



CFD MODELLING OF THE IMPACT OF URBAN HEDGEROWS ON AIR QUALITY IN AN IDEALIZED STREET CANYON

Riccardo Buccolieri¹, Elisa Gatto¹, Paolo Maria Congedo², Cristina Bagliivo² and Christof Gromke³

(1) Dipartimento di Scienze e Tecnologie Biologiche ed Ambientali, University of Salento, Lecce, Italy
(2) Department of Engineering for Innovation, University of Salento, Lecce, Italy
(3) Institute for Hydromechanics, Karlsruhe Institute of Technology KIT, Karlsruhe, Germany

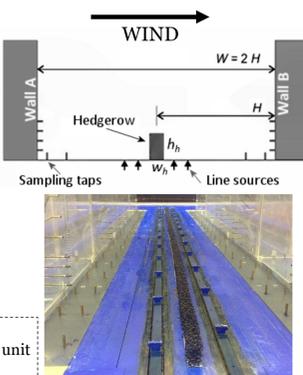
This poster presents a study of the effects of hedges on pollutant dispersion in an idealized street canyon of width-to-building height aspect ratio equal to 2. The dispersion of traffic pollutants is analyzed by CFD simulations and wind tunnel experiments.

Wind tunnel experiments

(Gromke et al., 2016; Atmospheric Environment, 139, 75-86)

a) Geometry and set-up

- Wind tunnel model: scale 1:150
- Isolated urban street canyon: length $L = 18\text{m}$, height $H = 18\text{m}$ and width $W = 36\text{m}$, i.e. aspect ratios $W/H = 2$ and $L/H = 10$
- One central hedgerow placed on the street
- Boundary layer flow: $\frac{U(z)}{U(z_{ref})} = \left(\frac{z}{z_{ref}}\right)^{a_U}$, $\frac{I(z)}{I(z_{ref})} = \left(\frac{z}{z_{ref}}\right)^{-a_I}$, $U(z_{ref}) = u_H = 4.65\text{m/s}$, $a_U = 0.30$, $a_I = 0.36$
- Four tracer gas emitting line sources
- Concentration measurement sampling taps at the bottom of the building walls (28 at each wall) and in the reduced traffic zones at pedestrian level (40 at each floor).
- Samples were analysed by Electron Capture Detection (ECD) yielding mean concentrations and normalized according to: $c^+ = \frac{cU_H H}{Q_l}$, $c =$ measured concentration, $Q_l =$ source strength per unit length of the gas emission



b) Vegetation model

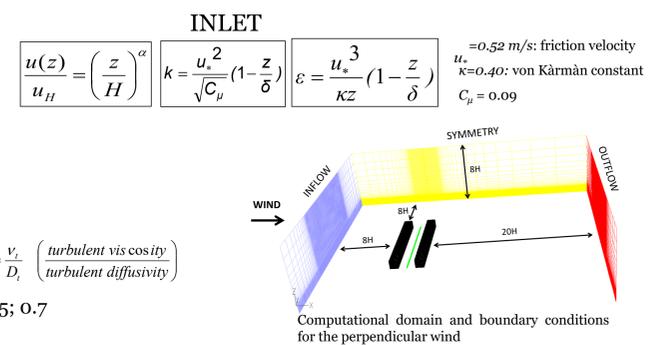
- Porous open-cell foam materials, with pore volume fractions - pressure loss coefficient λ :
 - 96.1% - 250m^{-1} (1.67m^{-1} at full scale)
 - 94.5% - 500m^{-1} (3.34m^{-1} at full scale)
- Full-scale hedgerows of height either $h_h = 1.50\text{m}$ or 2.25m and width $w_h = 1.50\text{m}$



