{\partial E}{\partial u_s} \right)^T}_{n_u \times 1} + \underbrace{\left( \frac{\partial E}{\partial m_s} \right)^T}_{n_m \times 1} \quad (3)$$

the matrix  $\frac{du_s}{dm_s}$  appears as the bottleneck term as  $u_s$  does not normally depend explicitly on  $m_s$ , preventing the differentiation of  $u_s$ . Moreover, this term, which needs to be computed for each perturbation  $dm_s$ , i.e. typically on each grid point, depends on the number of parameters. At the industrial scale, the number of grid points can exceed many thousands, leading to large computation cost. The adjoint method proposes an alternate, quicker way to compute  $\nabla J$ . It formally derives adjoint equations from transport models (Pudykiewicz, 1998), providing the sensitivity of model output (e.g. concentration) to input variables (e.g. emission rate and location). From the state equation (1) specifying the state variable  $u_s$ , the adjoint state equation is obtained such that:

$$\underbrace{\left( \frac{\partial F_s}{\partial u_s} \right)^T}_{n_u \times n_F} \underbrace{\lambda_s}_{n_F \times 1} = \underbrace{\left( \frac{\partial E}{\partial u_s} \right)^T}_{n_u \times 1} \quad (4)$$

specifying the adjoint state  $\lambda_s$ , of dimensions  $n_F \times 1$ . Equation (4) is nothing more than a linear system to solve, where  $\lambda_s$  is not a matrix but a vector this time. The adjoint state does not depend on the number of optimization parameters anymore, reducing computation time.

### Gradient computing

Once equation (4) is solved, i.e.  $\lambda_s$  found, the gradient  $\nabla J$  determined by each component can be computed:

$$\underbrace{\nabla J}_{n_m \times 1} := \underbrace{\left(\frac{dJ}{dm_s}\right)^T}_{n_m \times 1} = \underbrace{\left(\frac{\partial E}{\partial m_s}\right)^T}_{n_m \times 1} - \underbrace{\left(\frac{\partial F_s}{\partial m_s}\right)^T}_{n_m \times n_F} \lambda_s \quad (5)$$

### Extension to a Markovian explicit iterative model with least-square misfit

To apply the adjoint to a LS model, the method has been extended to an explicit iterative model case, with a Markov process and a least-square error functional. In this case,  $\frac{\partial F_s}{\partial u_s}$  becomes the identity matrix in (4) and  $\lambda_s$  now equals the source term  $\left(\frac{\partial E}{\partial u_s}\right)^T$ , such that:

$$\lambda_s = \underbrace{\left(\frac{\partial E}{\partial u_s}\right)^T}_{n_F \times 1} = \underbrace{\left(\frac{u_s - d}{d * d}\right)^T}_{n_u \times 1} \quad (6)$$

Moreover,  $E$  does not depend explicitly on  $m_s$ ,  $\frac{\partial E}{\partial m_s} = 0$  in equation (5). Finally, combining equation (5), the derivative of the forward explicit model (1) and equation (6),  $\nabla J$  can be computed such that:

$$\underbrace{\nabla J}_{n_m \times 1} = - \underbrace{\left(\frac{\partial F_s}{\partial m_s}\right)^T}_{n_m \times n_F} \lambda_s = \underbrace{\left(\frac{\partial f_s}{\partial m_s}\right)^T}_{n_m \times n_F} \underbrace{\left(\frac{u_s - d}{d * d}\right)^T}_{n_F \times 1} \quad (7)$$

Considering an iterative model of  $N$  total iterations, the outputs are now computed by successive applications of a sub-model of  $f_s$ . Moreover, in the atmospheric dispersion context, the model includes a Markov process. Hence, only the first sub-model  $f_s^1$  depends on  $m_s$ . Besides, the global output vector  $u_s$  is now the concatenation of the  $N$  sub-vectors  $u_s^i$ . Finally, the global forward model vector  $F_s$  is defined as:

$$\underbrace{F_s}_{n_u \times 1} \left( \underbrace{u_s}_{n_u \times 1}, \underbrace{m_s}_{n_m \times 1} \right) = \left[ \underbrace{[u_s^1 - f_s^1(m_s)]^T}_{1 \times n_1} \dots \underbrace{[u_s^i - f_s^i(u_s^{i-1})]^T}_{1 \times n_i} \dots \underbrace{[u_s^N - f_s^N(u_s^{N-1})]^T}_{1 \times n_N} \right]^T = \mathbf{0}_{n_u \times 1} \quad (8)$$

