

# Summary of results from the Jack Rabbit III international model inter-comparison exercise on Desert Tortoise and FLADIS

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# Aims

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- Run a model inter-comparison exercise to evaluate the performance of atmospheric dispersion models using data from previous ammonia release experiments
  - To understand the accuracy of models that may be used to design the Jack Rabbit III trials, e.g. to design the JR III sensor array
  - To identify important model input parameters that we may need to carefully assess or measure in the trials

# Methodology

- Simulate 3 trials each from the Desert Tortoise and FLADIS pressure-liquefied ammonia field trials
- Desert Tortoise
  - Tests conducted in 1983 at DOE Nevada Test Site
  - Release rates of 81 – 133 kg/s
  - 10 – 41 tonnes of ammonia released
  - Dispersion measurements at 100 m and 800 m
  - Largest tests to date on ammonia
- FLADIS
  - Tests conducted in 1993-4 at Landskrona, Sweden
  - Release rates of 0.25 – 0.55 kg/s
  - Dispersion measurements at 20 m, 70 m and 240 m (transition from dense to passive dispersion)

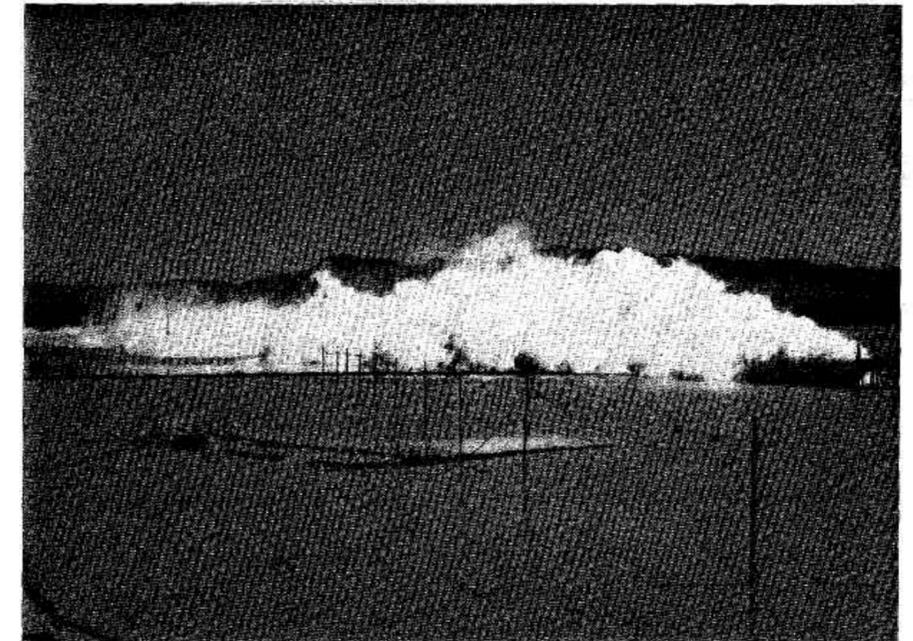


Fig. 15. Desert Tortoise 2 (upwind wide angle camera) Time = 230s. Lawrence Livermore National Laboratory



# Methodology

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- Participants provided with specified set of model inputs for Desert Tortoise and FLADIS
- Requested to provide basic set of model outputs (as a minimum)
  - Long time-averaged centerline plume concentrations for each of 6 trials
- Optionally, modelers can provide additional model outputs
  - E.g., predicted plume widths, temperatures, results from sensitivity tests
- Coordinators collated results, cross-plotted predictions against experimental measurements and shared results with participants
- Not a competition but a collaborative effort, with the ultimate goal of improving toxic industrial chemical modeling tools in general
- Timeline
  - Exercise initiated over Winter 2021-2022
  - Results shared with participants in Spring 2022
  - Concluded in Summer 2022 with aim to present findings at GMU conference

# Modeling Inputs

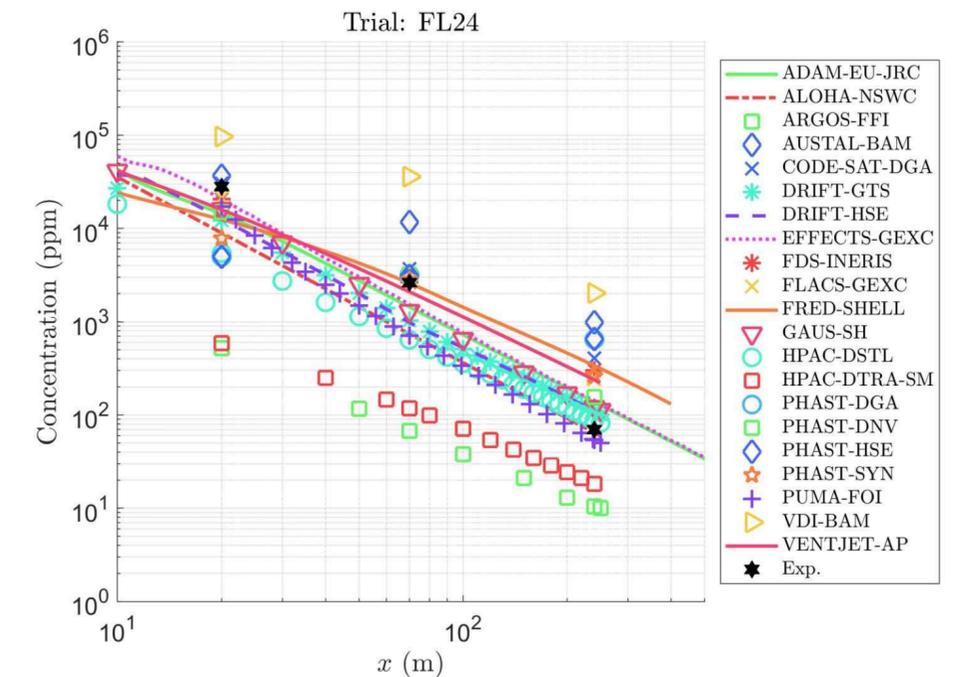
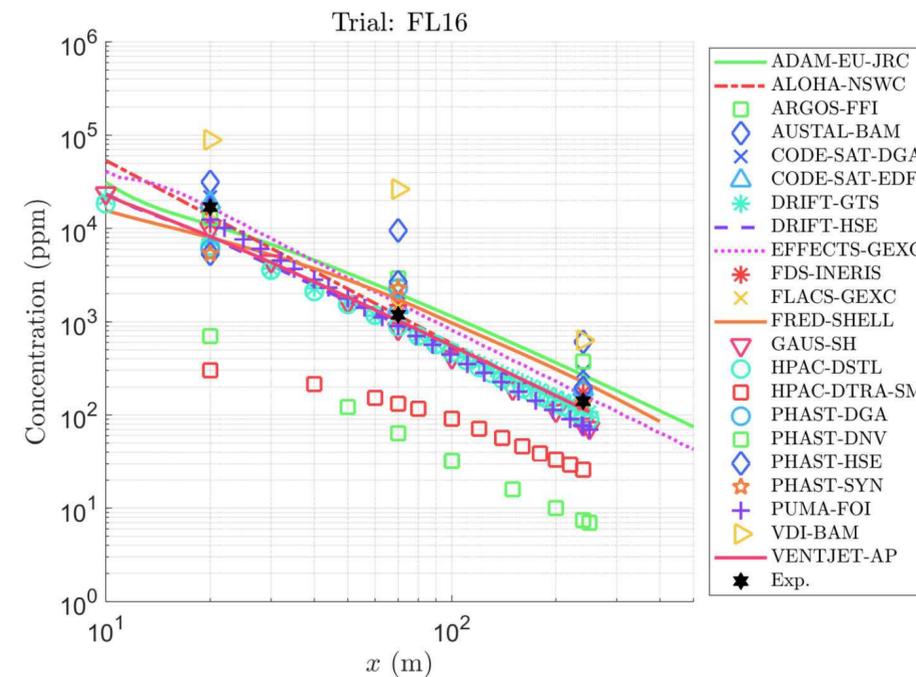
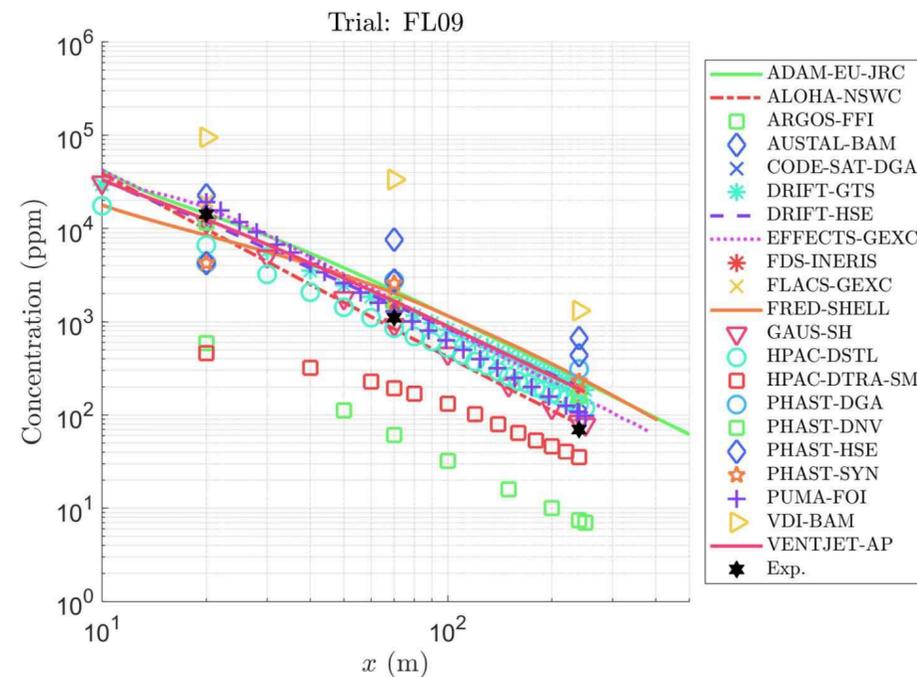
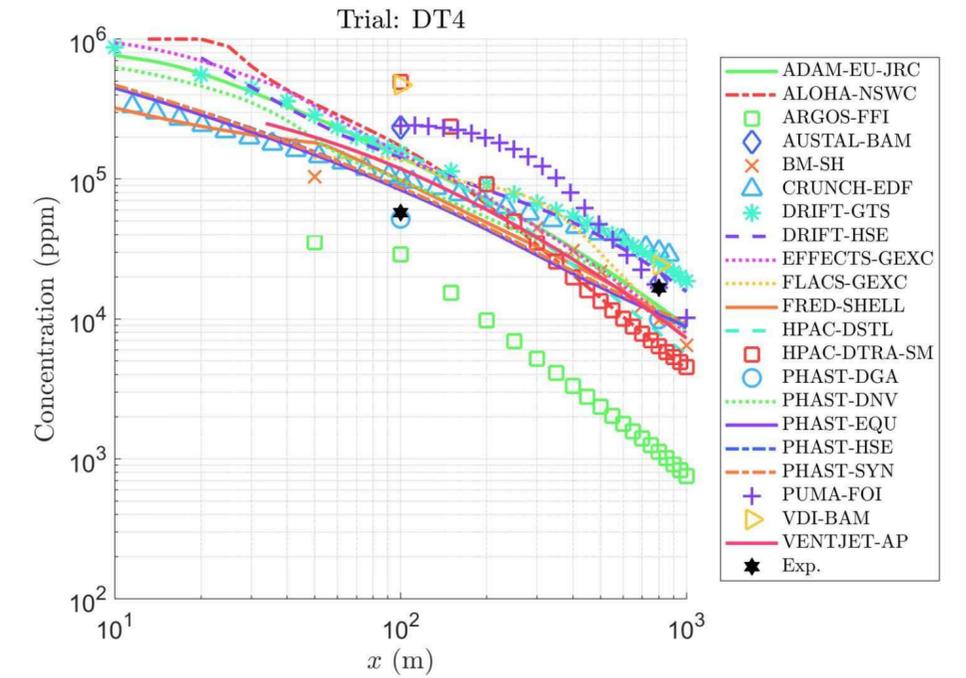
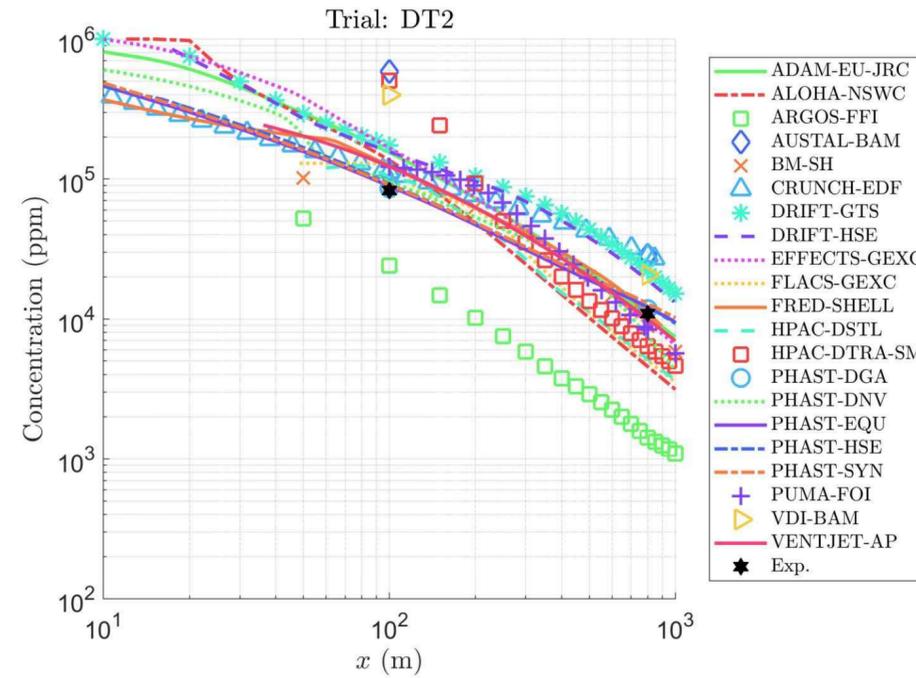
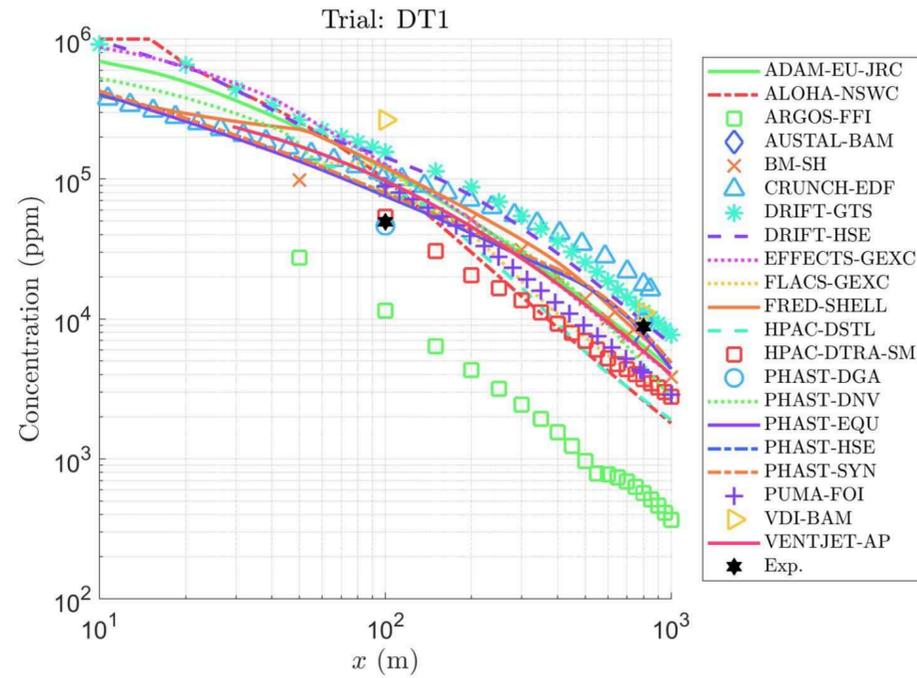
|  |      | DT1                | DT2              | DT4               | FLADIS9           | FLADIS16          | FLADIS24          |
|--|------|--------------------|------------------|-------------------|-------------------|-------------------|-------------------|
| Orifice diameter                               | m    | 0.081 <sup>a</sup> | 0.0945           | 0.0945            | 0.0063            | 0.004             | 0.0063            |
| Release height                                 | m    | 0.79               | 0.79             | 0.79              | 1.5               | 1.5               | 1.5               |
| Exit temperature                               | °C   | 21.5               | 20.1             | 24.1              | 13.7              | 17.1              | 9.45              |
| Exit pressure <sup>b</sup>                     | bara | 10.1               | 11.2             | 11.8              | 6.93 <sup>c</sup> | 7.98 <sup>c</sup> | 5.70 <sup>c</sup> |
|  | barg | 9.22               | 10.3             | 10.9              | 5.91              | 6.96              | 4.69              |
| Release rate                                   | kg/s | 80.0 <sup>d</sup>  | 117 <sup>e</sup> | 108 <sup>f</sup>  | 0.40              | 0.27              | 0.46              |
| Release duration                               | s    | 126                | 255              | 381               | 900               | 1200 <sup>g</sup> | 600               |
| Site average wind speed<br>at reference height | m/s  | 7.42               | 5.76             | 4.51 <sup>h</sup> | 6.1 <sup>i</sup>  | 4.4               | 4.9 <sup>j</sup>  |
|  | m    | 2                  | 2                | 2                 | 10                | 10                | 10                |
| Friction velocity                              | m/s  | 0.442              | 0.339            | 0.286             | 0.44              | 0.41              | 0.405             |
| Surface roughness                              | m    | 0.003              | 0.003            | 0.003             | 0.04              | 0.04              | 0.04              |
| Monin-Obukhov length                           | m    | 92.7               | 94.7             | 45.2              | 348               | 138               | -77               |
| Pasquill stability class                       | -    | D                  | D                | D-E <sup>k</sup>  | D                 | D-E               | C-D <sup>l</sup>  |
| Ambient temperature<br>at reference height     | °C   | 28.8               | 30.4             | 32.4              | 15.5              | 16.5              | 17.5              |
|  | m    | 0.82               | 0.82             | 0.82              | 1.5               | 1.5               | 1.5               |
| Ambient pressure                               | bar  | 0.909              | 0.910            | 0.903             | 1.020             | 1.020             | 1.013             |
| Relative humidity                              | %    | 13.2               | 17.5             | 21.3              | 86                | 62                | 53.6              |
| Averaging time for mean values                 | s    | 80                 | 160              | 300               | 600               | 600               | 400               |

