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Large-eddy simulation of wind flows and pollutant transport inside and over idealized urban street canyons in unstable thermal stratification

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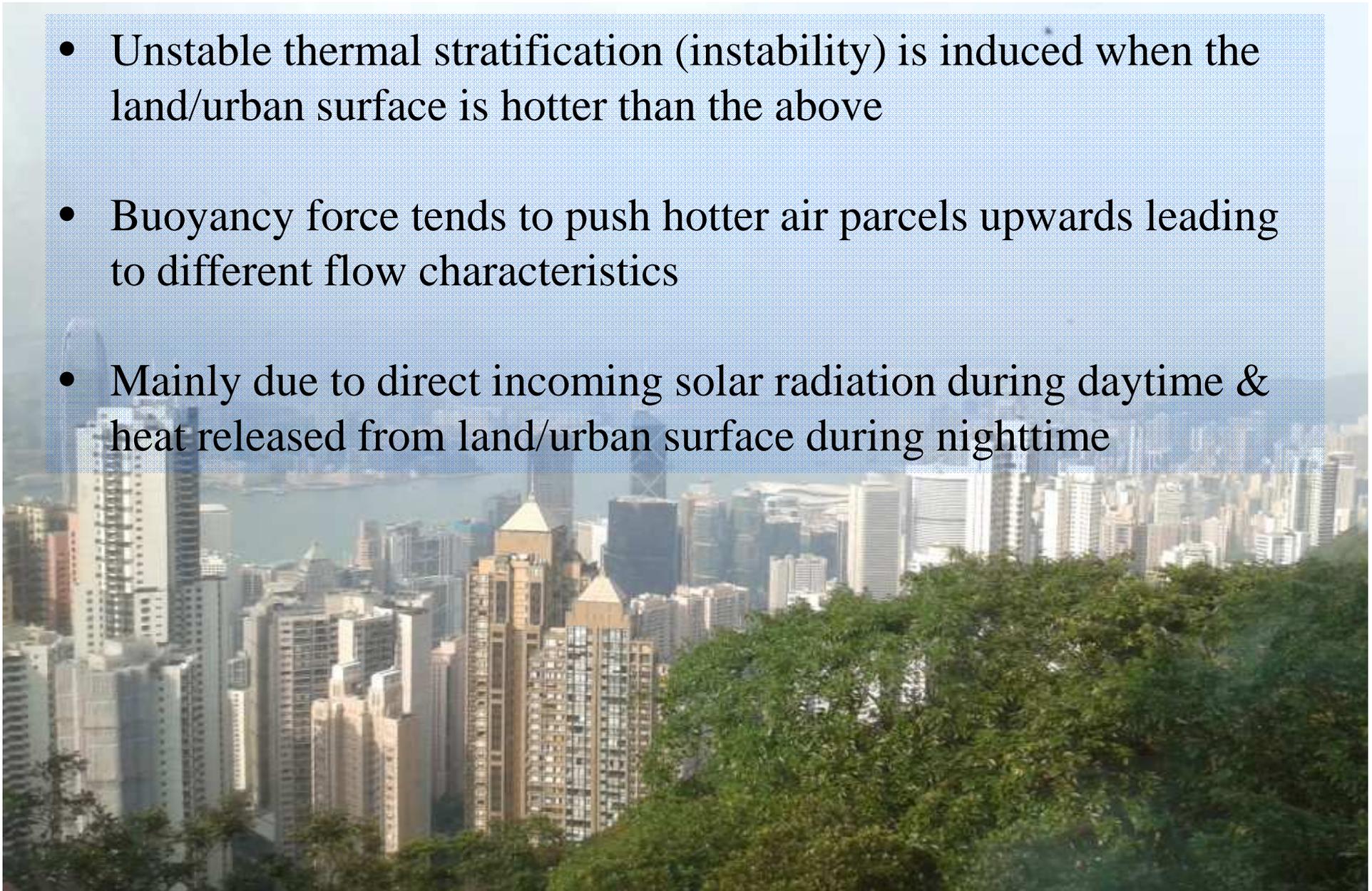
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Introduction

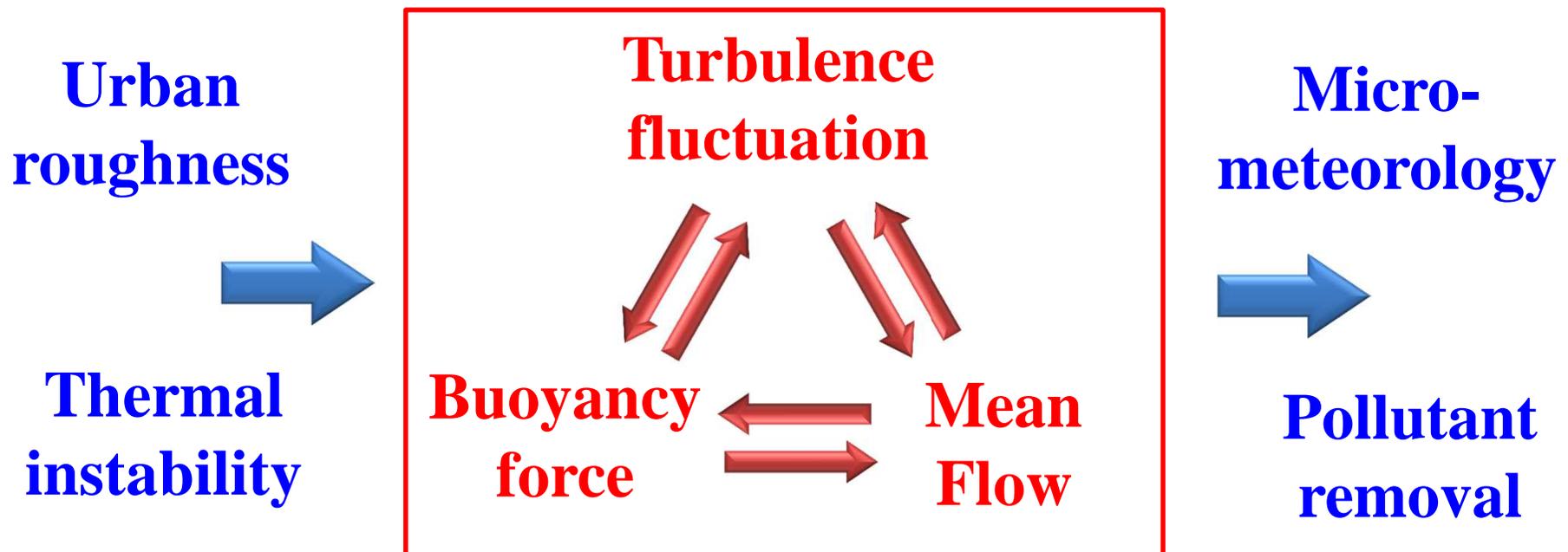
- Unstable thermal stratification (instability) is induced when the land/urban surface is hotter than the above
- Buoyancy force tends to push hotter air parcels upwards leading to different flow characteristics
- Mainly due to direct incoming solar radiation during daytime & heat released from land/urban surface during nighttime