CFD modelling simulations

a) Flow and dispersion set-up

- FLUENT (commercial CFD code)
- RANS-Equations
- turbulence closure scheme
 - standard $k-\epsilon$
- second order discretization schemes
- grid: hexahedral elements
 - $\sim 1,500,000$
 - $\delta_x = 0.05H$, $\delta_y = 0.05H$, $\delta_z = 0.03H$
 - expansion rate < 1.3
- turbulent Schmidt number $Sc_t = 0.3; 0.5; 0.7$



b) Vegetation model

- Momentum sink term added to standard fluid flow equations

$$S_i = -LAD c_d U u_i$$

where $LAD = \lambda/c_d$

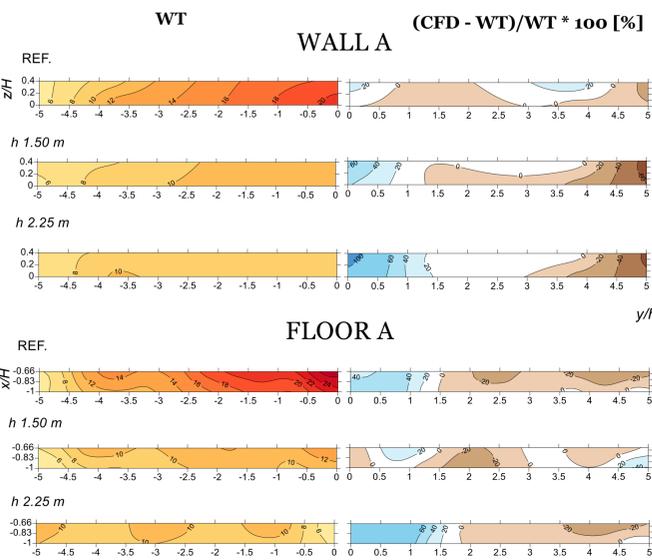
u_i = wind velocity component
 U = wind speed
 $c_d = 0.2$: drag coefficient for vegetation (dimensionless)
 LAD : leaf area density [m^2m^{-3}]

Summary of cases investigated (dimensions in full scale) by wind tunnel experiments and CFD simulations (Note: n=no; y=yes; ref.=reference case (no hedges))

| WT CFD | Hedge height h_h (m) | | | Pressure loss coefficient λ (m^{-1}) | | | Wind direction ($^\circ$) | |
|-----------|------------------------|-----|------|---------------------------------------------------------|------|------|-----------------------------|--------------|
| | 1 | 1.5 | 2.25 | 0 (ref.) | 1.67 | 3.34 | 90 (perp.) | 45 (oblique) |
| n | y | y | y | y | y | y | y | n |
| y | y | y | y | y | y | y | y | y |

Results

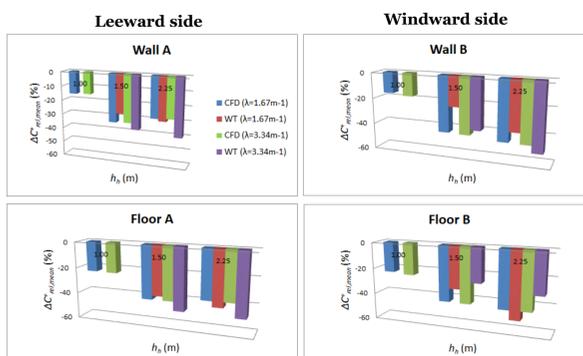
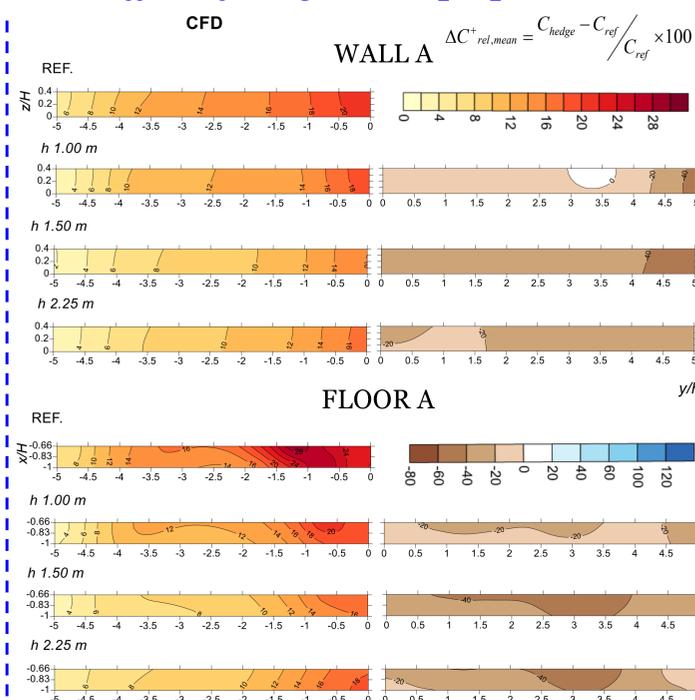
Validation (90°, perpendicular)