- All trials involved horizontal releases of pressure-liquefied ammonia over flat, unobstructed terrain
- Data taken primarily from SMEDIS database (<https://admlc.com/smedis-dataset>)
- Cross-checks carried out with other information sources
  - Modelers Data Archive
  - REDIPHEM
  - Original data reports, e.g. Goldwire *et al.* (1985)
  - Notes provided to explain choice of values

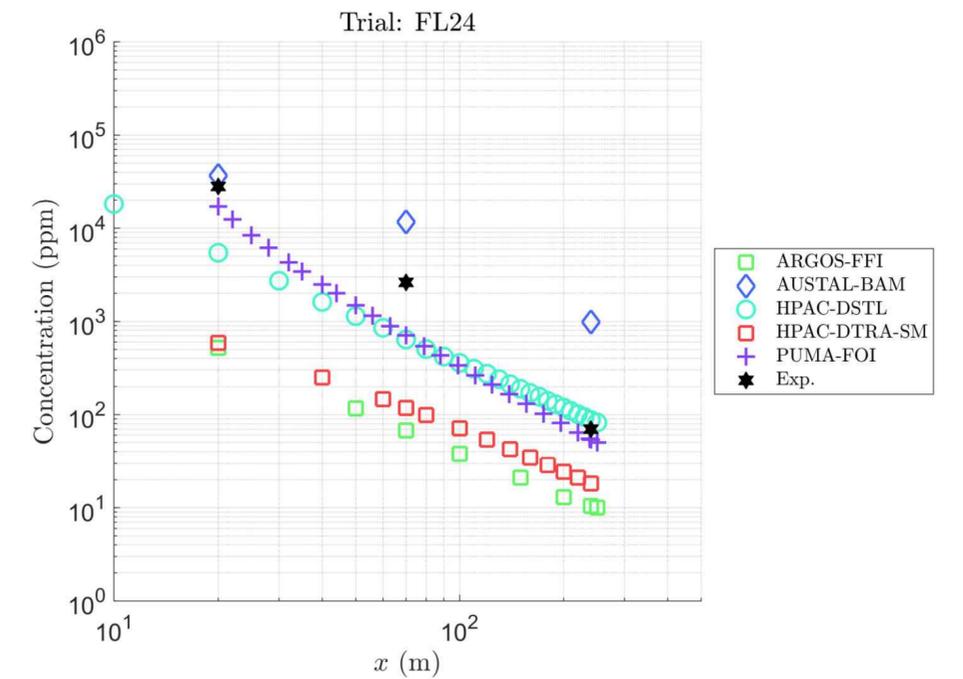
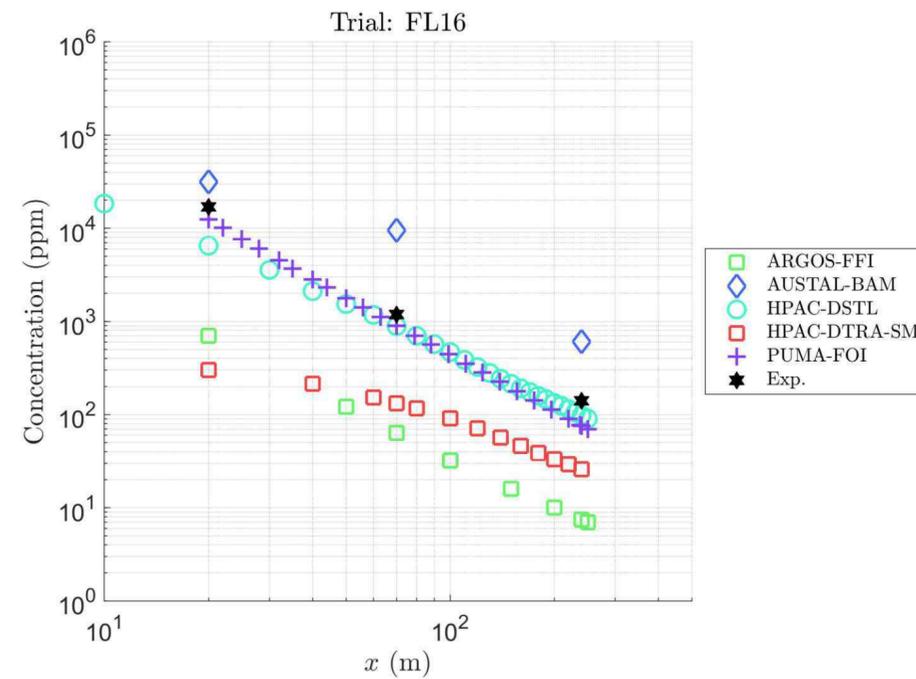
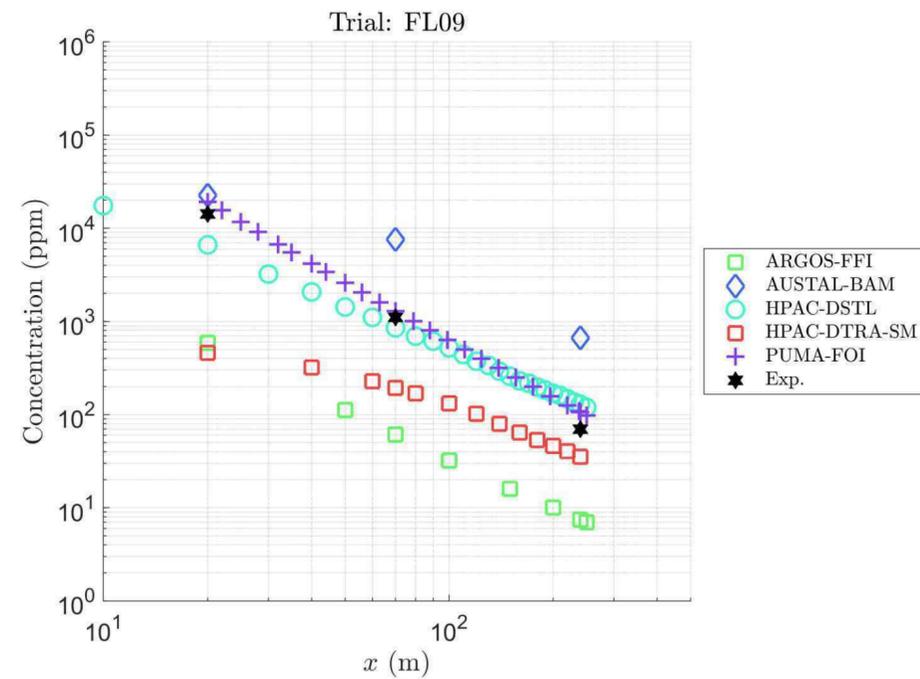
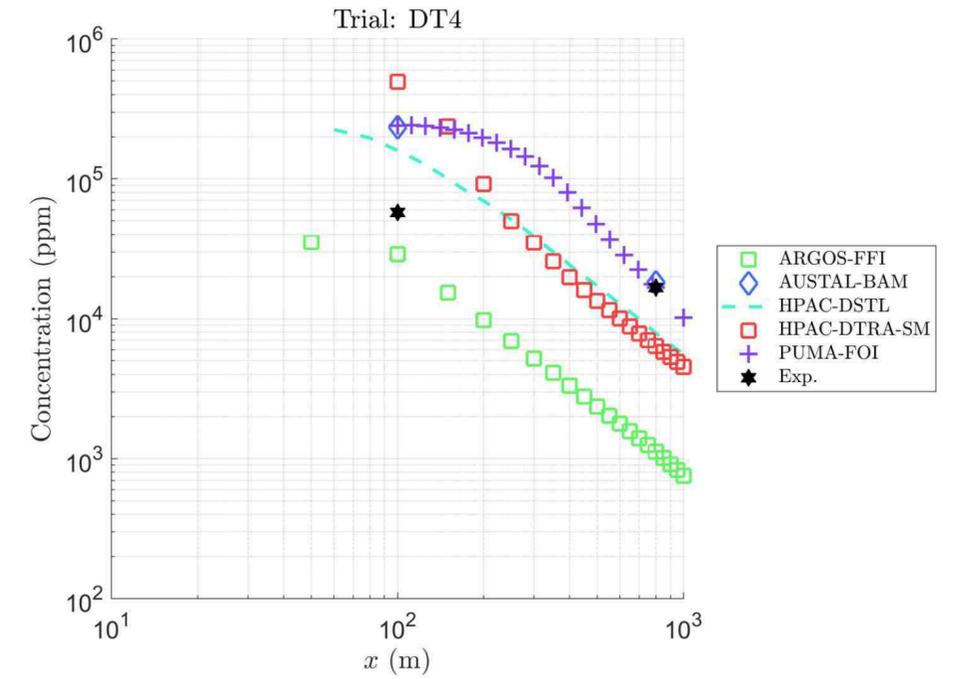
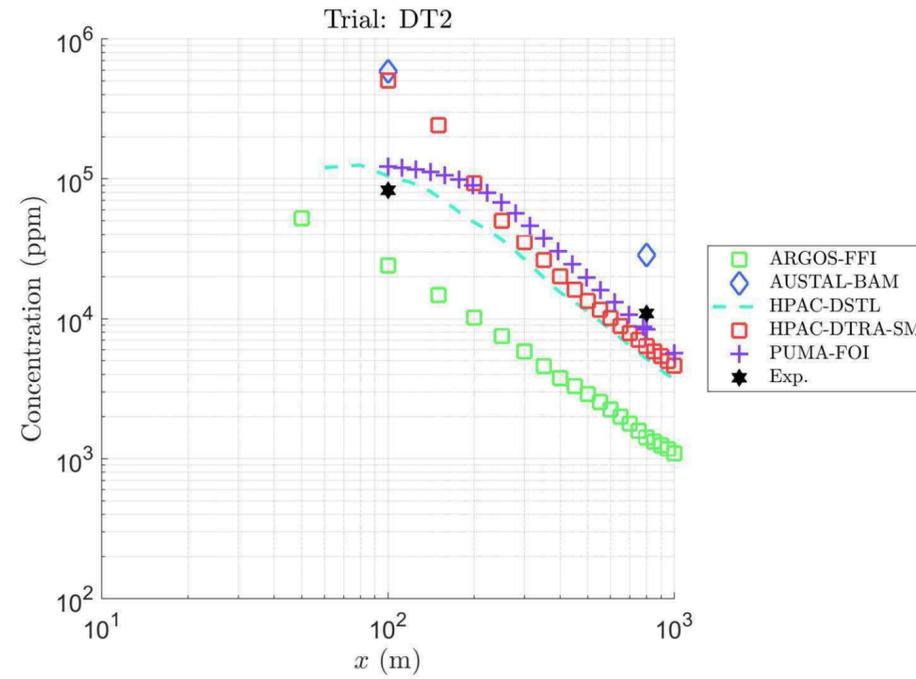
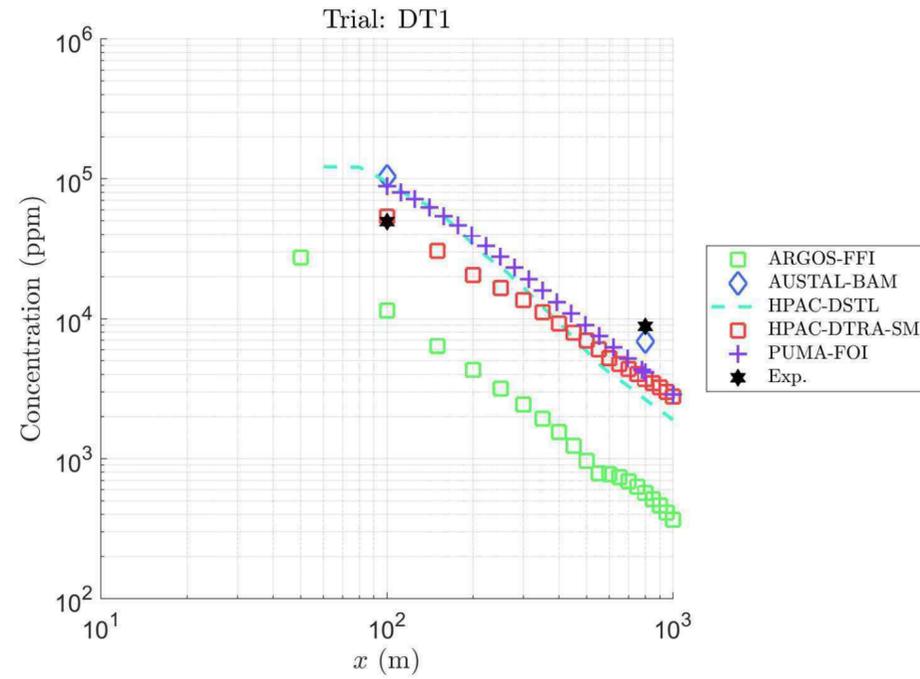
# Participants in the JR111 Initial Modeling Exercise

| #  | Organization                   | Model                | Model Type                            |          |                              |     | Desert Tortoise |   |   | FLADIS |    |    |
|----|--------------------------------|----------------------|---------------------------------------|----------|------------------------------|-----|-----------------|---|---|--------|----|----|
|    |                                |                      | Empirical nomogram/<br>Gaussian plume | Integral | Gaussian Puff/<br>Lagrangian | CFD | 1               | 2 | 4 | 9      | 16 | 24 |
| 1  | Air Products, USA              | VentJet              |                                       |          |                              |     |                 |   |   |        |    |    |
| 2  | BAM, Germany                   | AUSTAL               |                                       |          |                              |     |                 |   |   |        |    |    |
| 3  |                                | VDI                  |                                       |          |                              |     |                 |   |   |        |    |    |
| 4  | DGA, France                    | PHAST v8.6           |                                       |          |                              |     |                 |   |   |        |    |    |
| 5  |                                | Code-Saturne v6.0    |                                       |          |                              |     |                 |   |   |        |    |    |
| 6  | DNV, UK                        | PHAST v8.61          |                                       |          |                              |     |                 |   |   |        |    |    |
| 7  | DSTL, UK                       | HPAC v6.5            |                                       |          |                              |     |                 |   |   |        |    |    |
| 8  | DTRA, ABQ, USA                 | HPAC v6.7            |                                       |          |                              |     |                 |   |   |        |    |    |
| 9  | DTRA, Fort Belvoir, USA        | HPAC                 |                                       |          |                              |     |                 |   |   |        |    |    |
| 10 | EDF/Ecole des Ponts,<br>France | Code-Saturne v7.0    |                                       |          |                              |     |                 |   |   |        |    |    |
| 11 |                                | Crunch v3.1          |                                       |          |                              |     |                 |   |   |        |    |    |
| 12 | Equinor, Norway                | PHAST v8.6           |                                       |          |                              |     |                 |   |   |        |    |    |
| 13 | FFI, Norway                    | ARGOS v9.10          |                                       |          |                              |     |                 |   |   |        |    |    |
| 14 | FOI, Sweden                    | PUMA                 |                                       |          |                              |     |                 |   |   |        |    |    |
| 15 | Gexcon, Netherlands            | EFFECTS v11.4        |                                       |          |                              |     |                 |   |   |        |    |    |
| 16 | Gexcon, Norway                 | FLACS                |                                       |          |                              |     |                 |   |   |        |    |    |
| 17 | GT Science & Software          | DRIFT v3.7.19        |                                       |          |                              |     |                 |   |   |        |    |    |
| 18 | Hanna Consultants, USA         | Britter & McQuaid WB |                                       |          |                              |     |                 |   |   |        |    |    |
| 19 |                                | Gaussian plume model |                                       |          |                              |     |                 |   |   |        |    |    |
| 20 | HSE, UK                        | DRIFT v3.7.12        |                                       |          |                              |     |                 |   |   |        |    |    |
| 21 |                                | PHAST v8.4           |                                       |          |                              |     |                 |   |   |        |    |    |
| 22 | INERIS, France                 | FDS v6.7             |                                       |          |                              |     |                 |   |   |        |    |    |
| 23 | JRC, Italy                     | ADAM v3.0            |                                       |          |                              |     |                 |   |   |        |    |    |
| 24 | NSWC, USA                      | RAILCAR-ALOHA        |                                       |          |                              |     |                 |   |   |        |    |    |
| 25 | Shell, UK                      | FRED 2022            |                                       |          |                              |     |                 |   |   |        |    |    |
| 26 | Syngenta, UK                   | PHAST v8.61          |                                       |          |                              |     |                 |   |   |        |    |    |