Photography taken at Noon, - The Peak, Hong Kong

Motivations

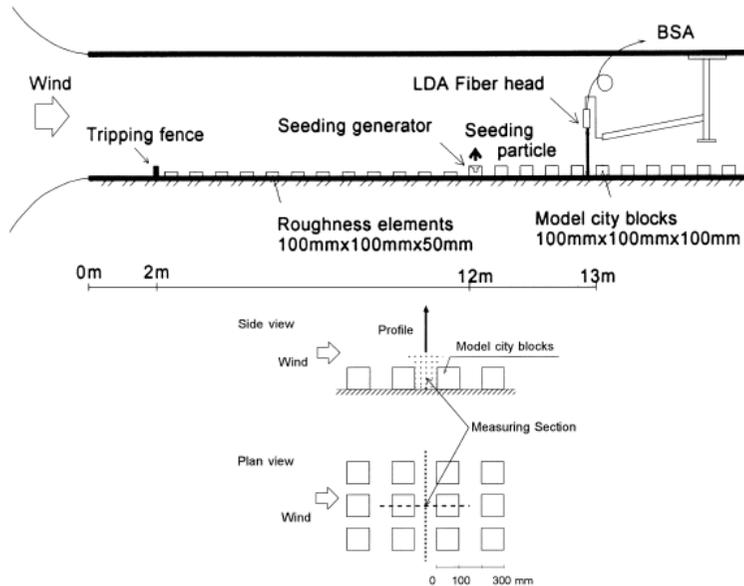
- Some previous studies showed that unstable stratification tends to promote pollutant dispersion & turbulent mixing, which in turn improves the street canyon air ventilation



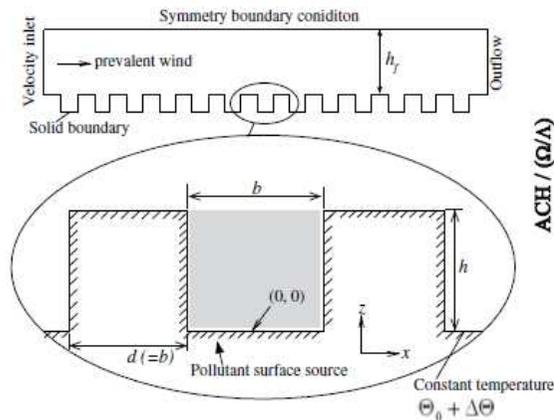
Motivations

- Urban morphology is characterized by large roughness height which enhances turbulent generation
- High heat capacity of urban surface & trapping of thermal energy inside street canyons increase the duration of unstable stratification, compared with that over rural terrain
 - e.g. observation showed 85% in daytime & 64% at nighttime (Niachou et al. 2008)
- It is advantageous to understand the characteristics of flows & pollutant dispersion under unstable stratification in urban areas
- However, those researches are limited in the literature

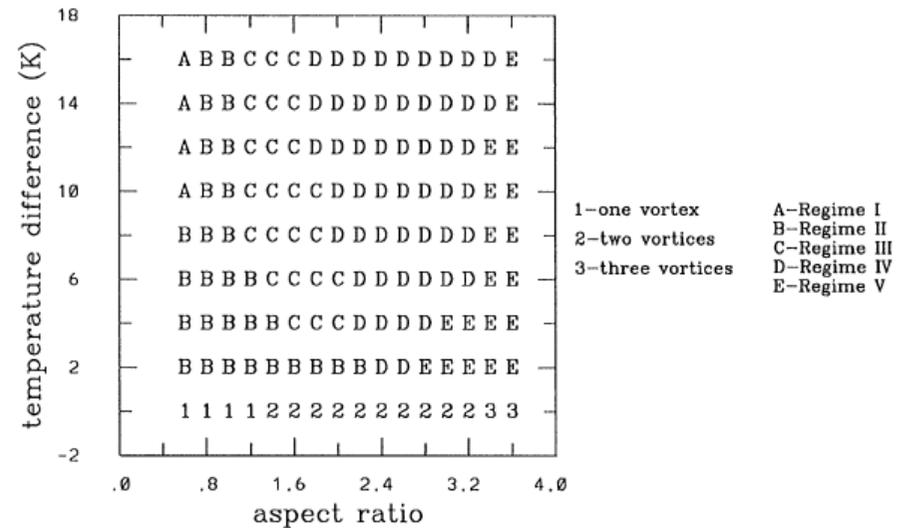
Highlights of previous studies



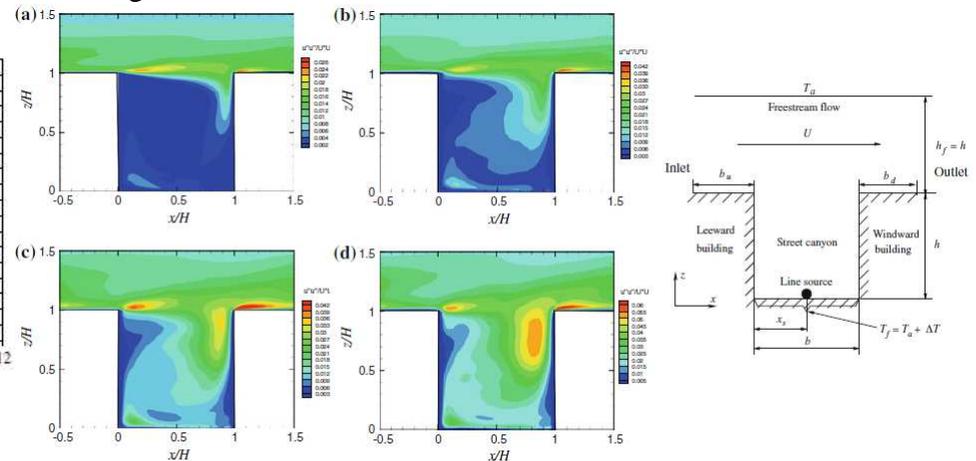
Uehara et al. (2000) – Wind tunnel experiments on how thermal stratification affects flows in and above urban street canyons



Cheng et al. (2009) – On the correlation of air and pollutant exchange for street canyons in combined wind-buoyancy-driven flow



Kim and Baik (2001) – Urban street-canyon flows with bottom heating



Li et al. (2010) – Large-eddy simulation of flow and pollutant transport in urban street canyons with ground heating