where  $u_s^i$  is the sub-vector of  $u_s$  of dimension  $n_i$ ,  $f_s^i$  is the corresponding explicit sub-model of  $f_s$  at the  $i^{th}$  iteration and  $n_u = \sum_{i=1}^N n_i = n_F$ . In (8), only the first member  $[u_s^1 - f_s^1(m_s)]^T$  depends on  $m_s$ . Hence, the Jacobian matrix  $\left(\frac{\partial F_s}{\partial m_s}\right)^T$  is null everywhere except at its terms involving  $f_s^1$ . Besides, under the assumption of only final iteration observations, one can solve iteratively the adjoint state equation (4), which is now:

$$\begin{bmatrix} 1 & -\left(\frac{\partial f_s^2}{\partial u_s^1}\right)^T & 0 & \dots & 0 \\ 0 & \ddots & -\left(\frac{\partial f_s^3}{\partial u_s^2}\right)^T & \ddots & \vdots \\ \vdots & \ddots & \ddots & \ddots & 0 \\ \vdots & & \ddots & \ddots & -\left(\frac{\partial f_s^N}{\partial u_s^{N-1}}\right)^T \\ 0 & \dots & \dots & 0 & 1 \end{bmatrix}_{n_u \times n_u} \begin{bmatrix} \lambda_s^1 \\ \lambda_s^2 \\ \vdots \\ \lambda_s^{N-1} \\ \lambda_s^N \end{bmatrix}_{n_u \times 1} = \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ \left(\frac{\partial E}{\partial u_s^N}\right)^T \end{bmatrix}_{n_u \times 1} \quad (9)$$

$$\text{with } \lambda_s^i = \underbrace{\prod_{j=i}^{N-1} \left(\frac{\partial f_s^{j+1}}{\partial u_s^j}\right)^T}_{n_i \times n_N} \underbrace{\left[\left(\frac{\partial E}{\partial u_s^N}\right)^T\right]}_{n_N \times 1} \stackrel{\text{by (6)}}{\cong} \underbrace{\prod_{j=i}^{N-1} \left(\frac{\partial f_s^{j+1}}{\partial u_s^j}\right)^T}_{n_i \times n_N} \underbrace{\left[\frac{u_s^N - d^N}{d^N * d^N}\right]}_{n_N \times 1} \quad (10)$$

Finally, one can compute  $\nabla J$ , using  $\lambda_s^1$  found solving iteratively equation (9) with equation (10), the sparse Jacobian matrix  $\left(\frac{\partial F_s}{\partial m_s}\right)^T$  with Markov process and the expression of  $\nabla J$  in equation (7):

$$\underbrace{\nabla J}_{n_m \times 1} = \underbrace{\left(\frac{\partial f_s^1}{\partial m_s}\right)^T}_{n_m \times n_1} \underbrace{\prod_{j=1}^{N-1} \left(\frac{\partial f_s^{j+1}}{\partial u_s^j}\right)^T}_{n_1 \times n_N} \underbrace{\left[\frac{u_s^N - d^N}{d^N * d^N}\right]}_{n_N \times 1} \quad (11)$$

Equation (11) is a clever way to compute the gradient, by the chain rule application.  $\nabla J$  is obtained computing only a product iteratively, by simply calculating the partial derivatives of  $f_s^i$  iteratively. Neither the a priori knowledge of the final output  $u_s^N$  nor the final observations  $d^N$  are necessary, being only required as global product terms. Knowing a priori the number of iterations  $N$  is not necessary either.

### APPLICATION TO A LAGRANGIAN STOCHASTIC PARTICLE DISPERSION MODEL

To present the methodology, it is applied to a simplified LS model, with Gaussian steady isotropic homogeneous turbulence and diagonal Reynolds stresses. A  $p$  particle originating from an instantaneous

point source position  $\mathbf{x}_s$  is transported at each time step  $\delta t$  through a stochastic advection process. Its path is described at each time  $t$  by its Lagrangian position  $X_{p,i}$  and Lagrangian fluctuating velocity  $U'_{p,i}$ :