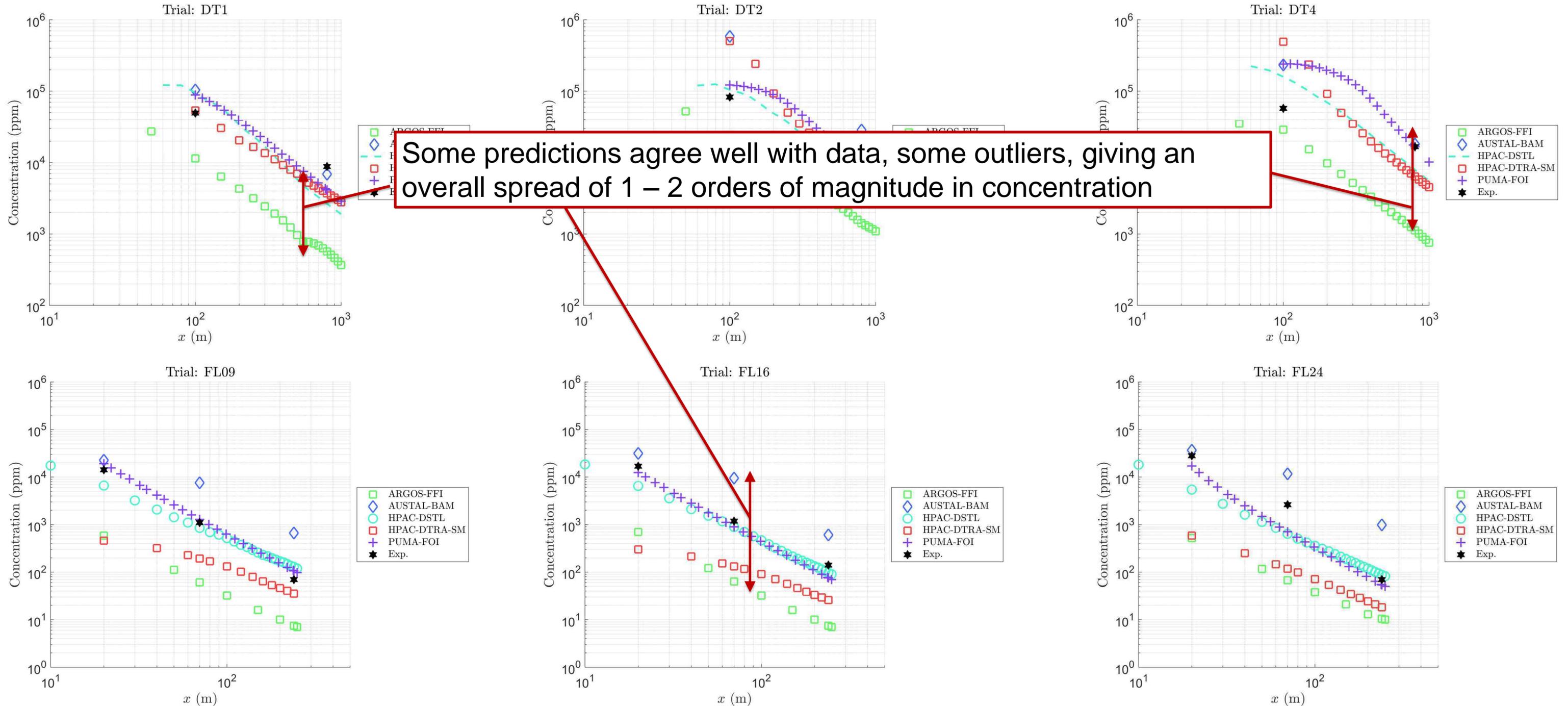
# All Model Results



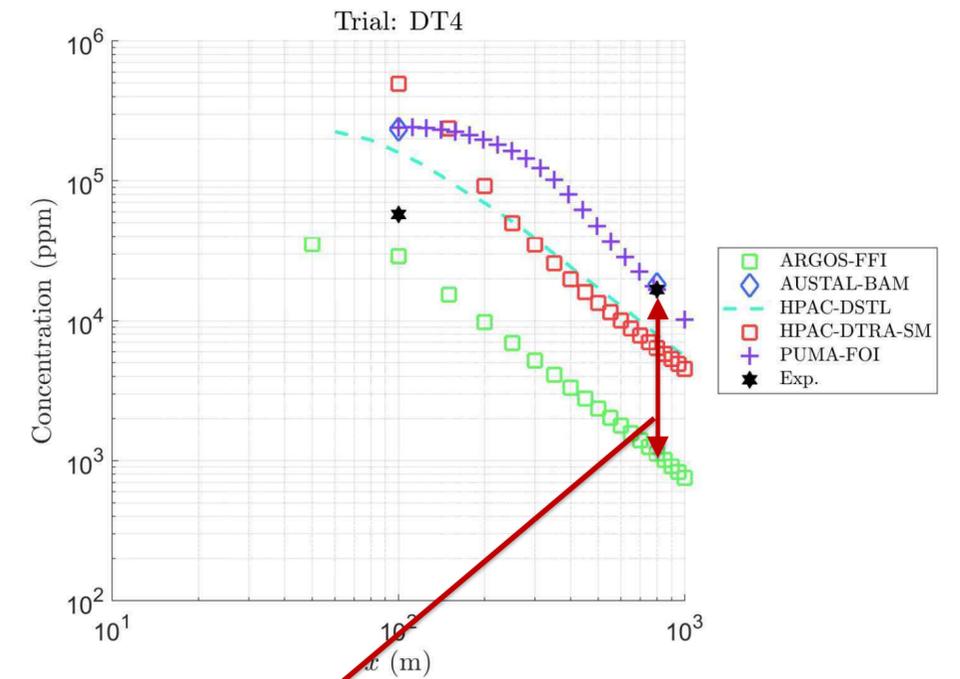
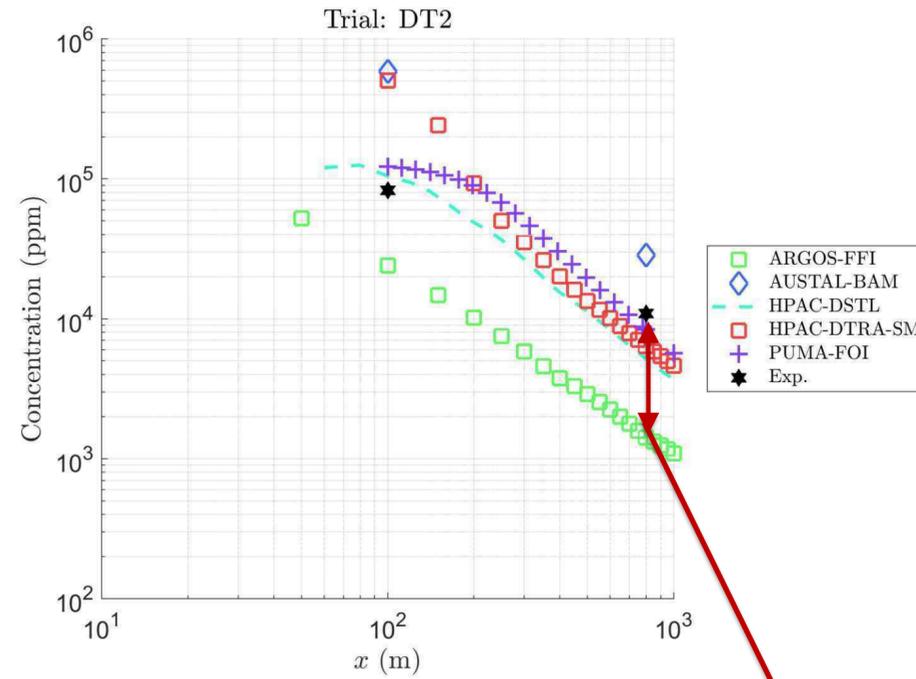
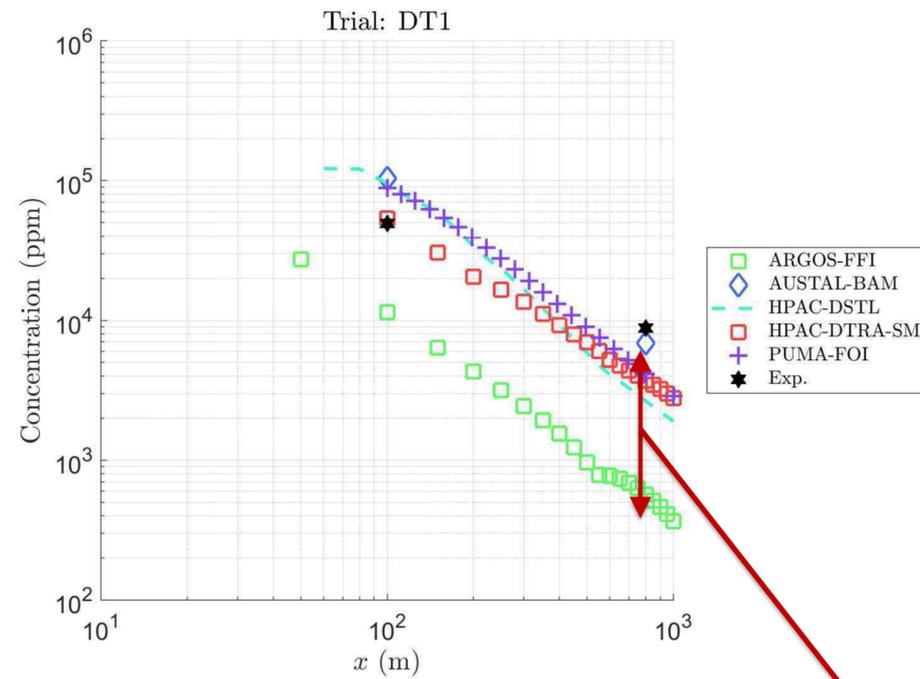
# Gaussian Puff, Lagrangian



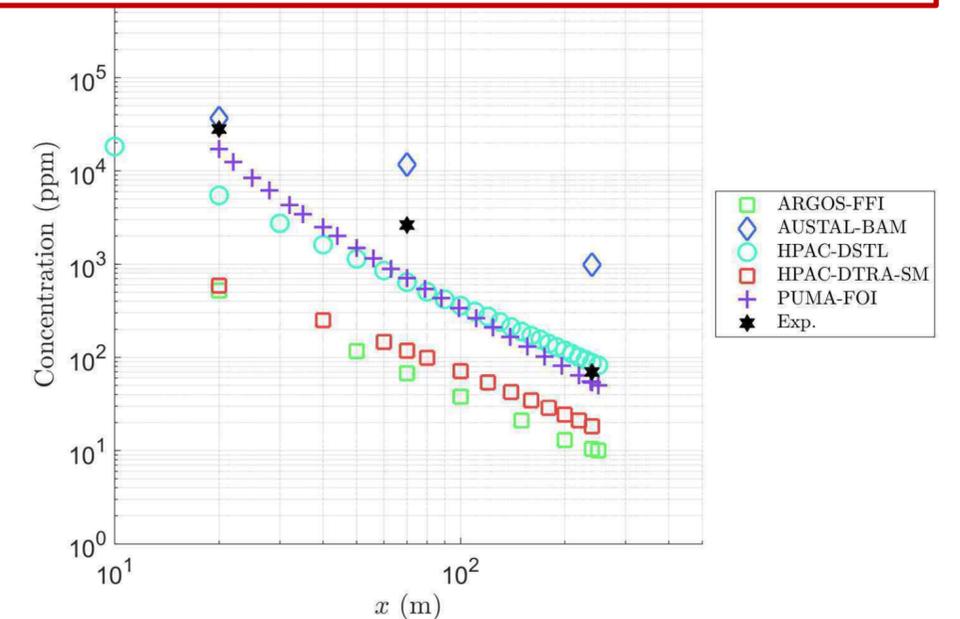
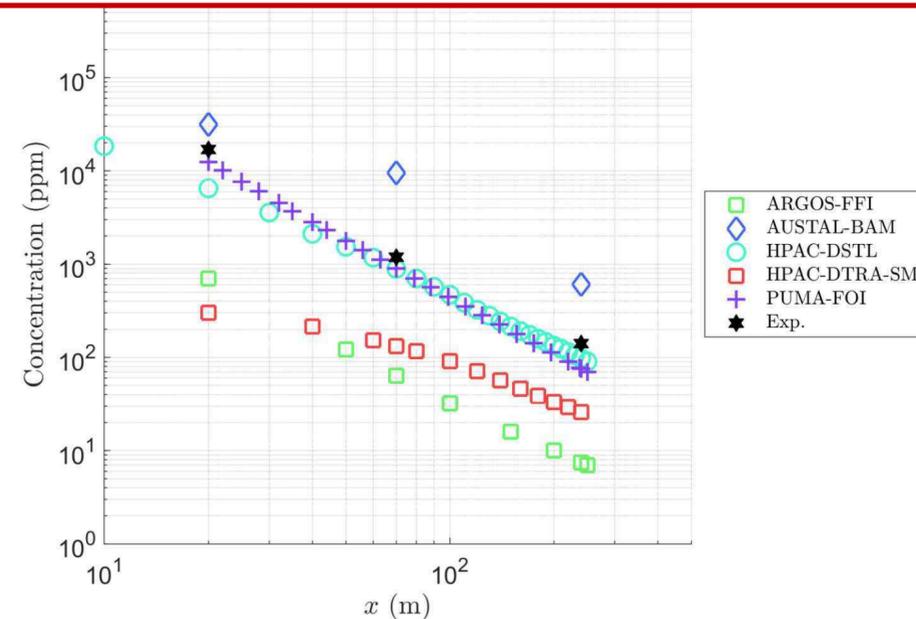
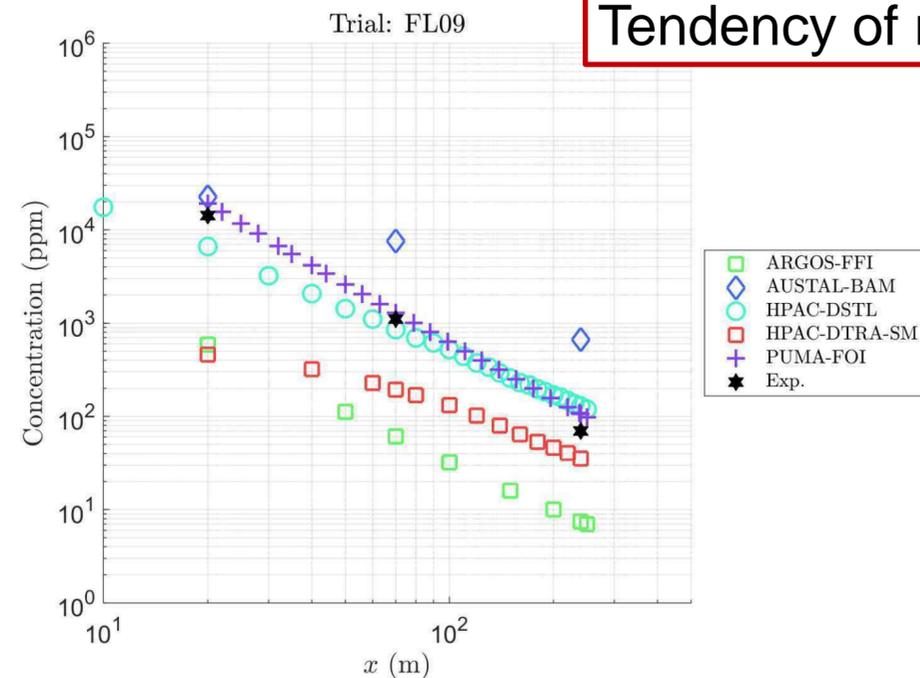
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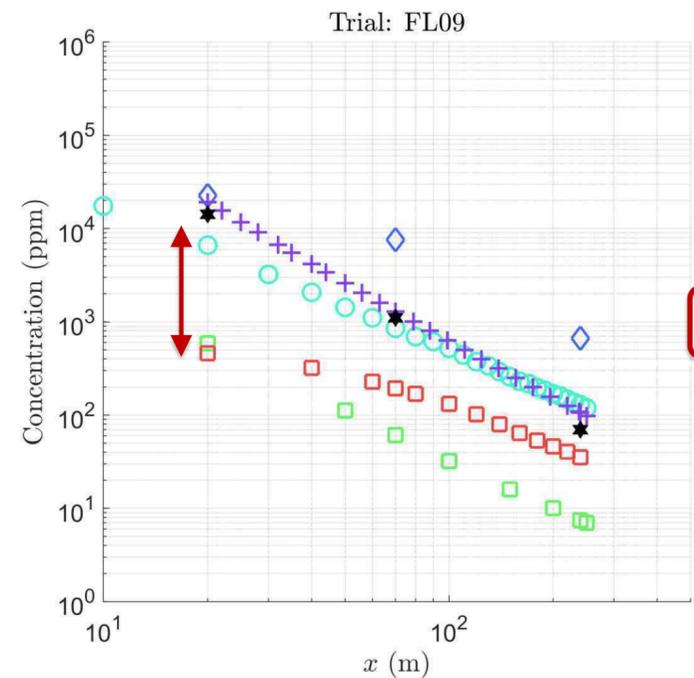
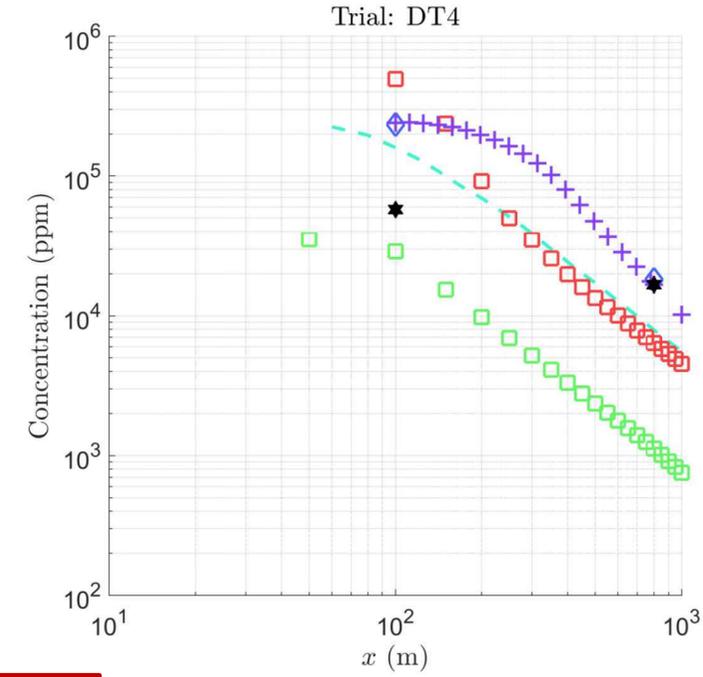
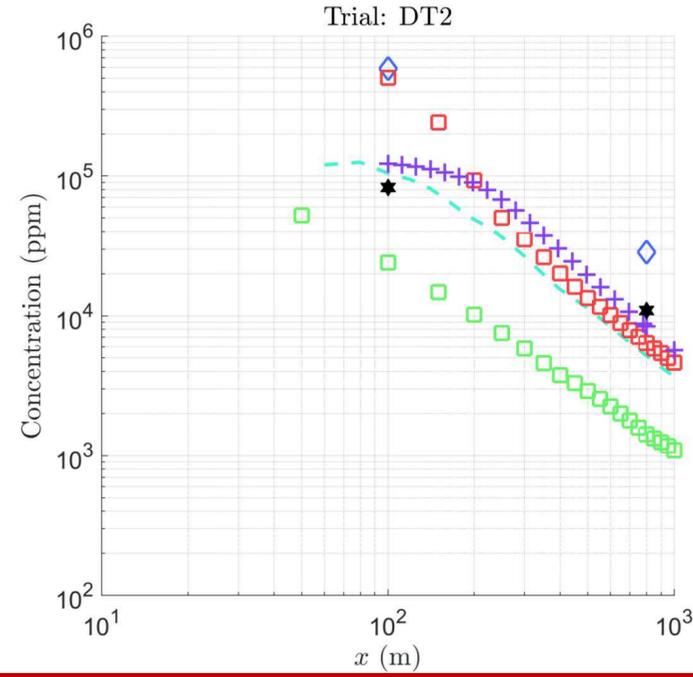
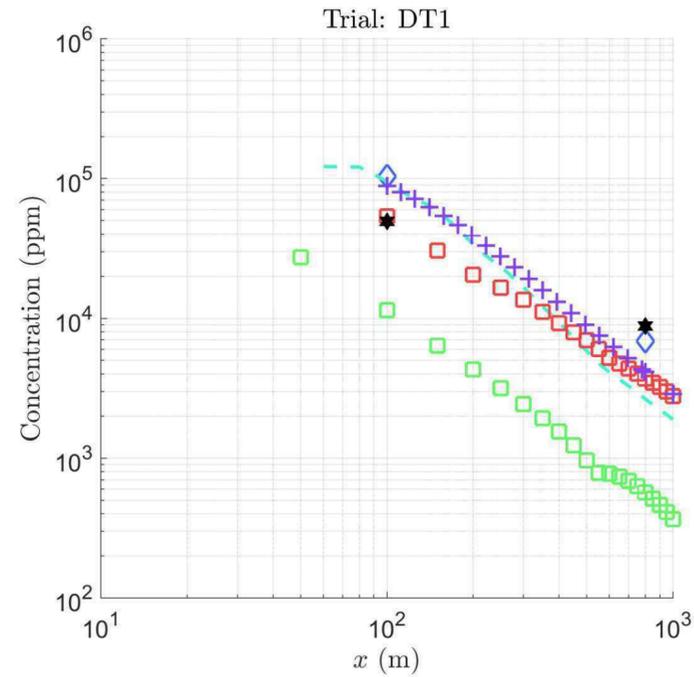
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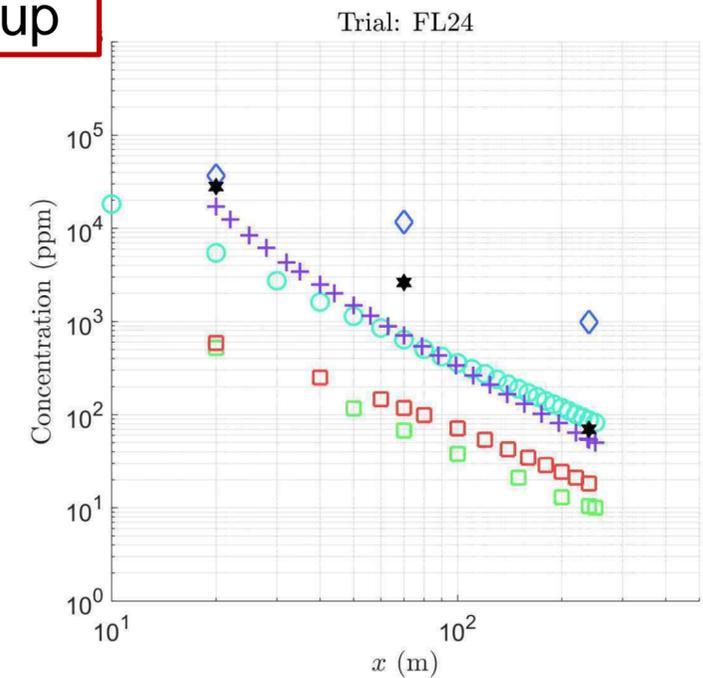
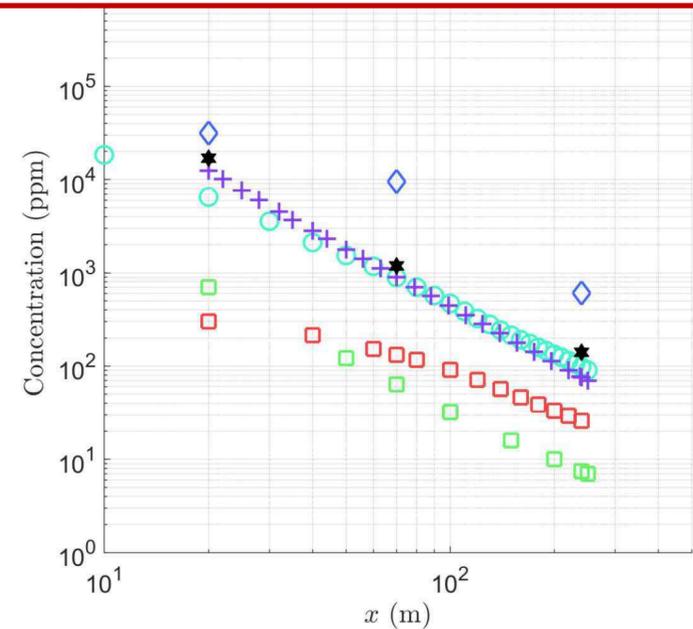
Tendency of most models to under-predict measured concentrations in far-field for Desert Tortoise