Objectives

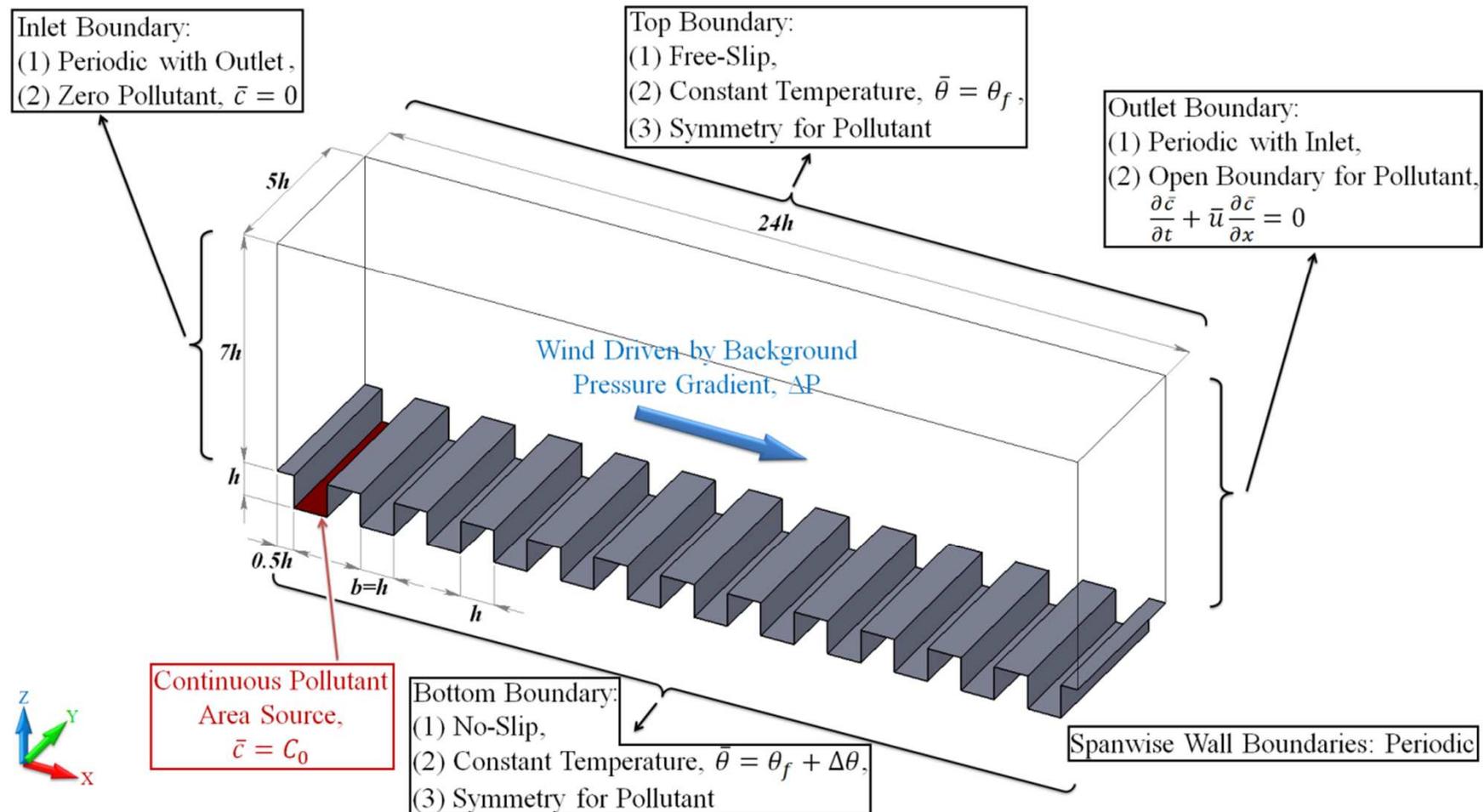
Since the micro-meteorology and pollutant removal of street canyons strongly depend on the flow conditions just above the urban roughness, this presentation mainly focuses on

- 1) the wind flows (mean wind & turbulent statistics),
- 2) the logarithmic mean wind profiles, and
- 3) the pollutant dispersion characteristics above urban surface under different intensities of (slightly) unstable stratification

This study is performed in a fundamental way by using idealized urban geometries & background conditions, & using LES to resolve all the large-scale turbulence explicitly

Methodology

- Large-eddy simulation (**LES**) with one-equation subgrid-scale (**SGS**) turbulence model (incompressible flow)
- By the open-source CFD code – **OpenFOAM**, version 2.1.0



Methodology

- Free-stream wind is driven by background pressure gradient ΔP (constant for all models)
- Buoyancy force is modeled by the Boussinesq approximation & is controlled by the gravitational acceleration g
- Solving the filtered governing equations for the resolved-scale flow vector, temperature & pollutant concentration

$$\frac{\partial \bar{u}_i}{\partial t} + \frac{\partial}{\partial x_j} \bar{u}_i \bar{u}_j = \boxed{\Delta P \delta_{i1}} - \frac{\partial \bar{p}}{\partial x_i} + (\nu + \nu_{SGS}) \frac{\partial^2 \bar{u}_i}{\partial x_j \partial x_j} + \boxed{\alpha g (\bar{\theta} - \theta_0) \delta_{i3}}$$

Background Pressure Gradient Buoyancy Force

Methodology

- Analyzing the pseudo steady-state properties
- Ensemble averaging in the temporal & spanwise domains that denoted by $\langle \phi \rangle$
- Simulation conditions:

AR	Re_τ	Re_H	Ri_τ	Ri_H
1	4140	89,000 ↓ 42,000	0 ↓ -400	0 ↓ -3.92

By force balance in free-stream domain,

$$\tau_w = \rho \cdot \Delta P \cdot H$$

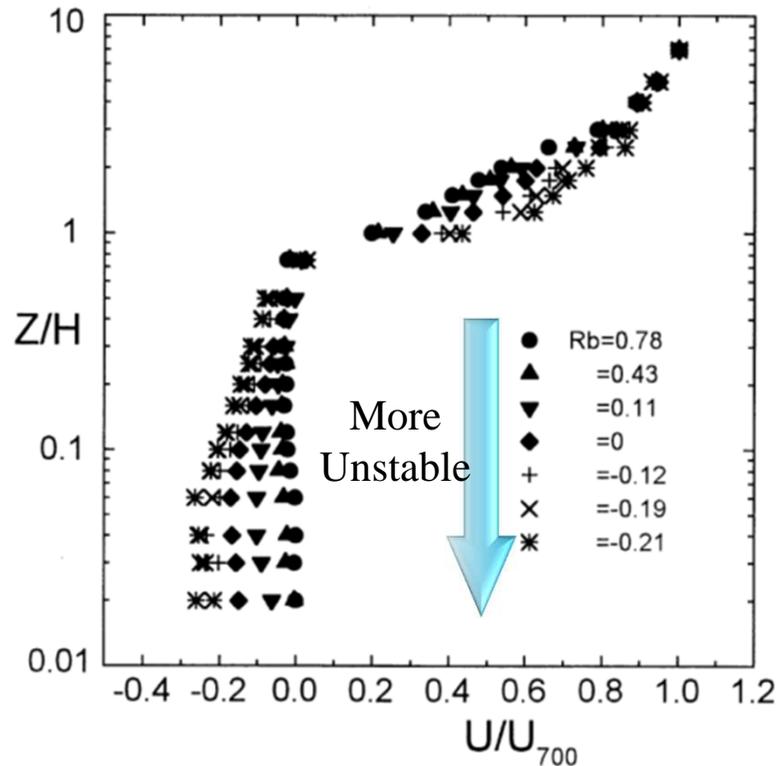
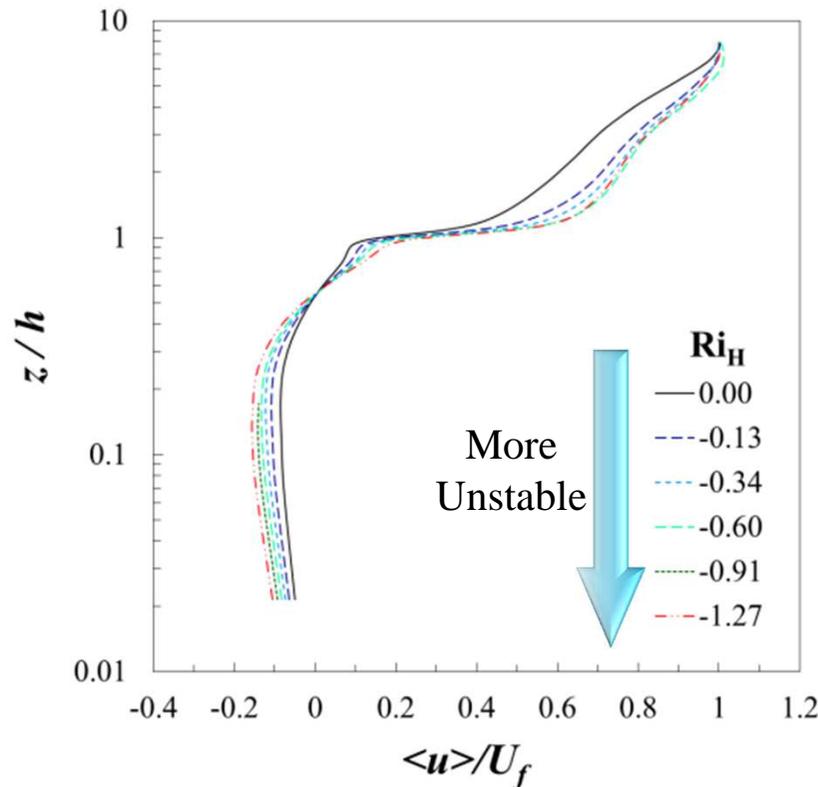
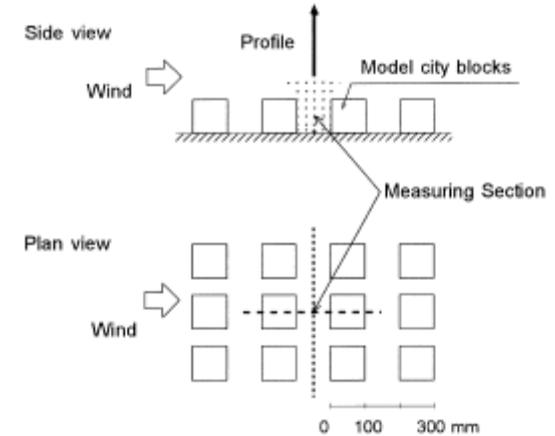
$$u_\tau = \sqrt{\tau_w / \rho} = \sqrt{\Delta P \cdot H}$$