$$\begin{cases} X_{p,i}(t + \delta t) = X_{p,i}(t) + \left( \bar{u}_i(\mathbf{X}_p, t) + U'_{p,i}(t) \right) \delta t \\ U'_{p,i}(t + \delta t) = \left( 1 - \frac{\delta t}{T_L} \right) U'_{p,i}(t) + \sigma_u \sqrt{\frac{2}{T_L}} \delta \xi_{p,u_i} \end{cases} \text{ with } U'_{p,i}(t_0) = \xi_{p,u_i}(t_0) \sigma_u \text{ and } X_{p,i}(t_0) = x_{s,i} \quad (12)$$

with  $i$  the spatial component at time  $t$ . The evolution of  $U'_{p,i}$  is given by the Langevin stochastic equation (Thomson, 1987).  $\bar{u}_i$  is the mean velocity, while  $\sigma_u$  is the standard deviation of velocity fluctuations and  $T_L$  the Lagrangian time.  $\delta \xi_{p,u_i}$  is a random variable with Gaussian p.d.f of 0 mean value and  $\delta t$  variance.

Moreover,  $p$  owns a pseudo-mass  $M_p$  such that, under the assumption of the absence of decay process:

$$\forall t, M_p(t + \delta t) = M_p(t) \text{ with } M_p(t_0) = \frac{M_s}{N_p} \quad (13)$$

with  $M_s$  and  $N_p$  respectively the mass of pollutant and the number of particles released from the source  $s$ . Finally, the average concentration  $\bar{C}_s(\mathbf{x}_r, t_N)$  at a sensor position  $\mathbf{x}_r$  for final time  $t_N$  is computed using a density kernel approach, i.e. as the sum of contributions from all particles in the computational domain:

$$\bar{C}_s(\mathbf{x}_r, t_N) = \sum_{p=1}^{N_p} M_p(t_N) K(\mathbf{X}_p(t_N) - \mathbf{x}_r, h_r) \quad (14)$$

with  $K$  a kernel function, modelling the detector response function of a sensor  $r$ , acting as a spatial filter centred in  $\mathbf{x}_r$  and  $h_r$  the smoothing radius of the chosen kernel function.

The adjoint method is applied to the forward LS Markovian explicit iterative model with least-square misfit described in the previous section. The matrices  $\frac{\partial f_s^1}{\partial m_s}$ ,  $\frac{\partial f_s^{j+1}}{\partial u_s^j}$  and  $\frac{\partial f_s^N}{\partial u_s^{N-1}}$  in equation (11) then become:

$$\left( \frac{\partial f_s^1}{\partial m_s} \right)^T = \begin{bmatrix} \underbrace{P_{1,s}^T}_{n_m \times 7} & \cdots & \underbrace{P_{p,s}^T}_{n_m \times 7} & \cdots & \underbrace{P_{N_p,s}^T}_{n_m \times 7} \end{bmatrix} \quad (15)$$

$$\left( \frac{\partial f_s^{j+1}}{\partial u_s^j} \right)^T = \text{diag} \left( \underbrace{Q_{1,s}^{j+1T}}_{7 \times 7}, \dots, \underbrace{Q_{p,s}^{j+1T}}_{7 \times 7}, \dots, \underbrace{Q_{N_p,s}^{j+1T}}_{7 \times 7} \right) \quad (16)$$

$$\left( \frac{\partial f_s^N}{\partial u_s^{N-1}} \right)^T = \begin{bmatrix} \underbrace{R_{1,s}}_{n_{N-1} \times n_N} & \cdots & \underbrace{R_{p,s}}_{n_{N-1} \times n_N} & \cdots & \underbrace{R_{N_p,s}}_{n_{N-1} \times n_N} \end{bmatrix}^T \quad (17)$$

For each particle  $p$ , the terms  $P_{p,s}$ ,  $Q_{p,s}^{j+1}$  and  $R_{p,s}$  correspond, for the LS model, to the sensitivity matrixes of, respectively, the seven characteristics of  $p$  ( $\mathbf{X}_p$ ,  $\mathbf{U}_p$  and  $M_p$ ) with respect to source parameters  $m_s$  at release time, the characteristics of  $p$  at the  $(j+1)^{th}$  iteration with respect to the  $j^{th}$  one (transport steps), and the concentration of particles at the sensor  $r$  with respect to the characteristics of  $p$  at iteration  $N$ . The gradient  $\nabla J$  in equation (11) is now, using equations (15), (16) and (17):