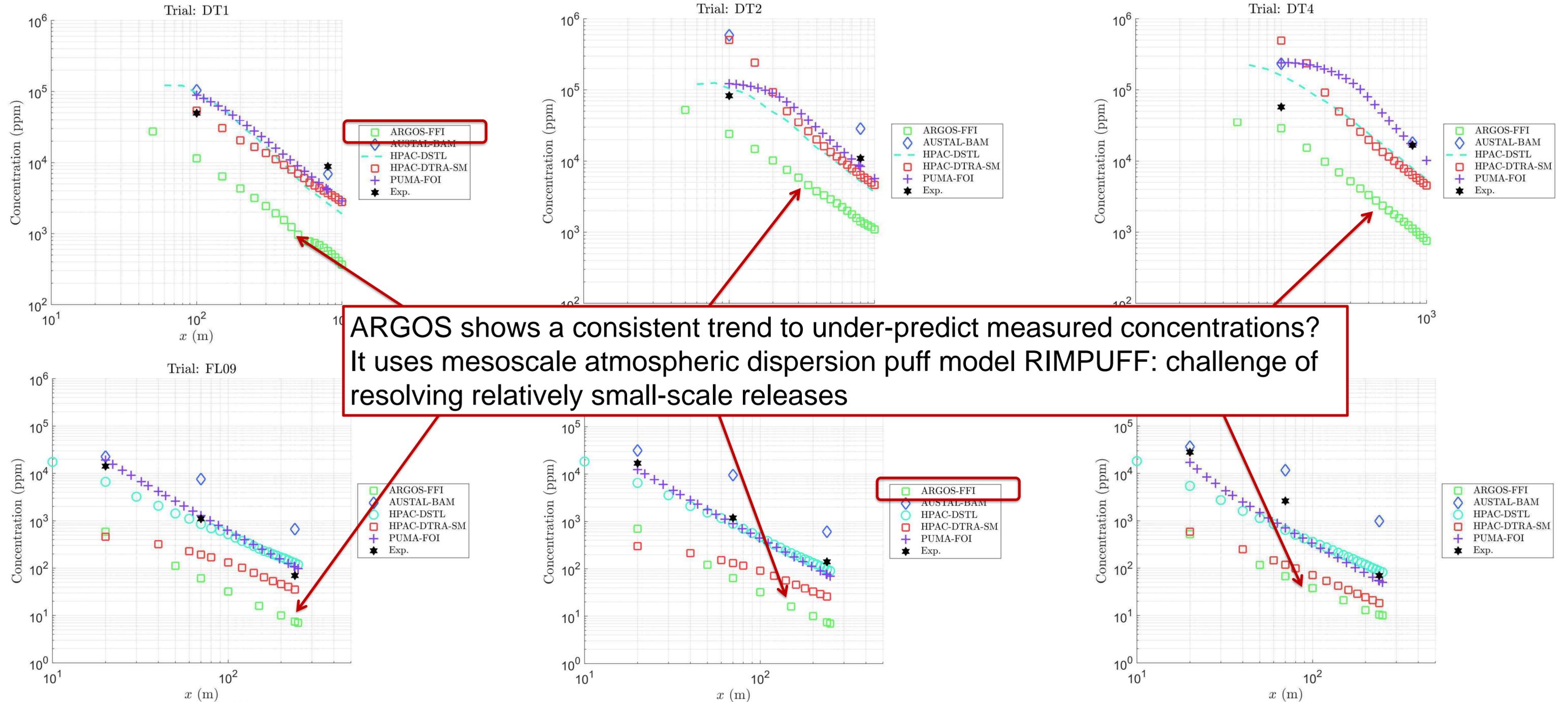
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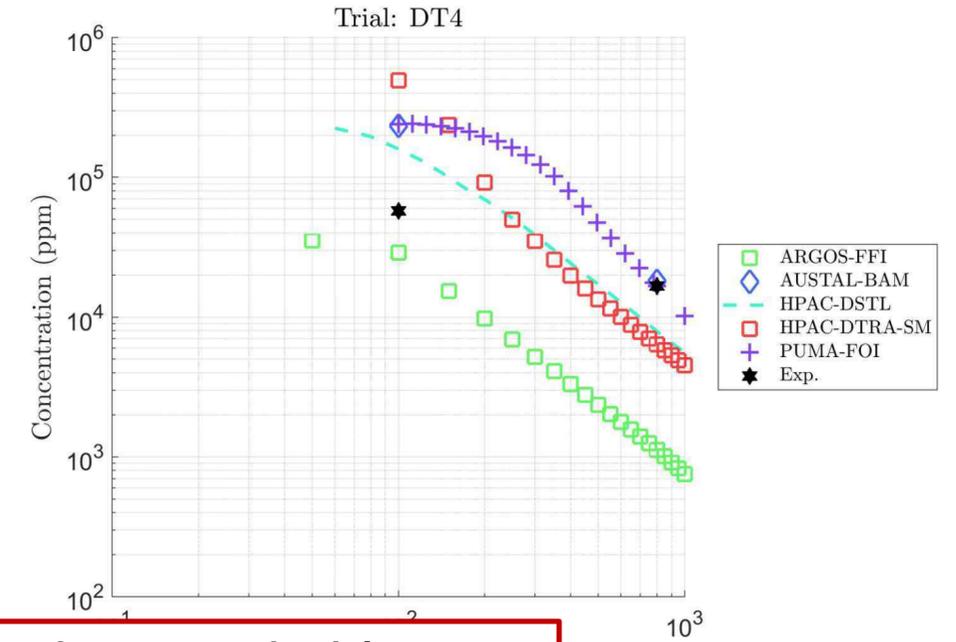
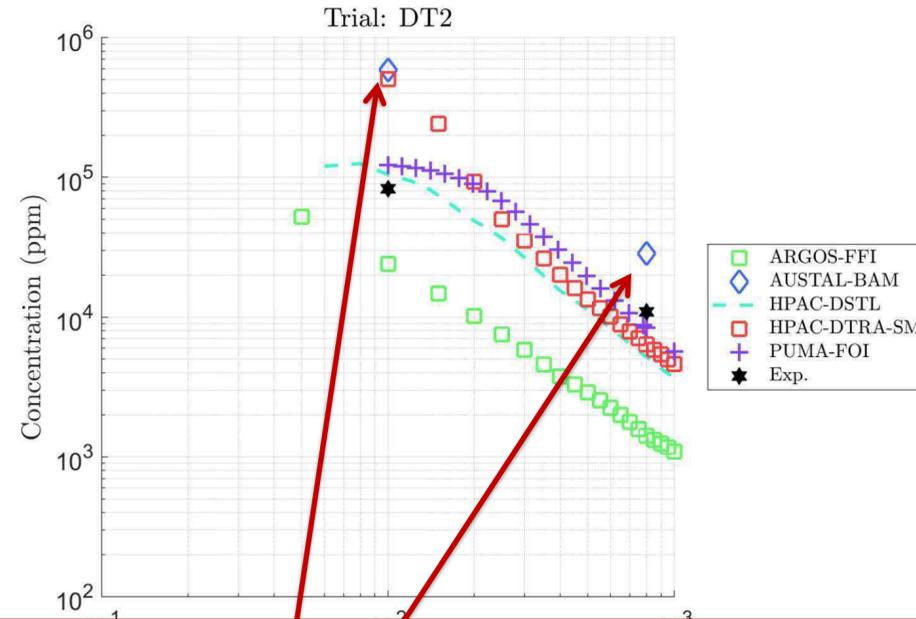
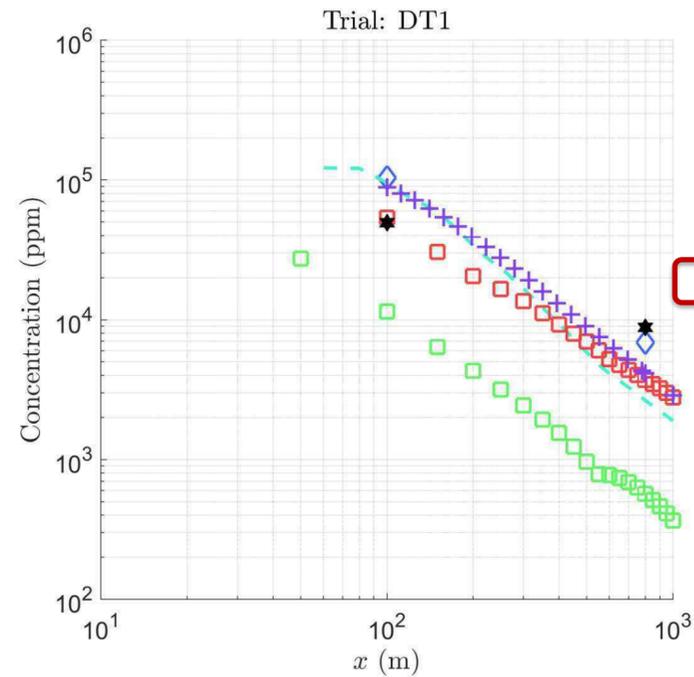
Spread in HPAC results: effect of different model setup