$$Re_H = \frac{H \cdot U_f}{\nu} \quad Ri_H = -\frac{\alpha g H \Delta \theta}{U_f^2}$$

$$Re_\tau = \frac{H \cdot u_\tau}{\nu} \quad Ri_\tau = -\frac{\alpha g H \Delta \theta}{u_\tau^2}$$

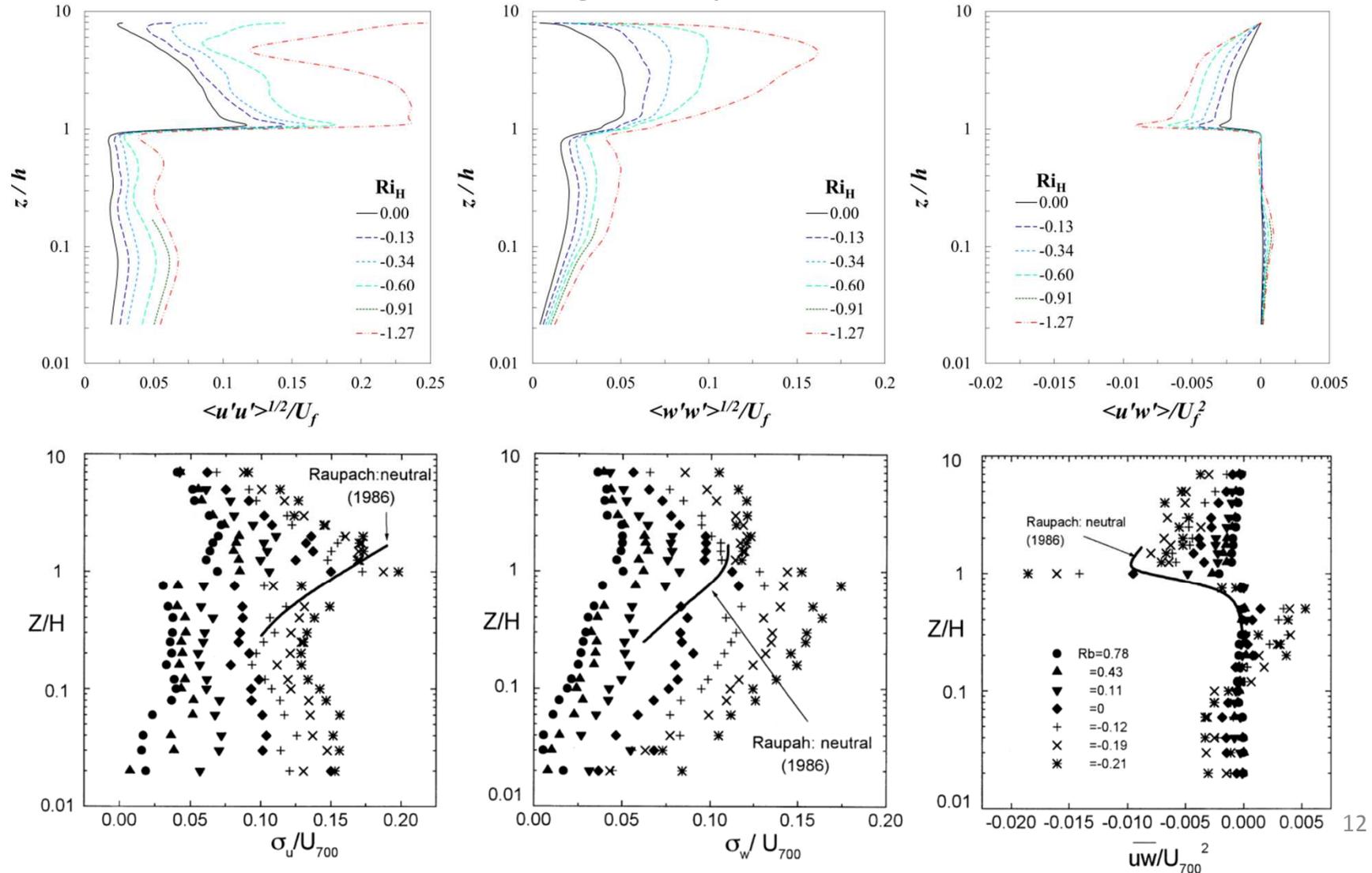
Comparison between LES & wind tunnel models

- LES results show trends which are similar to the tunnel results by Uehara et al. (2000):
 - Wind flow relative to free-stream is enhanced both inside and above street canyon