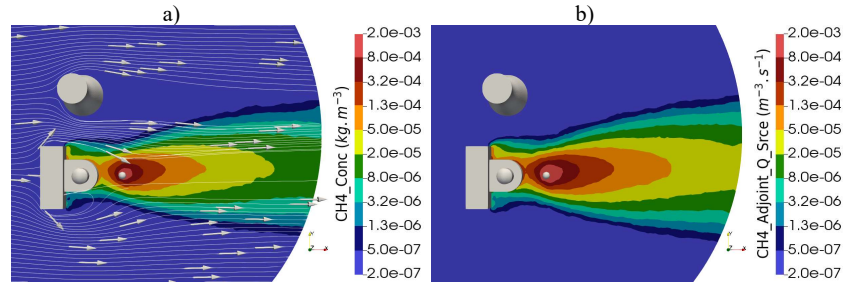
$$\nabla J = \left( \sum_{t=1}^N \sum_{p=1}^{N_p} O_{p,s} \right) \left[ \frac{u_s^N - d^N}{d^N \cdot d^N} \right] \text{ with } O_{p,s} = \underbrace{P_{p,s}^T}_{n_m \times n_N} \left[ \prod_{j=1}^{N-2} Q_{p,s}^{j+1T} \right] \underbrace{R_{p,s}^T}_{n_m \times n_N} \quad (18)$$

The term  $O_{p,s}$  in (18), of size  $4 * n_N$  here, can be computed independently for each particle, allowing parallelization hence reducing restitution time. As previously stated, the product is calculated iteratively while the forward model is running, which avoids particle data storage at each time step and excessive memory use. Lastly, this work deals with observations taken at final iteration only. Yet, in a more general case, if measurements occur at multiple times, or with an unsteady source moving and/or emitting at various instants,  $O_{p,s}$  can easily be adapted by summing equivalent terms corresponding to these cases.

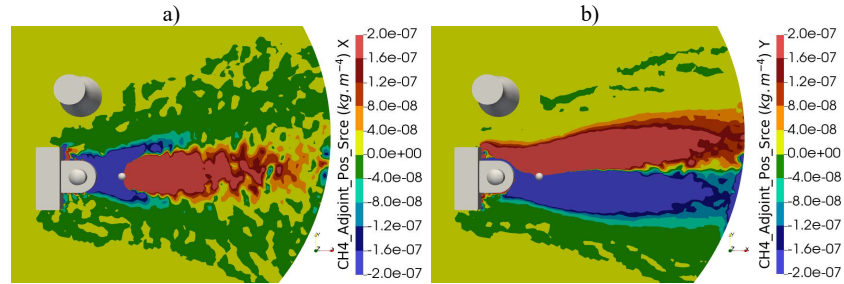
## APPLICATION RESULTS ON A NUMERICAL TEST CASE

A  $\text{CH}_4$  concentration field and its adjoint ones are computed, emitted by a continuous release from a point source located 10 meters above the ground, in a steady configuration with Gaussian isotropic homogeneous turbulence and diagonal Reynolds stresses, for a neutral atmosphere. The computational domain is a test case power plant at the centre of a 600-meter radius disk. The flow part is precomputed from a CFD database and the LS model runs the dispersion part ( $\delta t = 5s$ ) until it converges to a steady state. A smoothing stage

is applied to the concentration field. This direct field and its adjoint ones like the emission and the Y-position ones, shown respectively in Figures 1-a), 1-b) and 2, are used to compute sensitivities on the ground, using (18). These gradients represent the opposite directions of source displacement which reduce the concentration error between the model and the observations, i.e. the cost function, allowing to approach source true characteristics. Several results and sensitivity studies will be discussed to illustrate the application of the adjoint state method to the LS model.



**Figure 1.** In log. scale: a) Concentration field with wind streamlines; b) Adjoint emission field.



**Figure 2.** In linear scale: a) Adjoint X-position field; b) Adjoint Y-position field.

## CONCLUSION

In this work, a new application of the adjoint method has been presented for a LS model. Use of the adjoint to solve the minimization problem avoids the computation of the whole Jacobian matrix and dependence on the number of optimization parameters, saving significant computation time. In this study, the benefits of the approach have been highlighted and its use extended to a LS model, well suited to turbulent dispersion modelling in a complex environment. Hence, the combined use of the adjoint method with a LS model is well suited to source characterization with real time constraint in complex industrial sites.

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