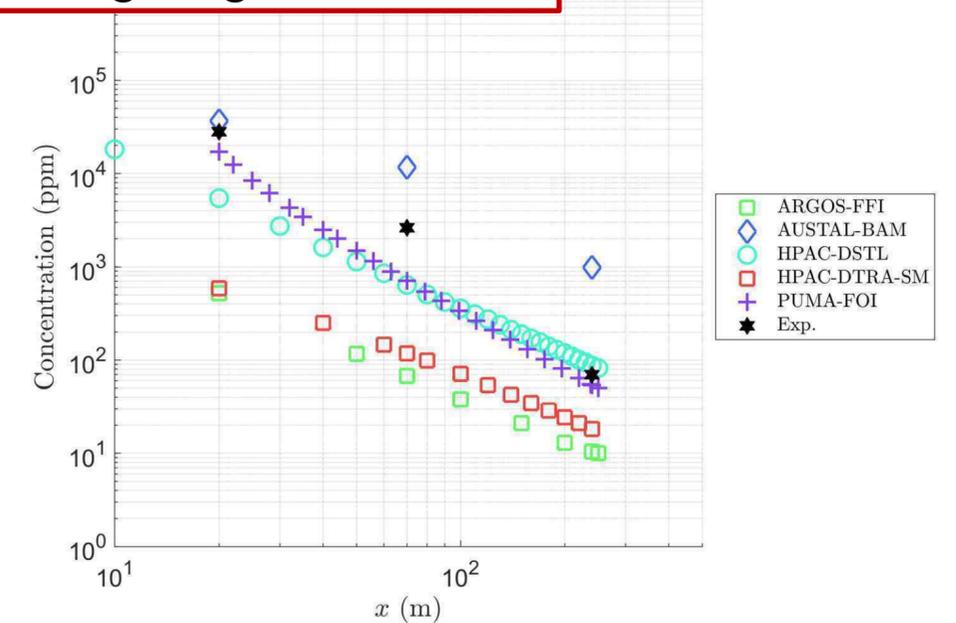
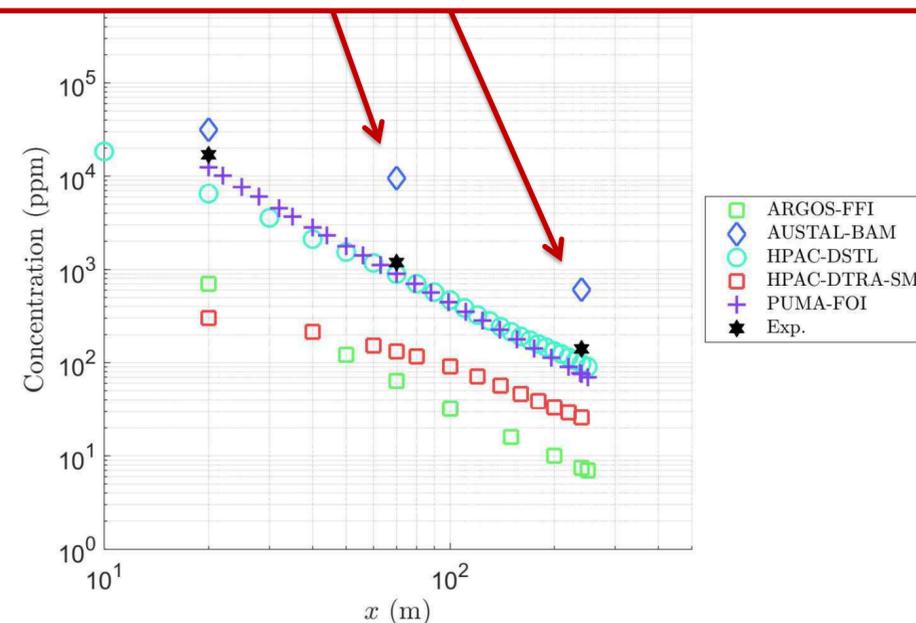
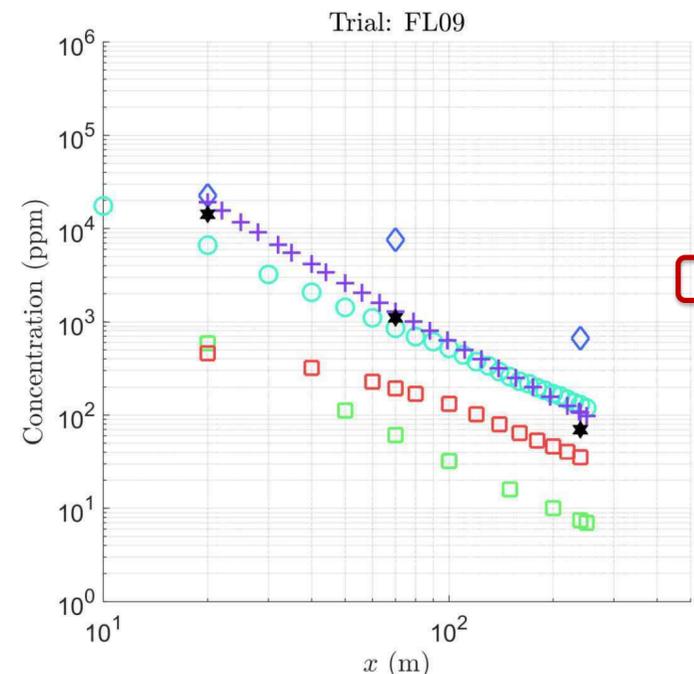
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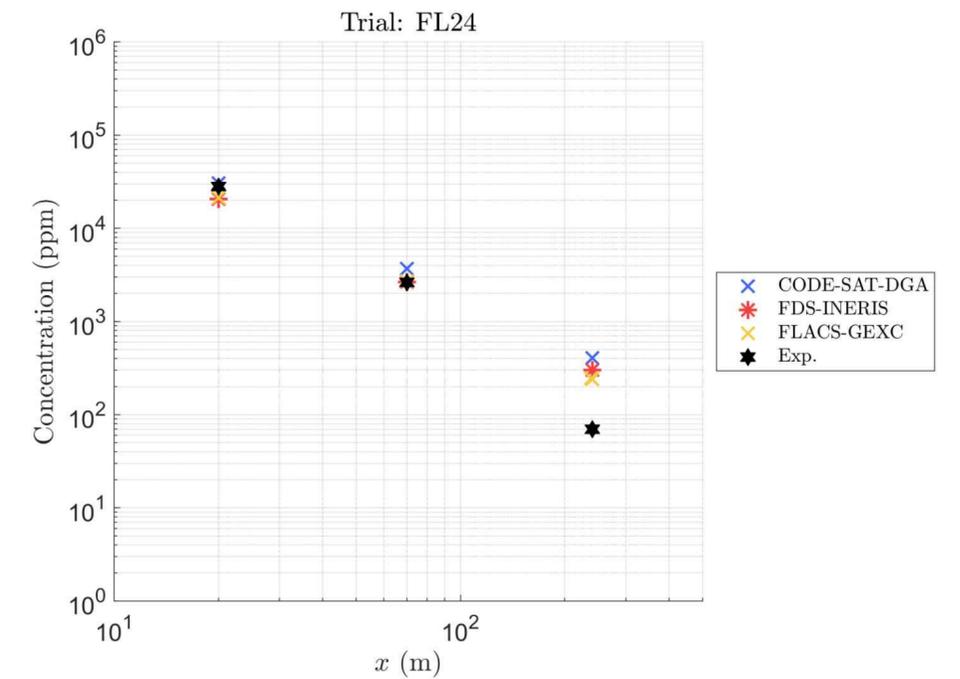
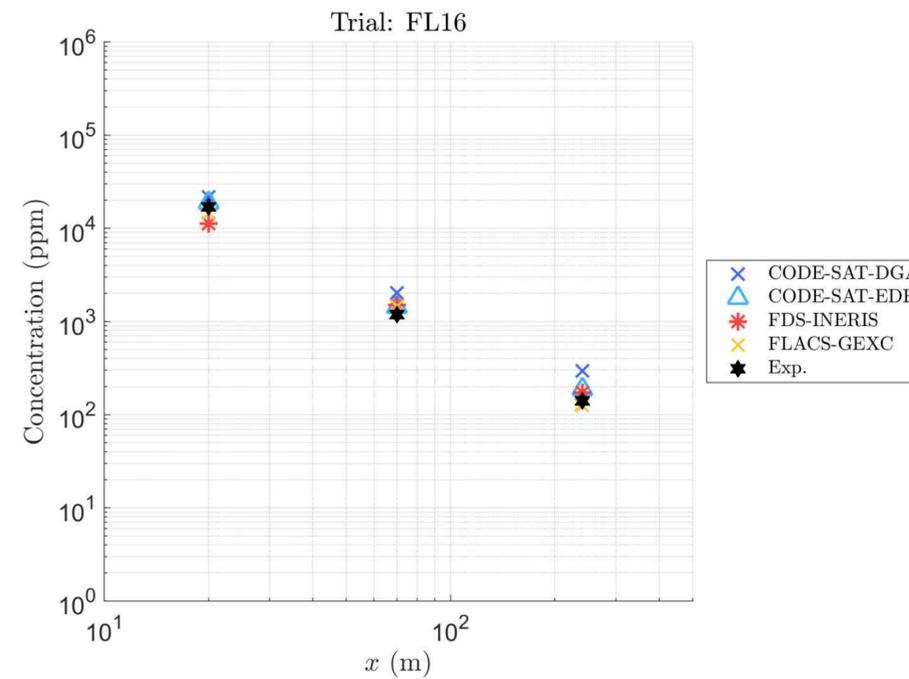
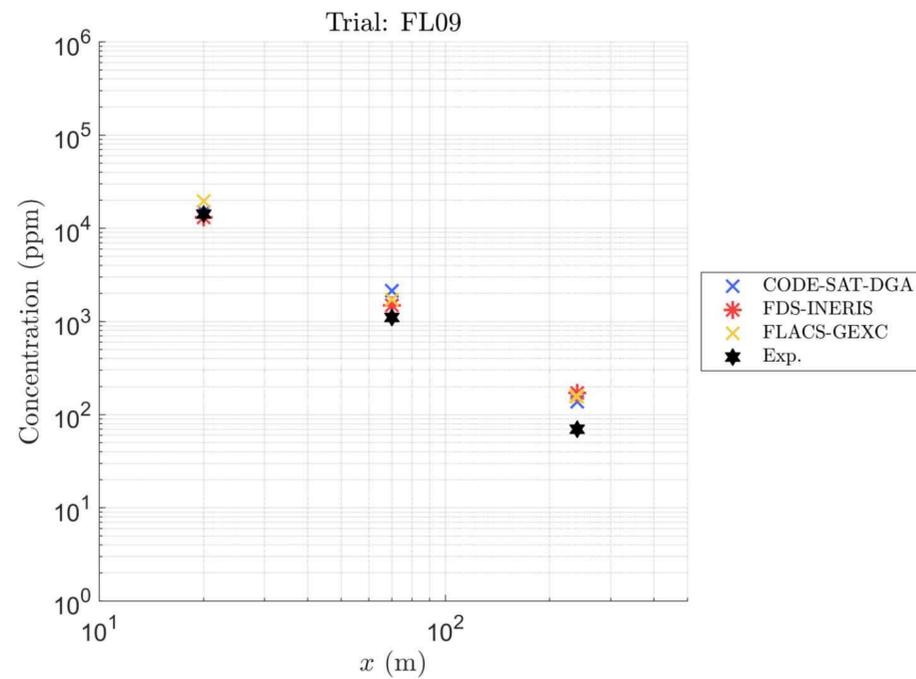
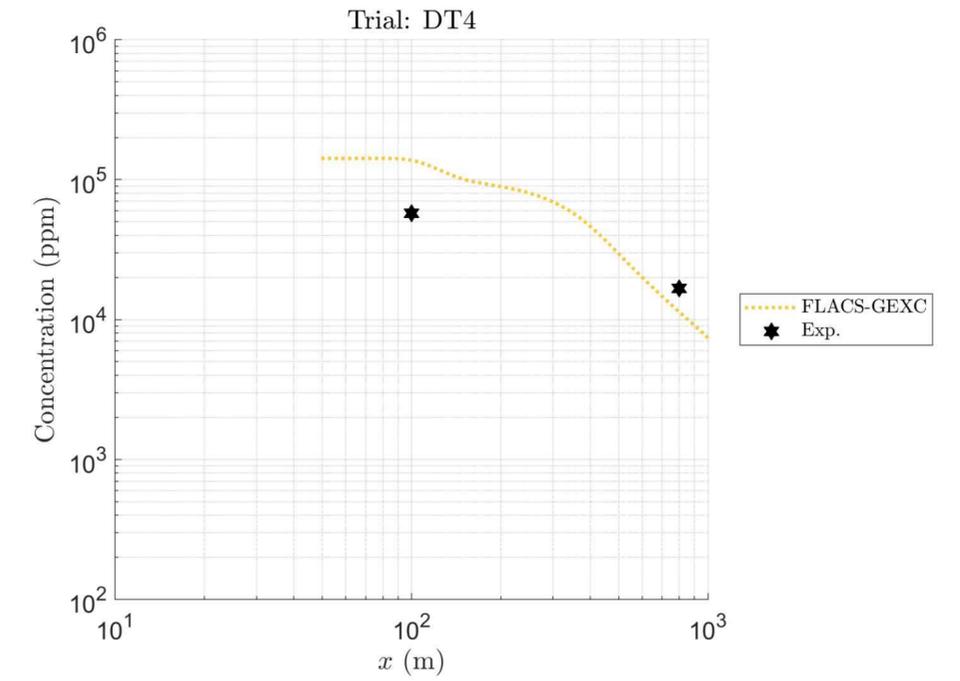
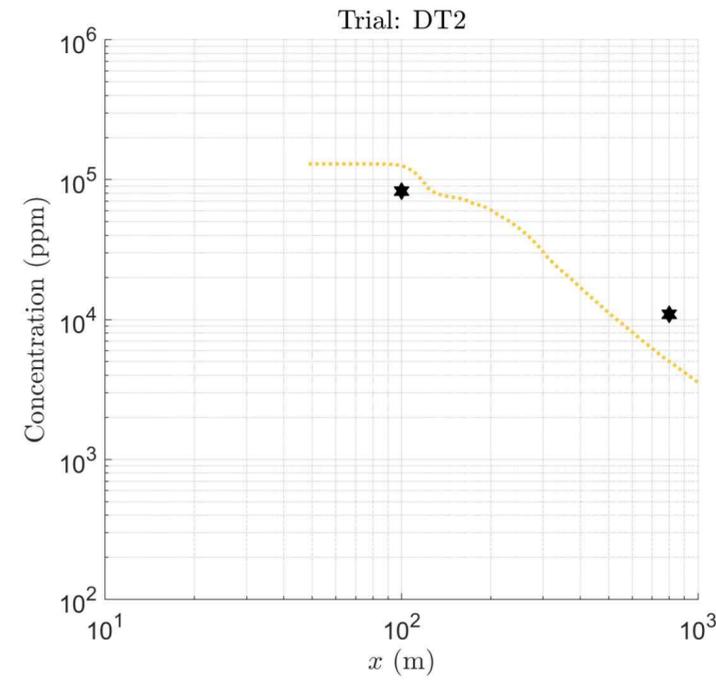
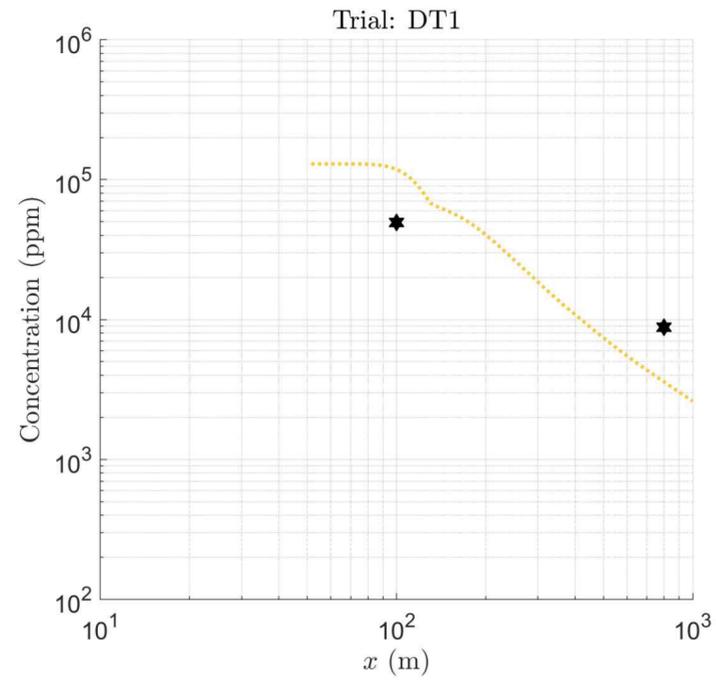
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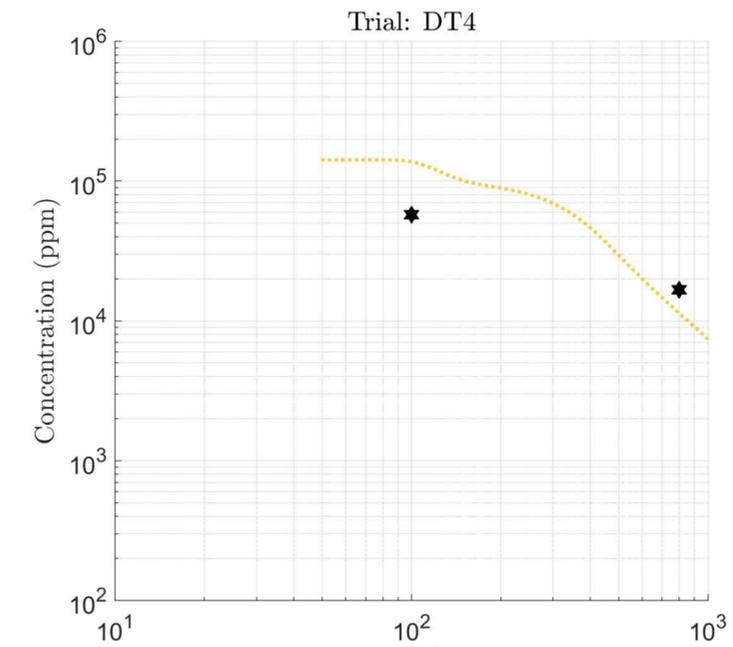
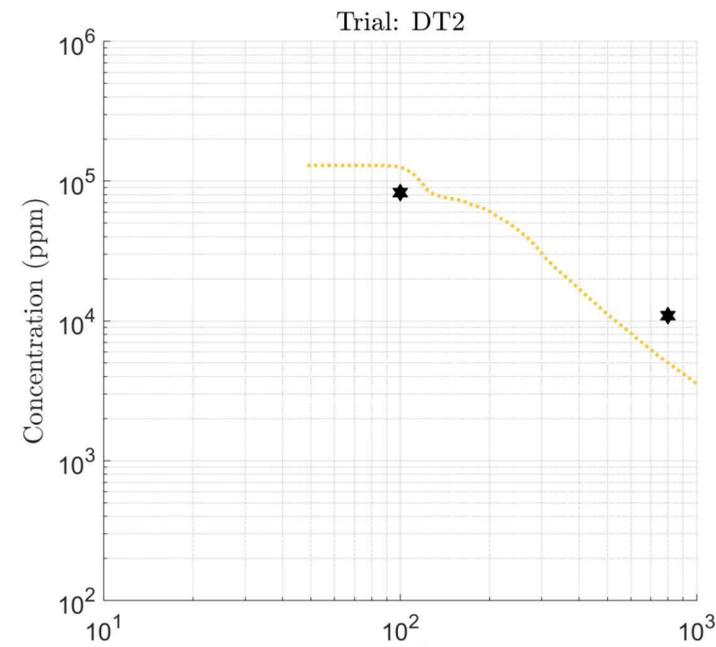
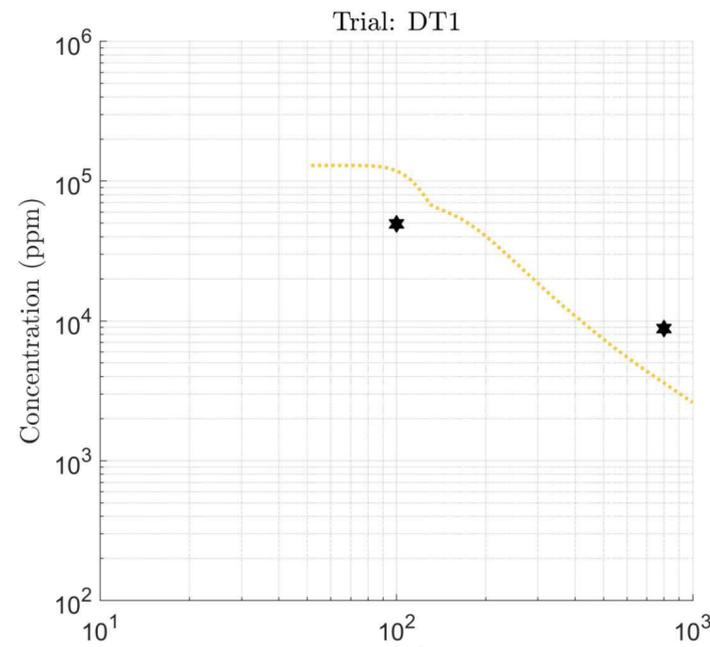
AUSTAL shows tendency to over-predict some concentrations: probably related to jet effects that are not taken into account in the Lagrangian model