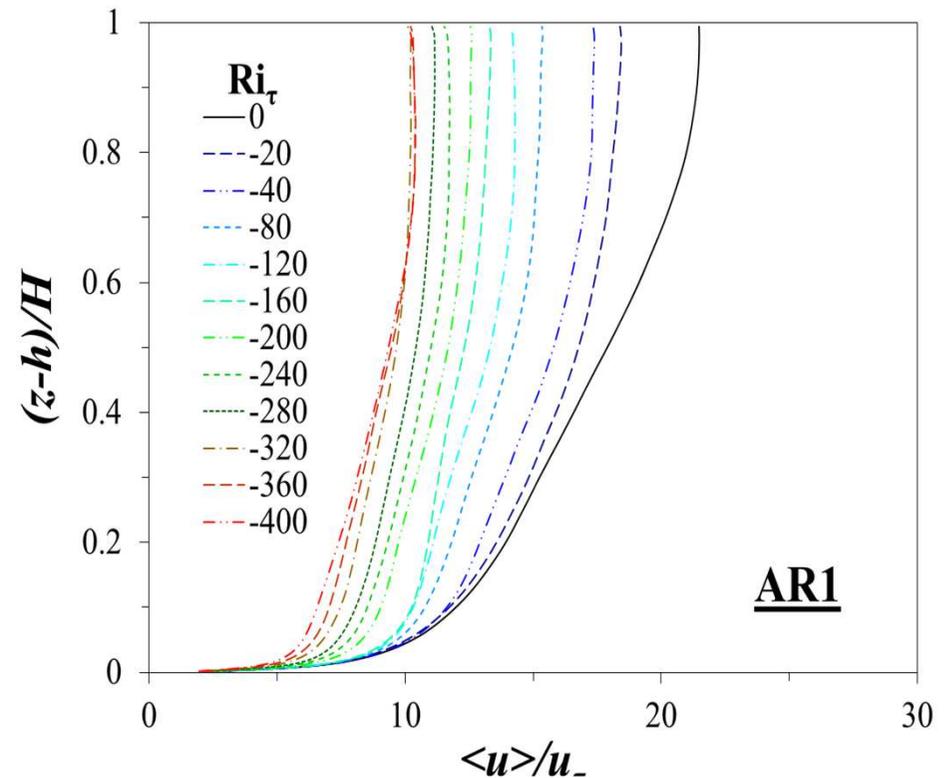
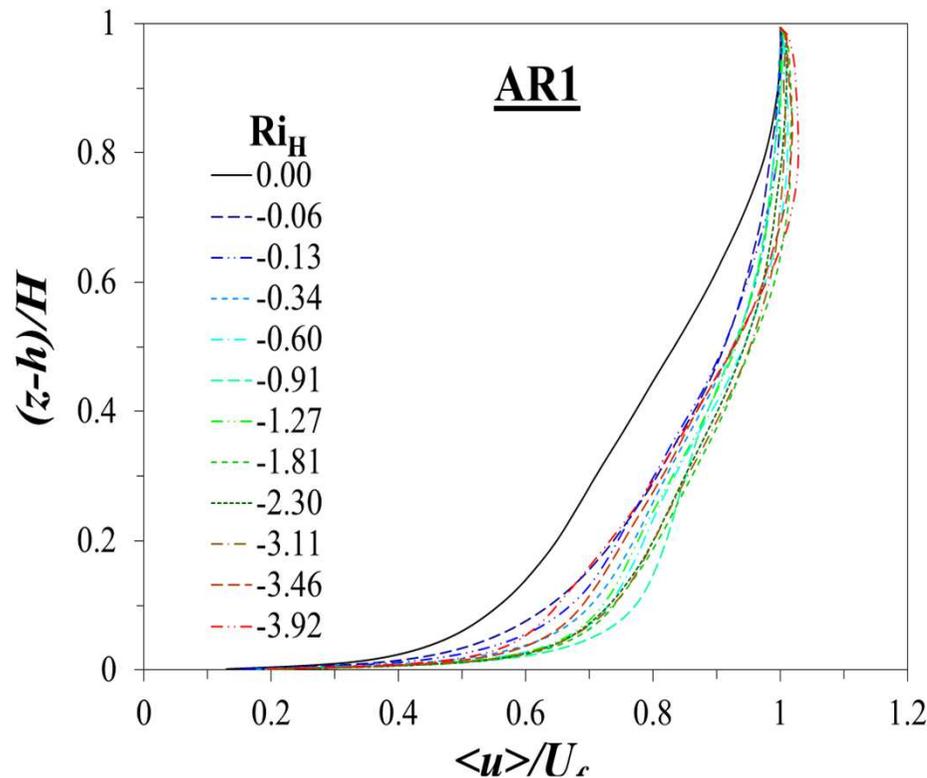
Comparison between LES & wind tunnel models

- Smaller magnitudes for wind fluctuations is observed since 2D geometry (ribs) is used in LES but 3D geometry is used in wind tunnel



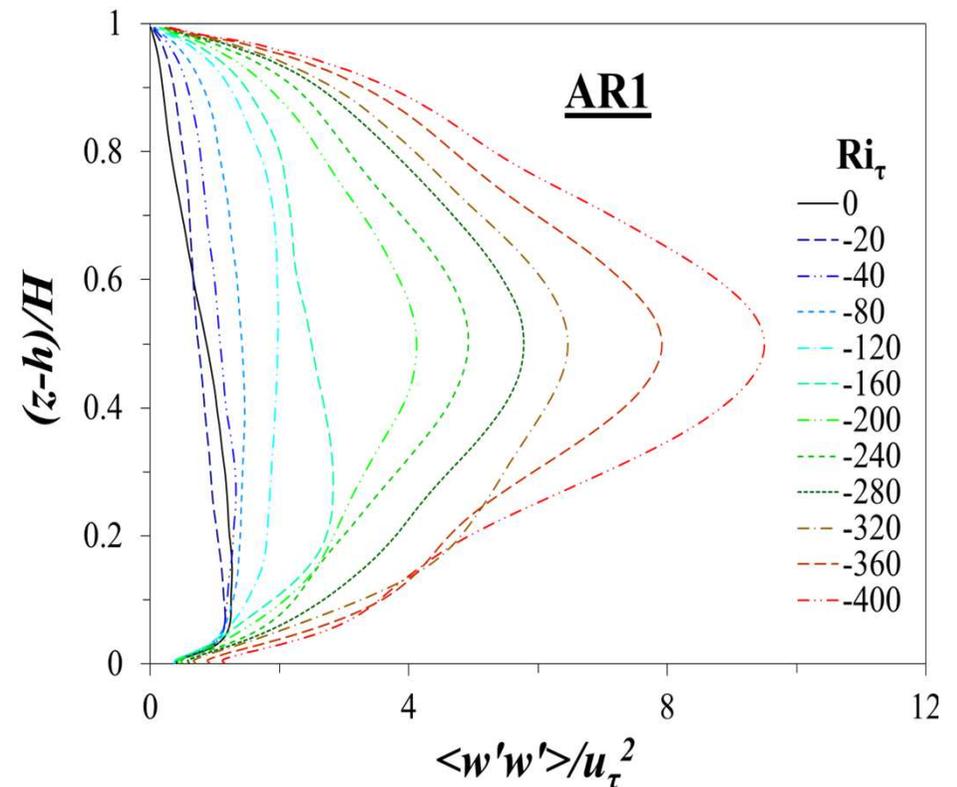
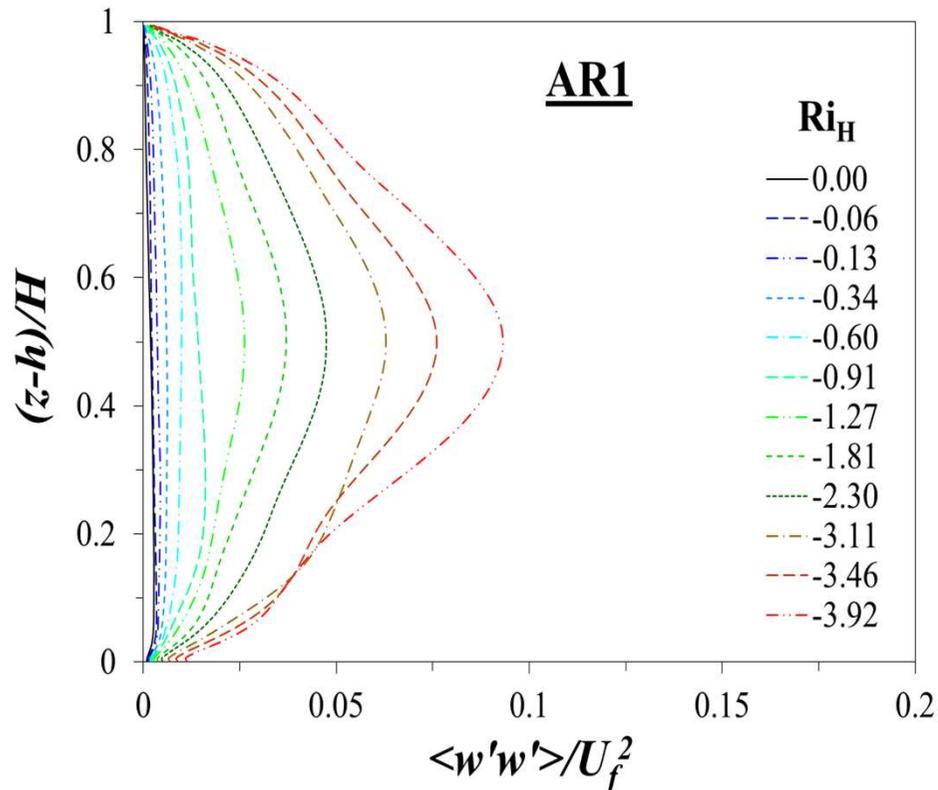
Mean flow above urban roughness