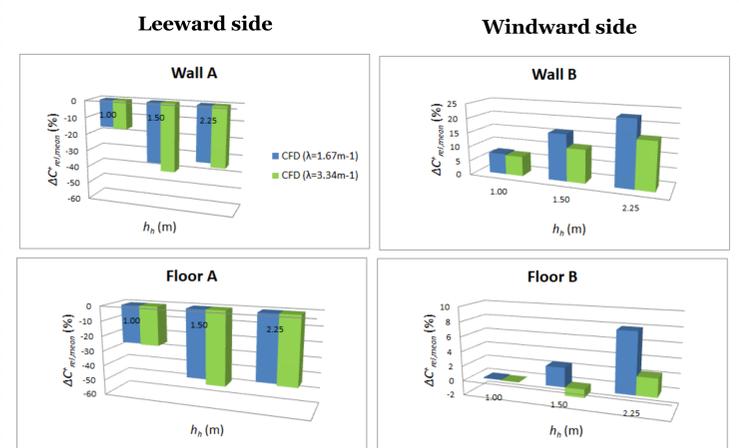
| λ (m^{-1}) | h_h (m) | WALL A | WALL B | FLOOR A | FLOOR B |
|-------------------------------|-----------|--------|--------|---------|---------|
| 1.67 | 1.50 | -27 | -34 | -23 | -43 |
| | 2.25 | -30 | -29 | -38 | -46 |
| 3.34 | 1.50 | -38 | -33 | -40 | -44 |
| | 2.25 | -40 | -28 | -52 | -46 |

Percentage differences of concentrations for street canyons with hedges referred to the reference case: $(C_{hedge} - C_{ref})/C_{ref} * 100$
Note: $Sc_t = 0.7$ for reference case, $Sc_t = 0.5$ for $h_h = 1\text{m}$ and $Sc_t = 0.3$ for the other cases

The effect of hedges (90°, perpendicular)



The effect of hedges (45°, oblique)



Conclusions

- Perpendicular wind direction (90°)**
 - Percentage differences quantitatively well predicted by the CFD model at both walls and floors
 - Higher hedges require lower values of Sc_t : the higher the hedge, the more the flow field is disturbed
 - The positive impact of hedges increases with increasing (i) hedge height from $h_h = 1\text{m}$ to $h_h = 1.50\text{m}$; and (ii) λ (or LAD), i.e. decreasing hedge porosity
- Oblique wind direction (45°)**
 - Similar to the perpendicular wind direction case, at the leeward side (side A) the positive impact of hedges increases with increasing height and porosity
 - At the windward side (side B), the impact of hedges turns to be adverse, with percentage increases up to about 20%. The negative impact (i) increases with increasing hedges height from $h_h = 1\text{m}$ to $h_h = 1.50\text{m}$ and 2.25m , due to the increased disturbance compared to the reference case; and (ii) decreases with increasing λ (or LAD)
 - Overall, concentrations at the windward side are much lower than those at the leeward side, and thus an overall decrease in concentrations occurs in the street canyon