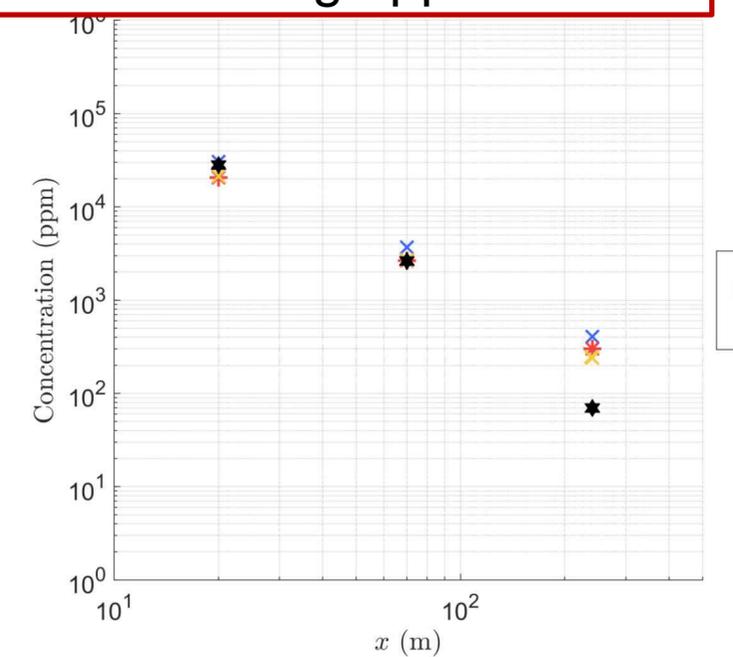
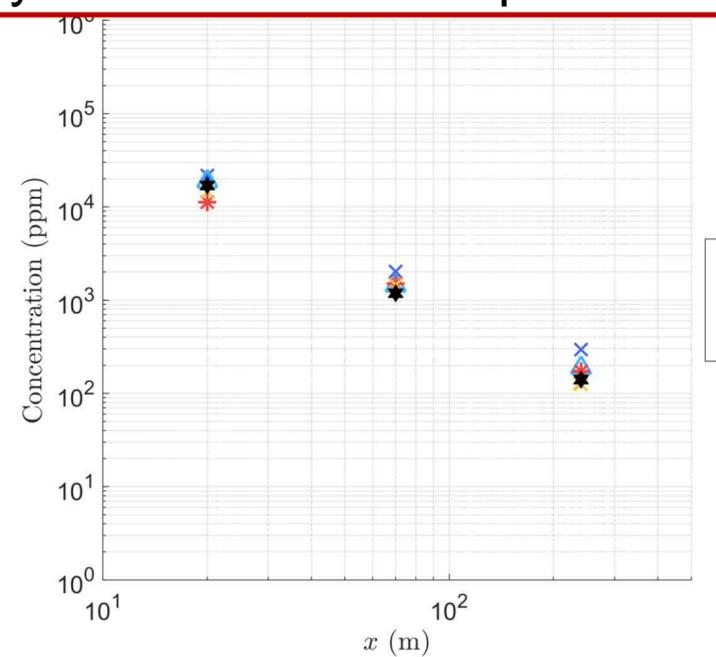
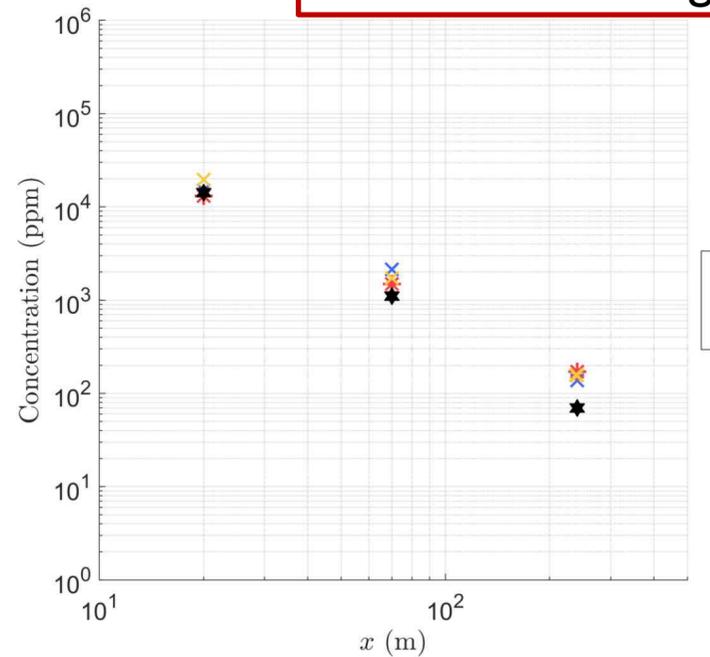
# CFD



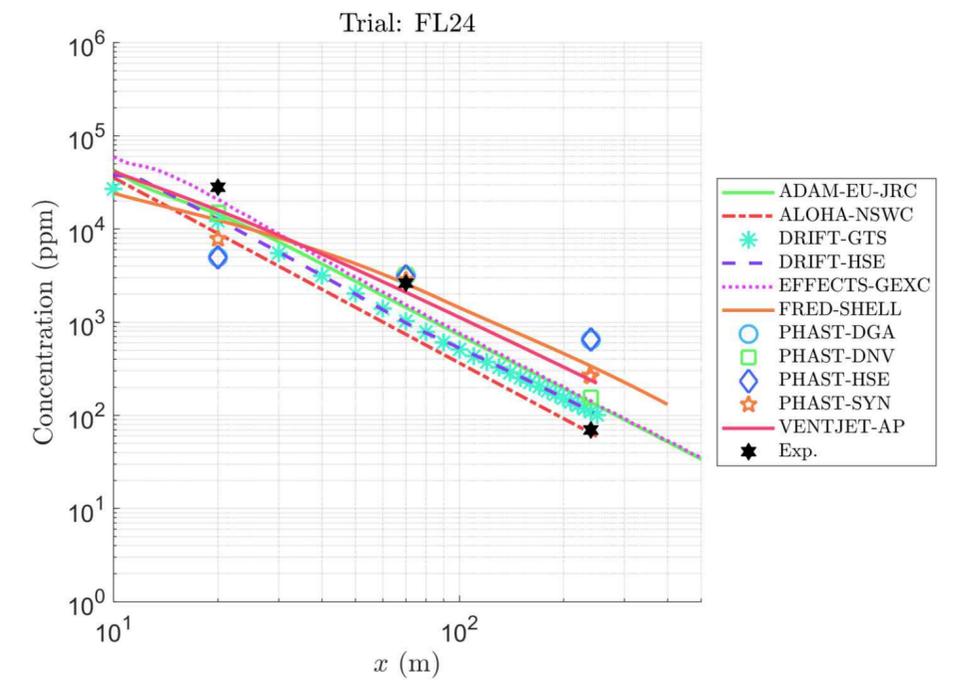
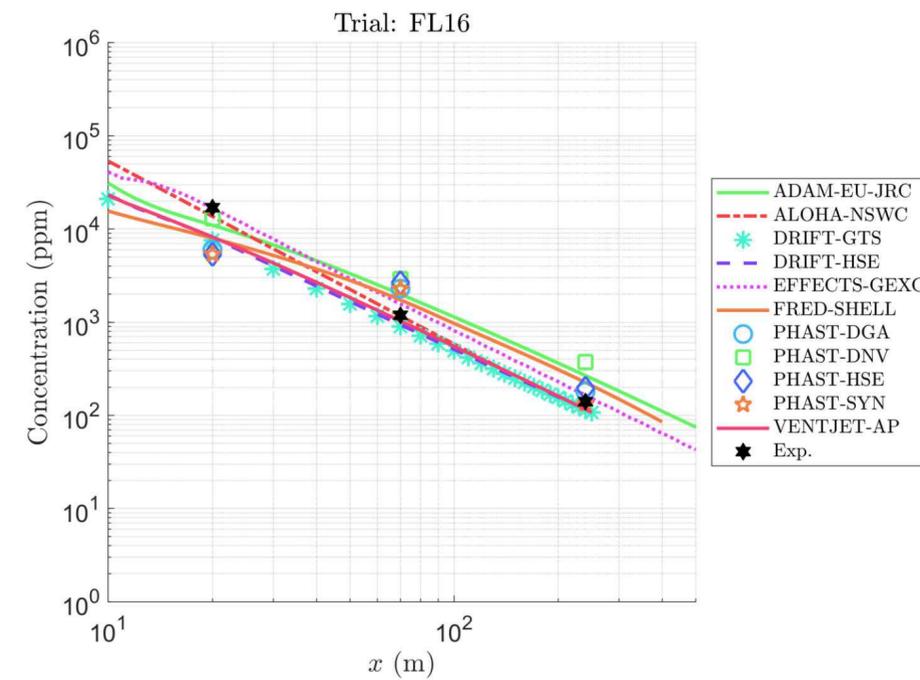
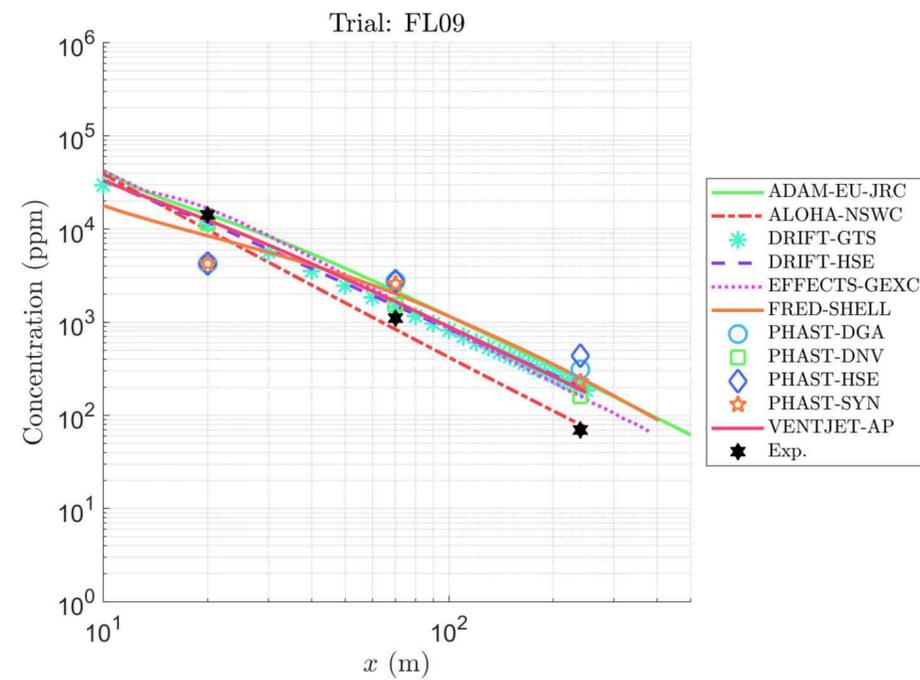
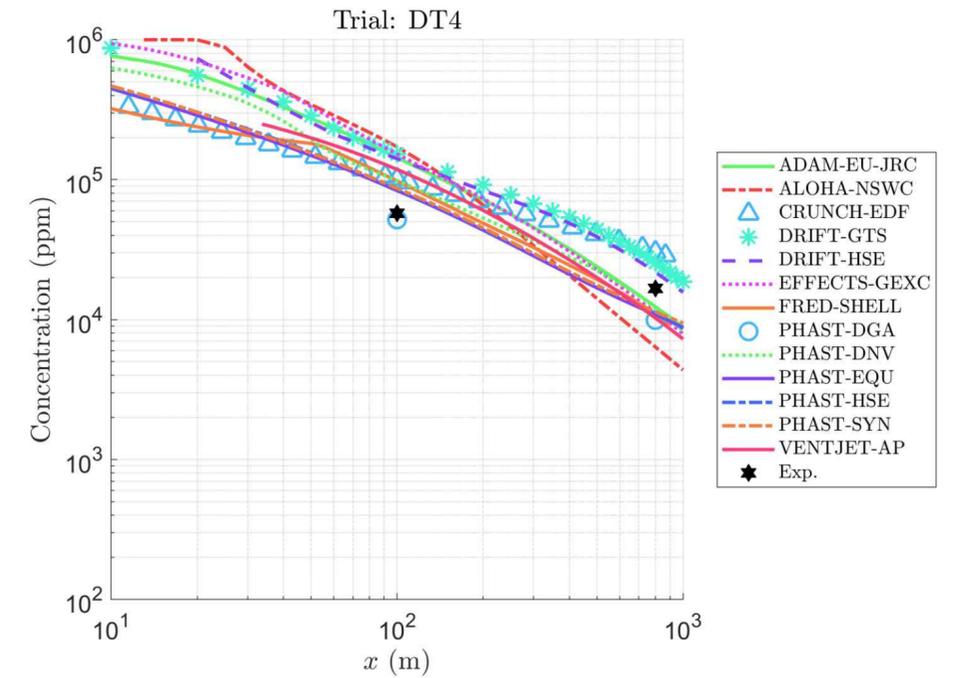
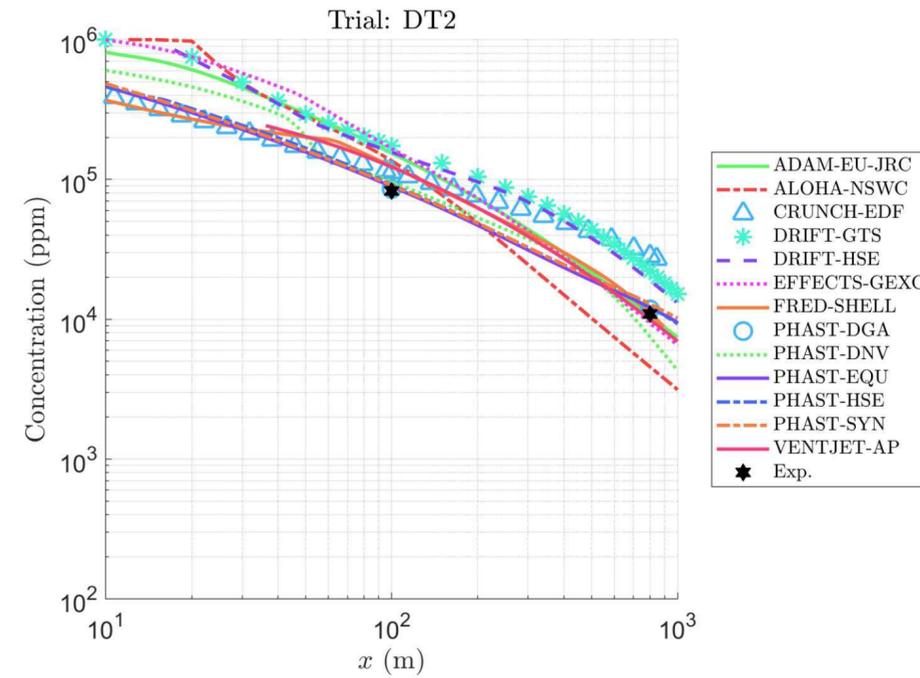
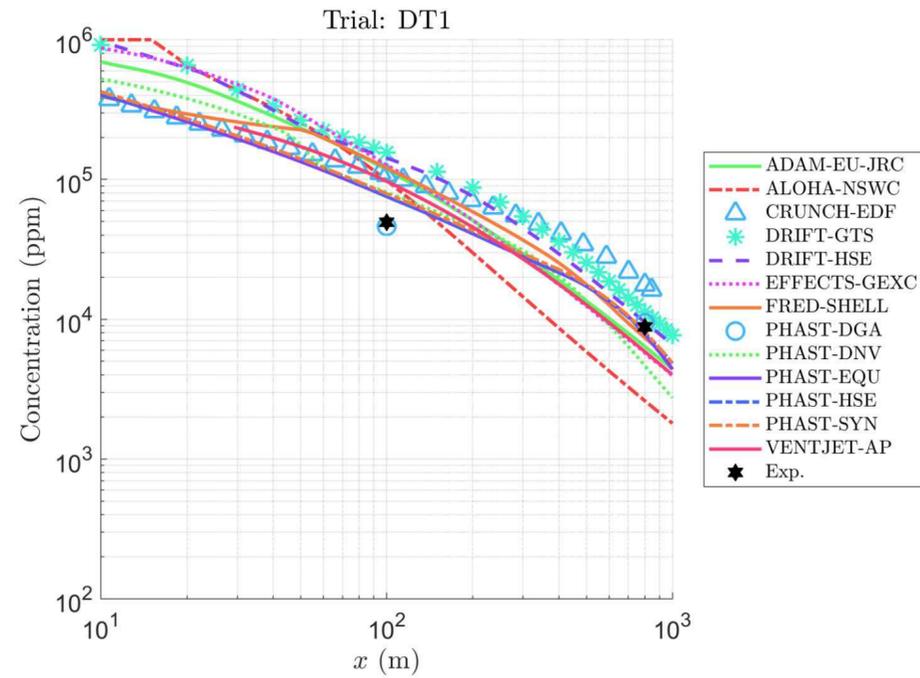
# CFD