- The mean flow is further averaged in streamwise direction
- When instability increases, gradient of mean wind profile near roughness elements increases & it is more uniform above
- With constant driving force (constant u_τ), mean wind reduces with instability



Wind fluctuation above urban roughness

- When instability increases, wind fluctuation increases that implies enhanced turbulent mixing
- The local maximum point of fluctuation shifts upwards as instability increases



Logarithmic law of the wall

Smooth surface

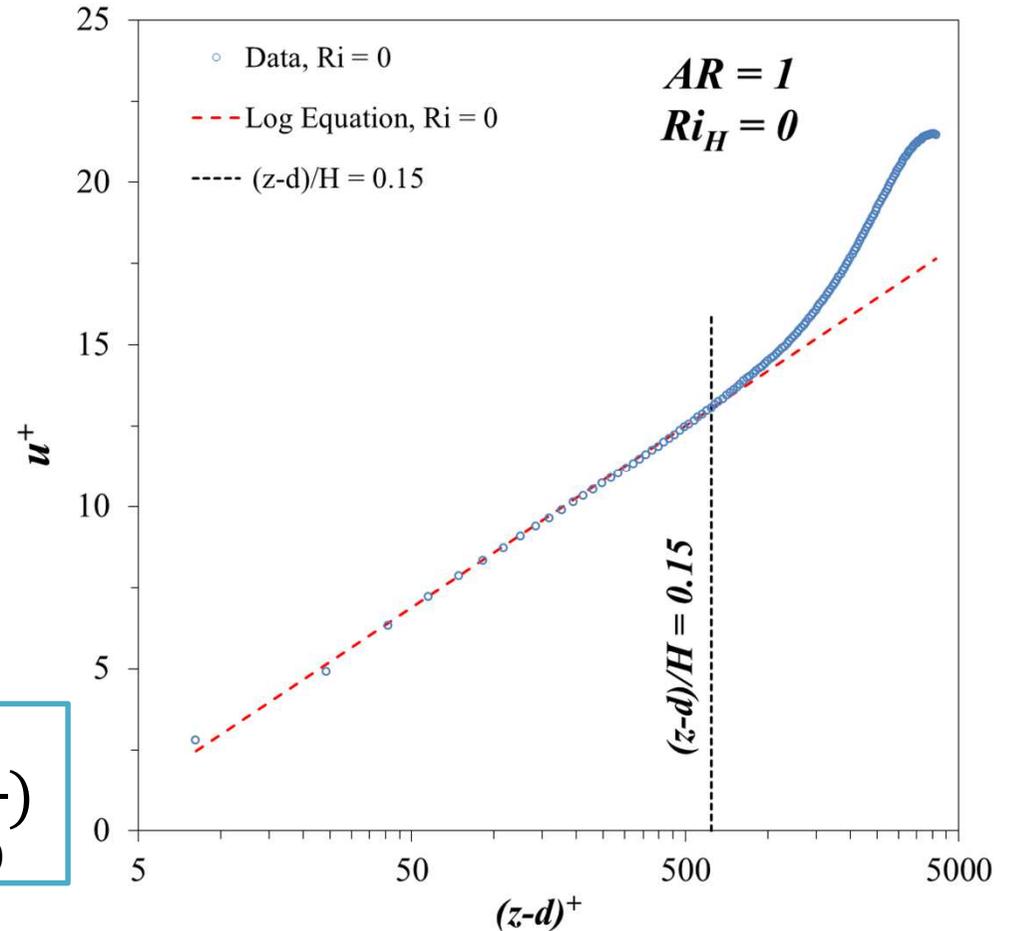
(by dimensional analysis):

$$\frac{du^+}{dz} = \frac{1}{z} \phi\left(\frac{z}{\delta_v}, \frac{z}{\delta}, \frac{z}{L}\right)$$

Neutral stratification:

($z/\delta_v \gg 1$, $z/\delta \ll 1$ & $z/L \sim 0$)

$$\frac{du^+}{dz} = \frac{1}{\kappa z} \rightarrow u^+ = \frac{1}{\kappa} \ln\left(\frac{z}{z_0}\right)$$



Rough surface:

$$u^+ = \frac{1}{\kappa} \ln\left(\frac{z-d}{z_0}\right)$$

where

$$u^+ = \frac{\langle u \rangle}{u_\tau} \text{ \& \ } \delta_v = \frac{\nu}{u_\tau}$$

u_τ : friction velocity

δ_v : viscous length scale

δ : boundary layer/channel height

L : Monin-Obukov length scale

κ : von Kármán constant (~ 0.41)

d : displacement height

Logarithmic law of the wall

Unstable stratification ($L < 0$):

$$\frac{du^+}{dz} = \frac{1}{\kappa z} \phi_M\left(\frac{z}{L}\right)$$

Expanding ϕ_M by Taylor's series and neglecting higher orders:

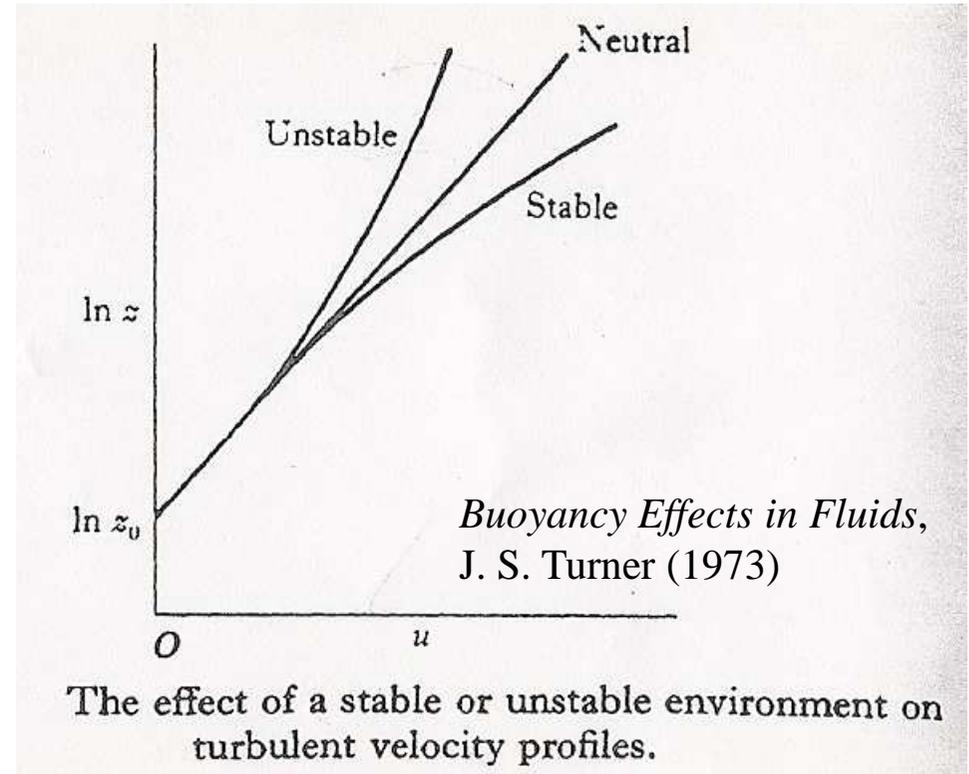
$$\frac{du^+}{dz} = \frac{1}{\kappa z} \left[1 + \alpha \left(\frac{z}{L} \right) \right]$$