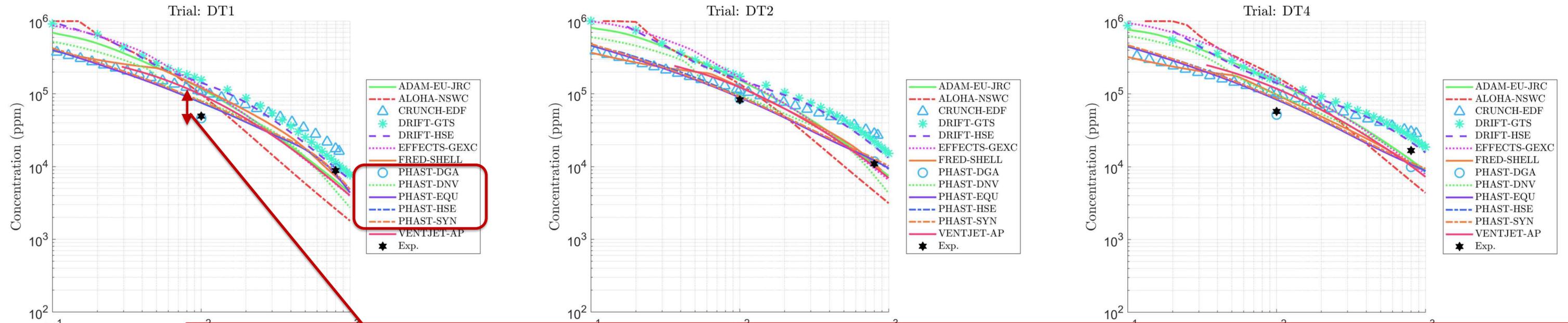
CFD models give remarkably similar results despite fundamentally different modeling approaches



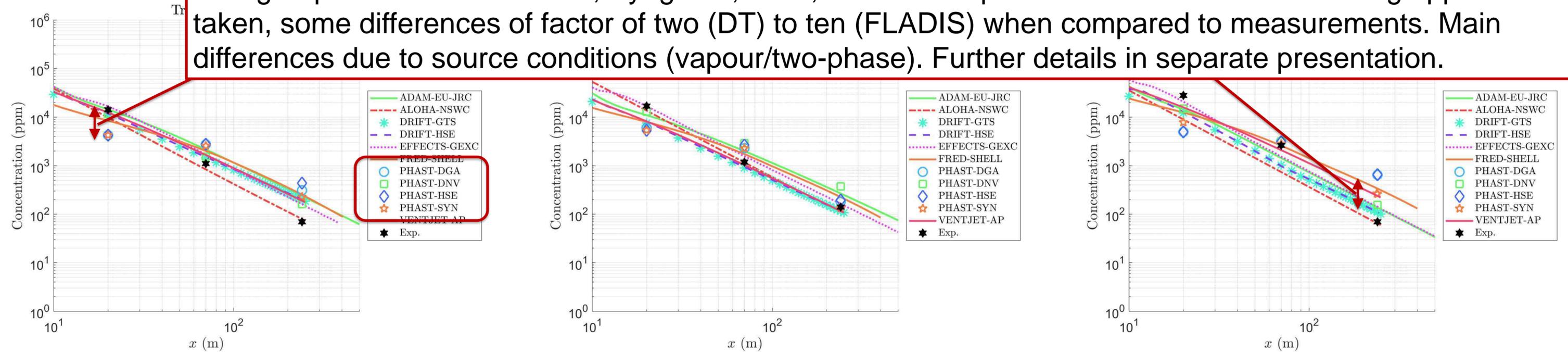
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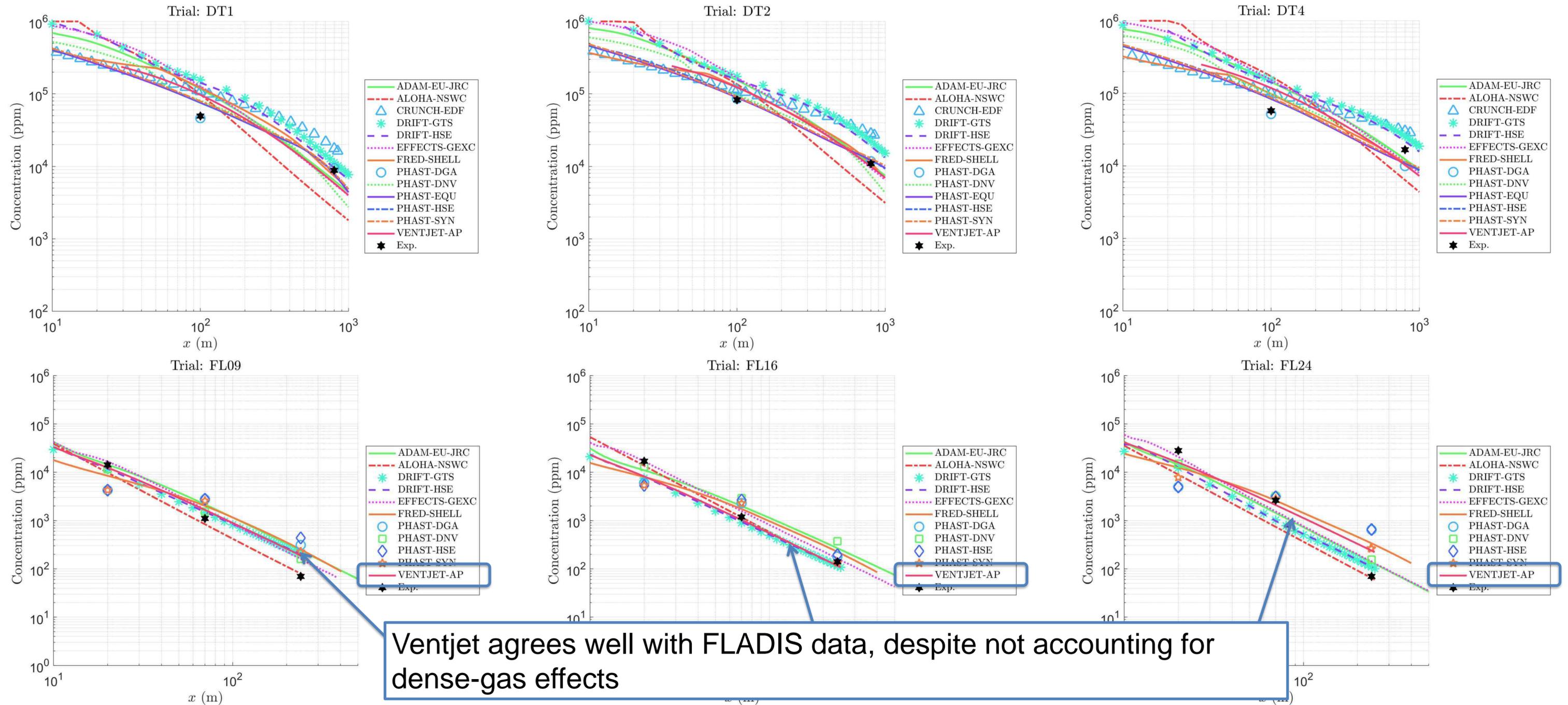
# Integral



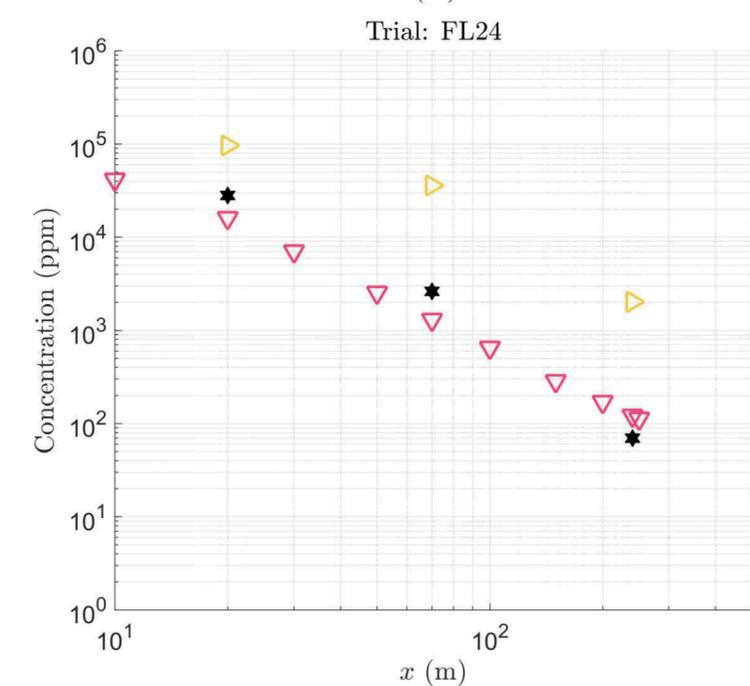
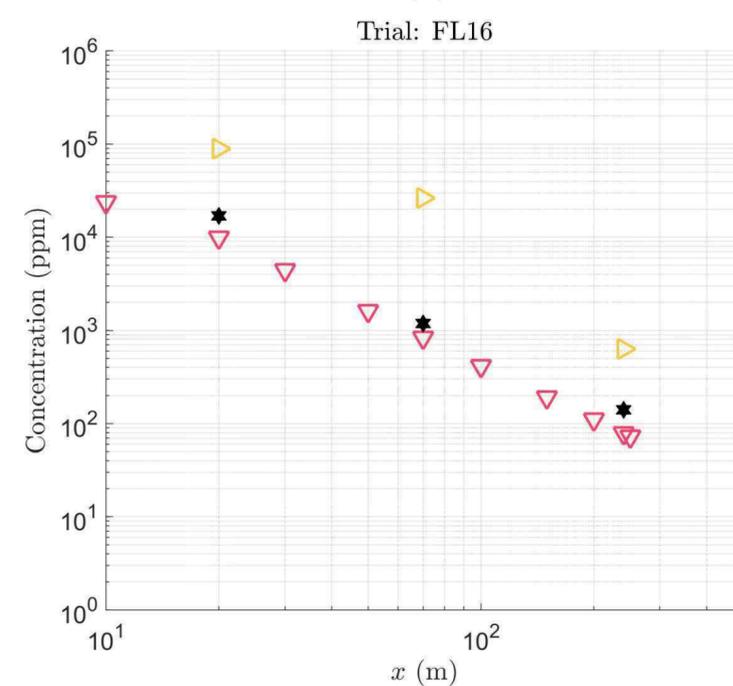
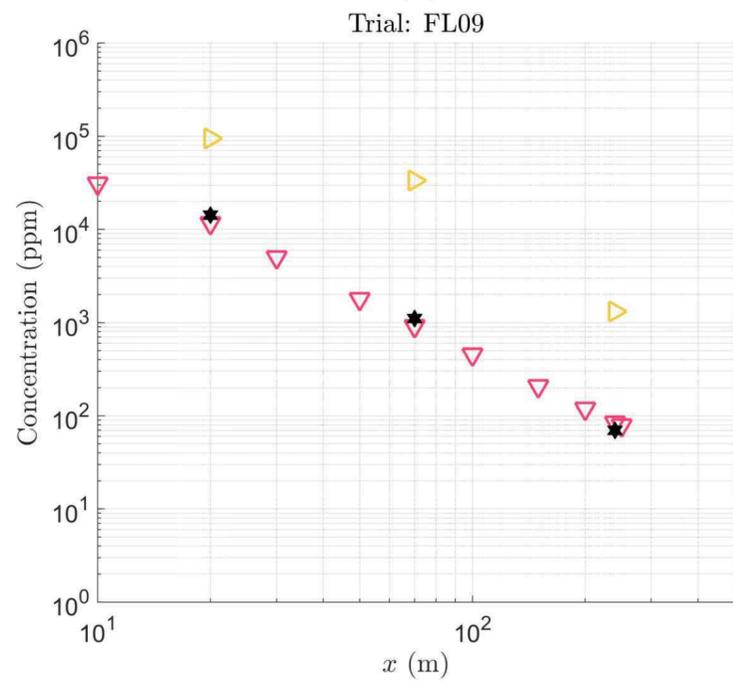
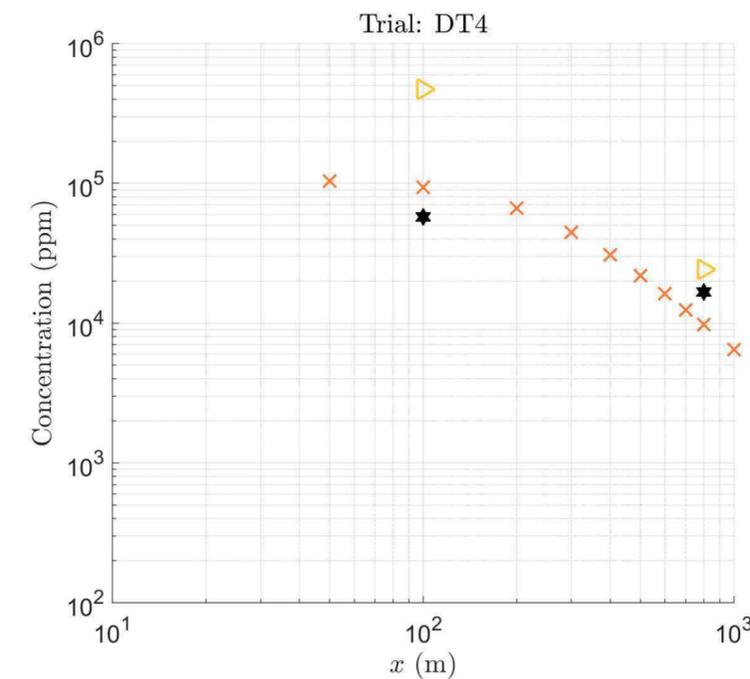
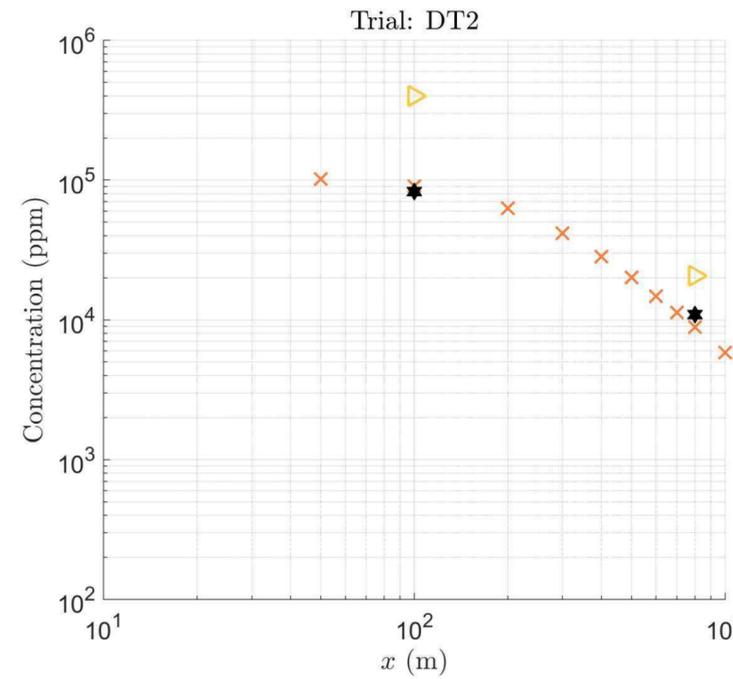
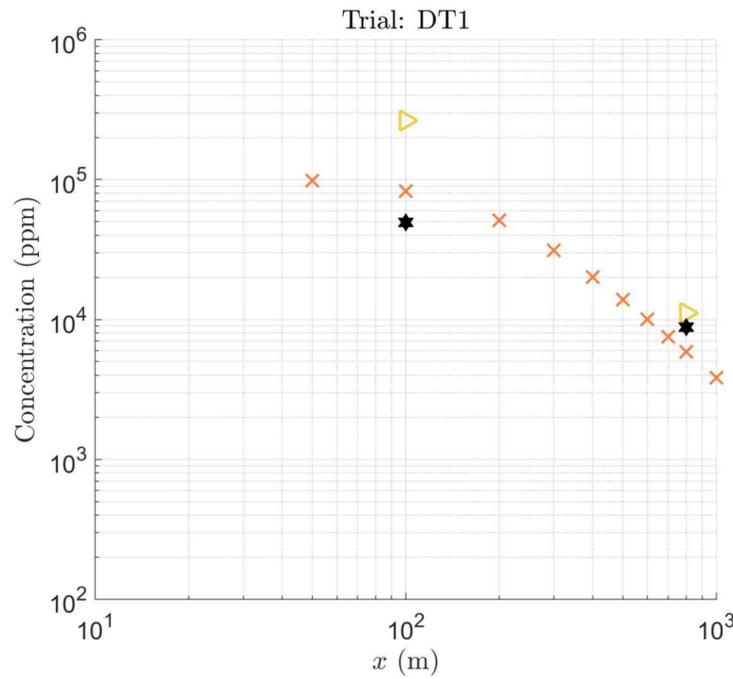
Five groups used PHAST: DNV, Syngenta, DGA, HSE and Equinor. Several different modeling approaches taken, some differences of factor of two (DT) to ten (FLADIS) when compared to measurements. Main differences due to source conditions (vapour/two-phase). Further details in separate presentation.