$$u^+ = \frac{1}{\kappa} \left[\ln \frac{z}{z_0} + \alpha \frac{z}{L} \right]$$

for $z/L \ll 1$

Rough surface:

$$u^+ = \frac{1}{\kappa} \left[\ln \frac{z-d}{z_0} + \alpha \frac{z-d}{L} \right]$$



where α is an empirical constant
(~ 4.5 by Webb, 1970)

Monin-Obukov length:

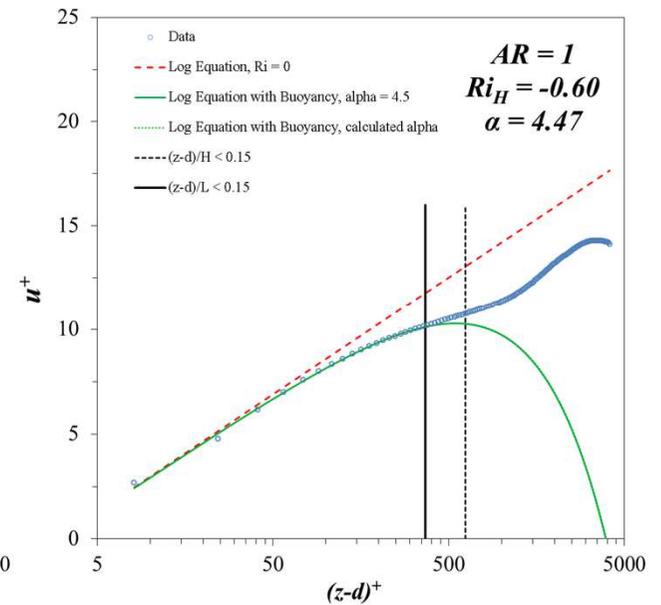
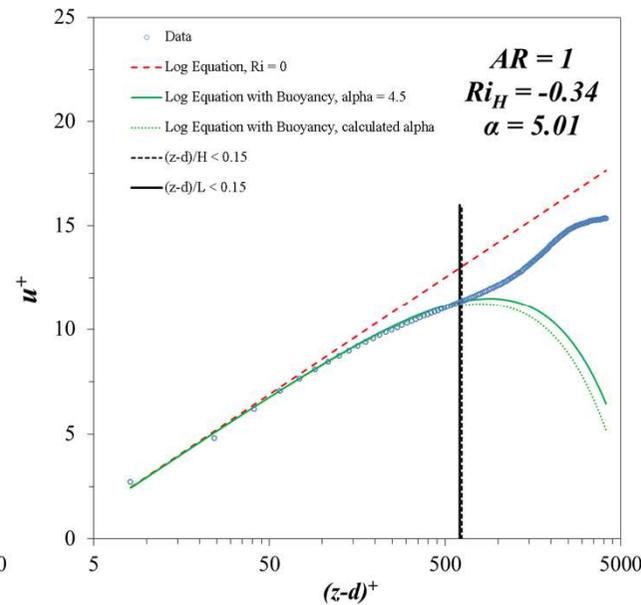
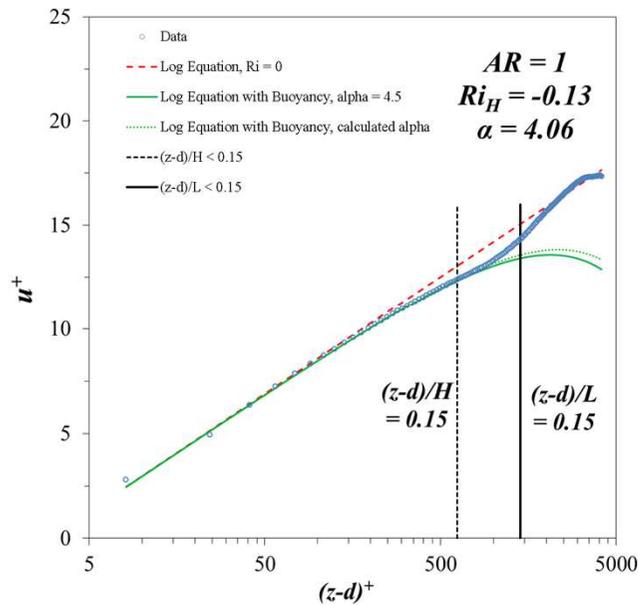
$$L = \frac{-u_\tau^3}{\kappa B}$$

Buoyancy flux:

$$B = \frac{g}{\theta} \cdot \overline{\theta' w'}$$

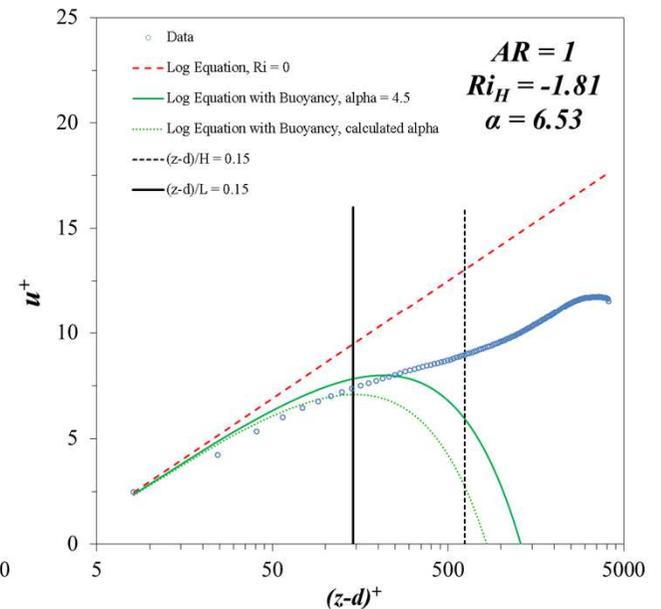
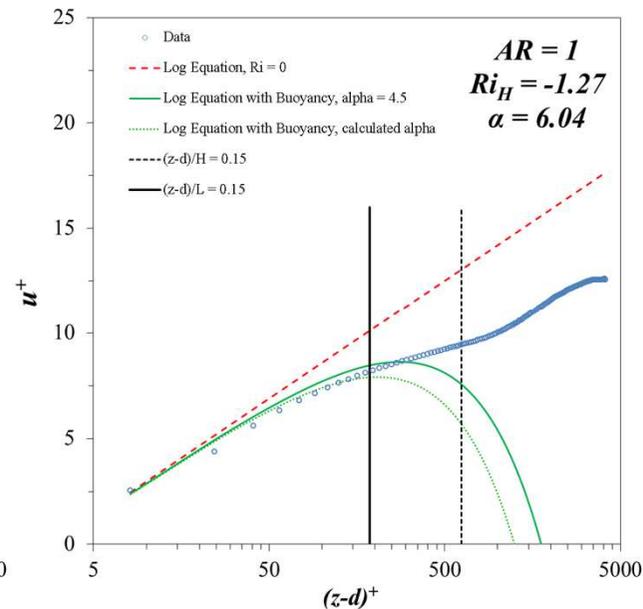
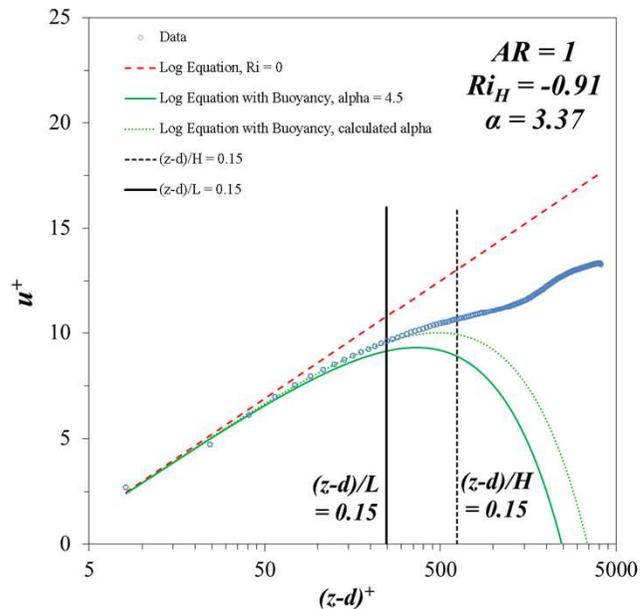
Logarithmic law of the wall

- For slightly unstable cases, mean wind profiles are well described by the log-law equation
- Decrease in wind speed is due to the increased drag by (enhanced) turbulent mixing
- Empirical constant α is calculated by the linear regression for small z/L (using data for $z/L < 0.15$) that is found to be ~ 4.5



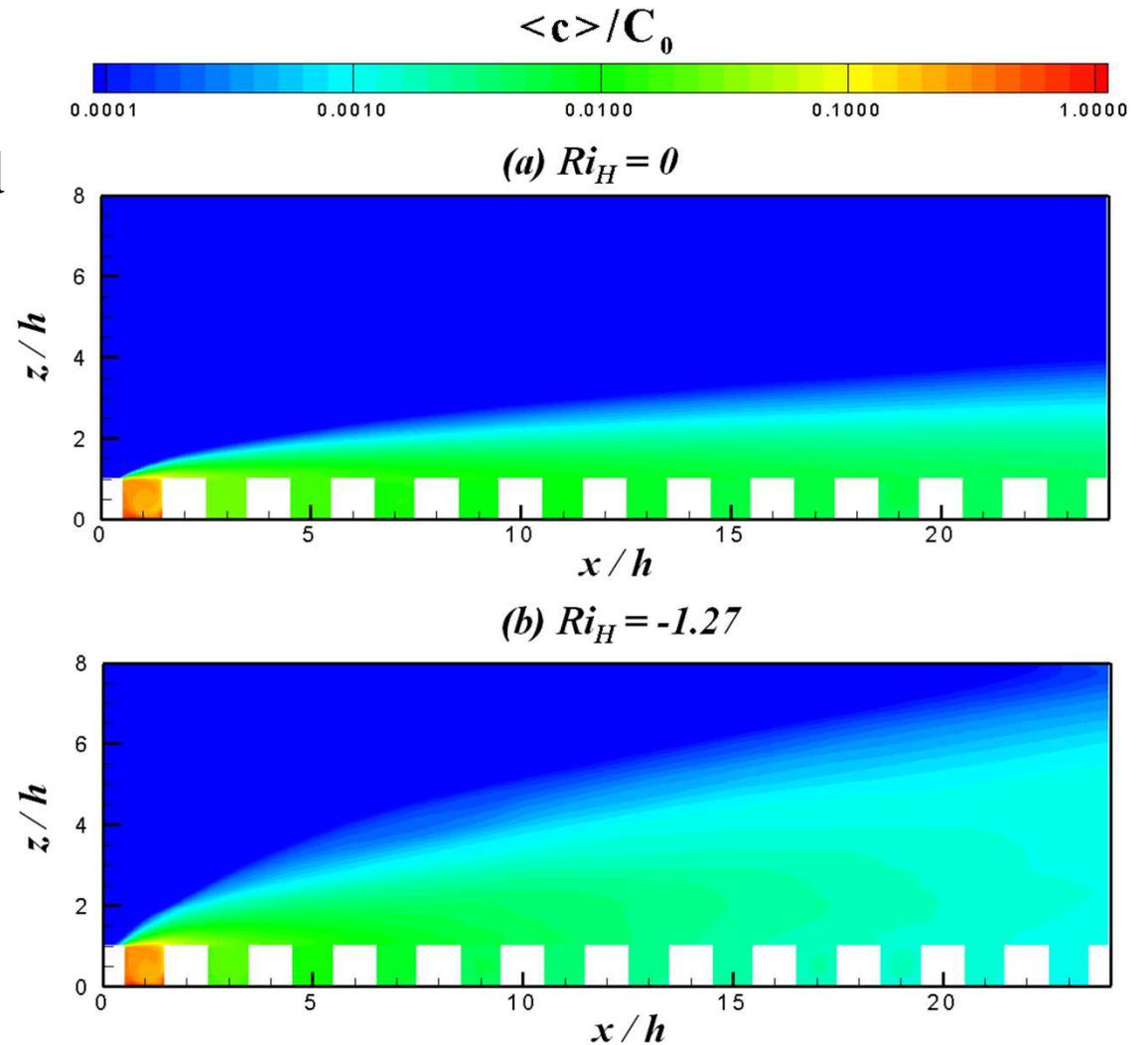
Logarithmic law of the wall

- Further increasing the intensity of instability, the wind profiles are not well described by the equation, since z/L starts to be significant
- d & z_0 also varies with instability (Ri)
- For very strong instability, buoyancy force changes the flow mechanism, thus another function of ϕ_M should be applied



Plume dispersion above urban roughness

- Constant area source on 1st street canyon ground
- Upward plume dispersion is promoted in unstable stratification
- Due to the enhanced turbulent mixing
- Less influence on the downstream areas



Conclusions

- The **LES** results show **similar trends** compared with those of the **wind tunnel** study by Uehara et al. (2000)
 - The deviation in magnitudes is due to the difference in **roughness geometry** (2D building elements in LES & 3D in wind tunnel study)
- The logarithmic law of the wall, which includes a **linear term of z/L** , describes well the mean wind profile only under **very slightly** unstable stratification
- When the unstable stratification **enhances**
 - 1) turbulence is **enhanced** everywhere
 - 2) mean wind profile **gradient** is **higher** near urban roughness due to the **enhanced shear** by **turbulent mixing**
 - 3) mean wind profile **deviates more** from (neutral) logarithmic law of the wall because of the **reduced wind speed**
 - 4) pollutant dispersion is **promoted** (in the vertical direction)



Thank you