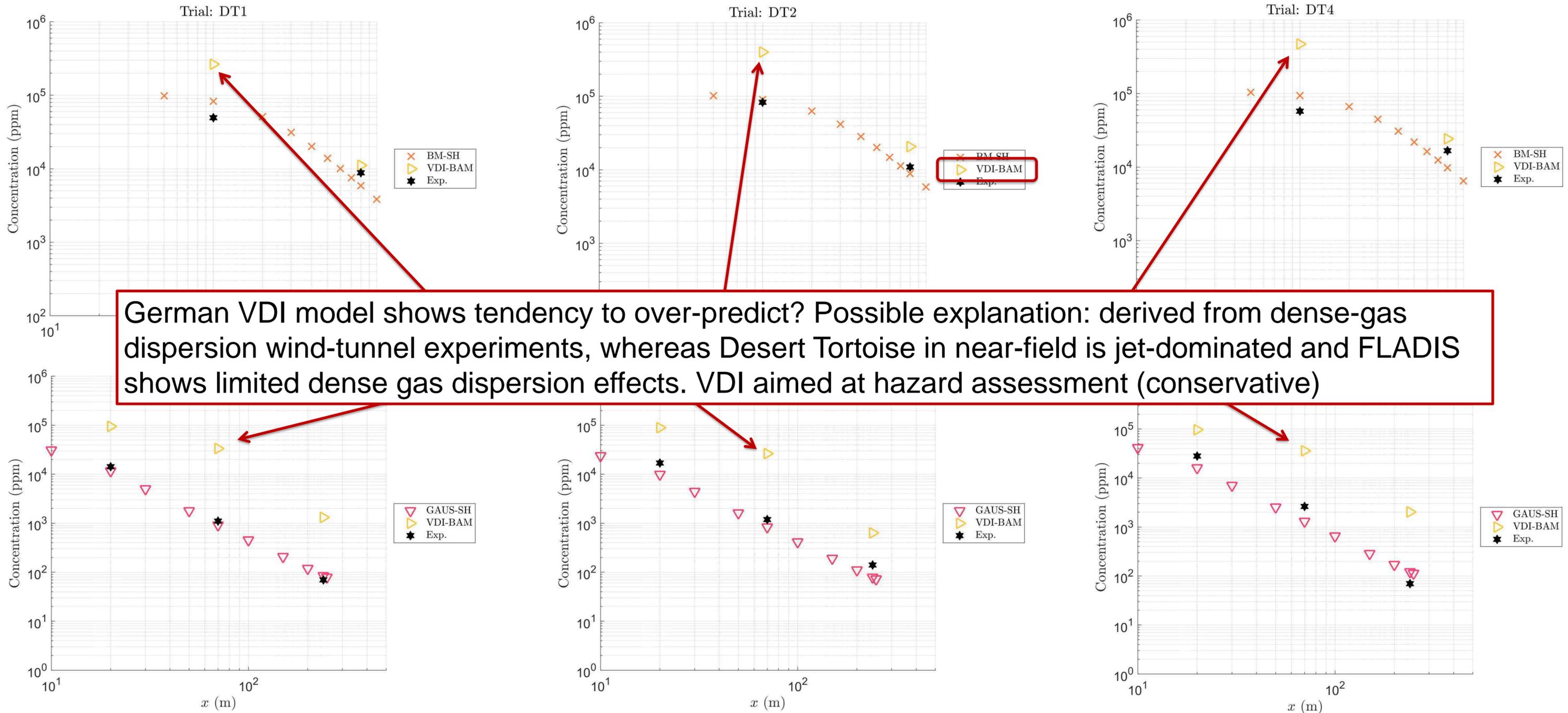
# Integral



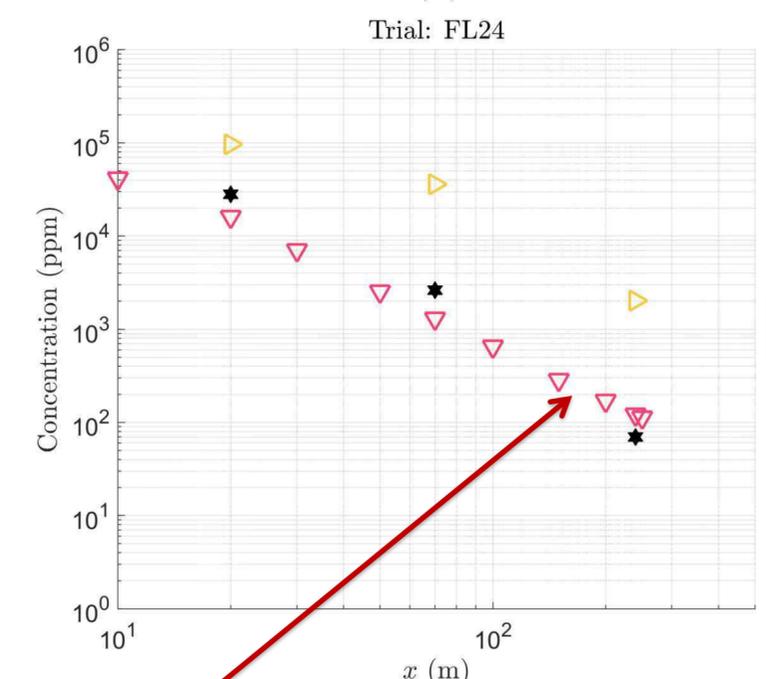
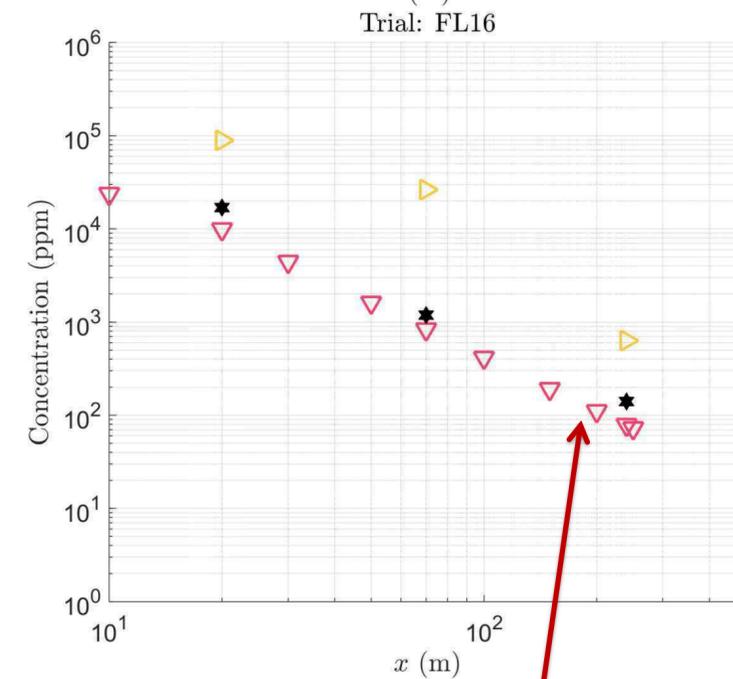
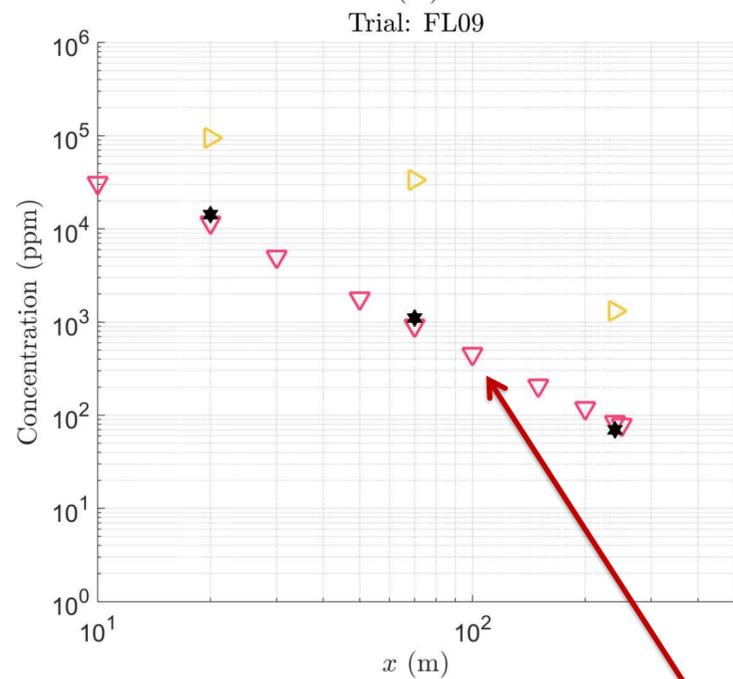
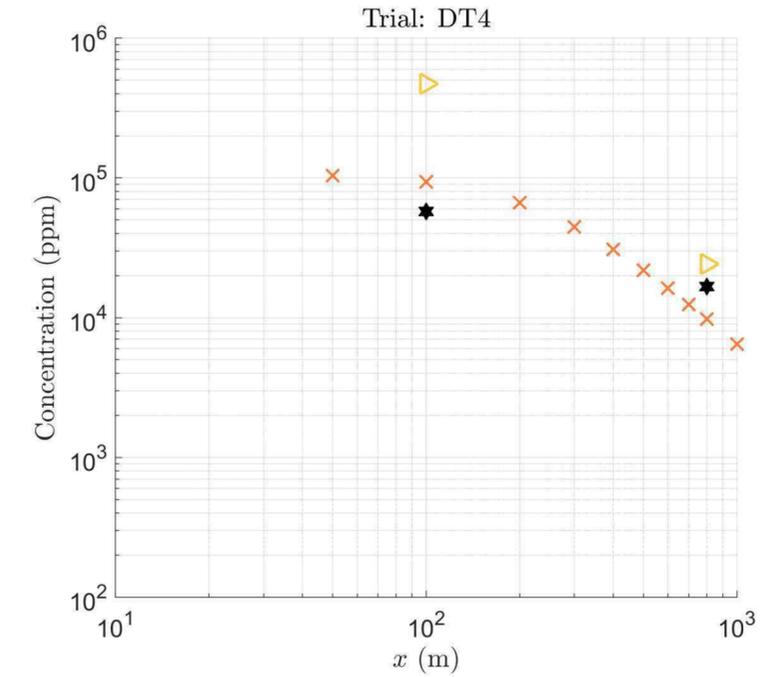
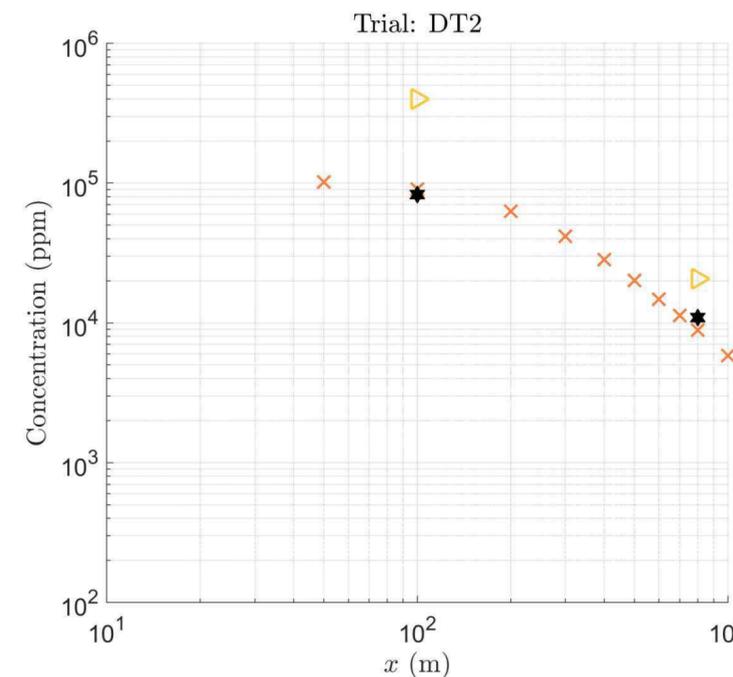
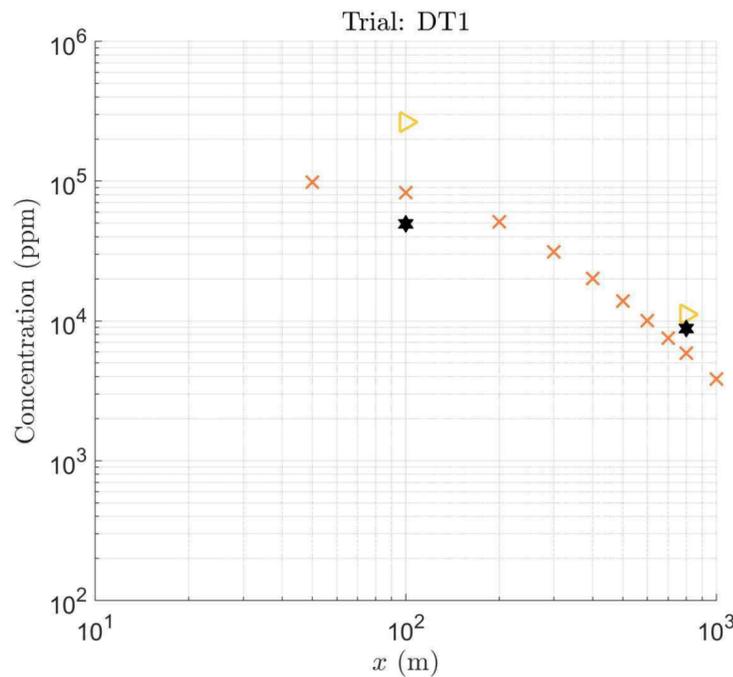
# Empirical Nomograms, Gaussian Plume



# Empirical Nomograms, Gaussian Plume

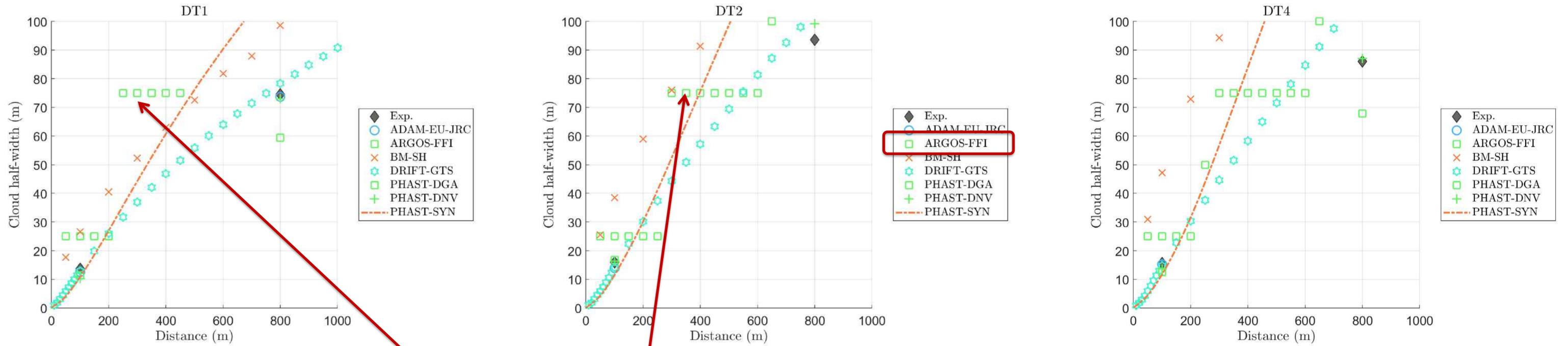


# Empirical Nomograms, Gaussian Plume

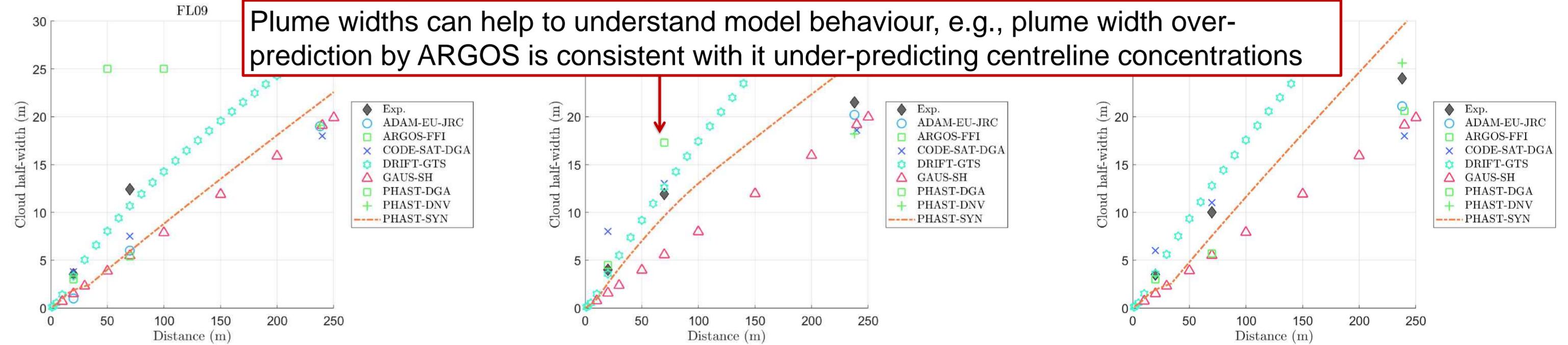


© Gaussian plume model agrees well with FLADIS data, despite not accounting for dense-gas effects

# Plume Half-Widths

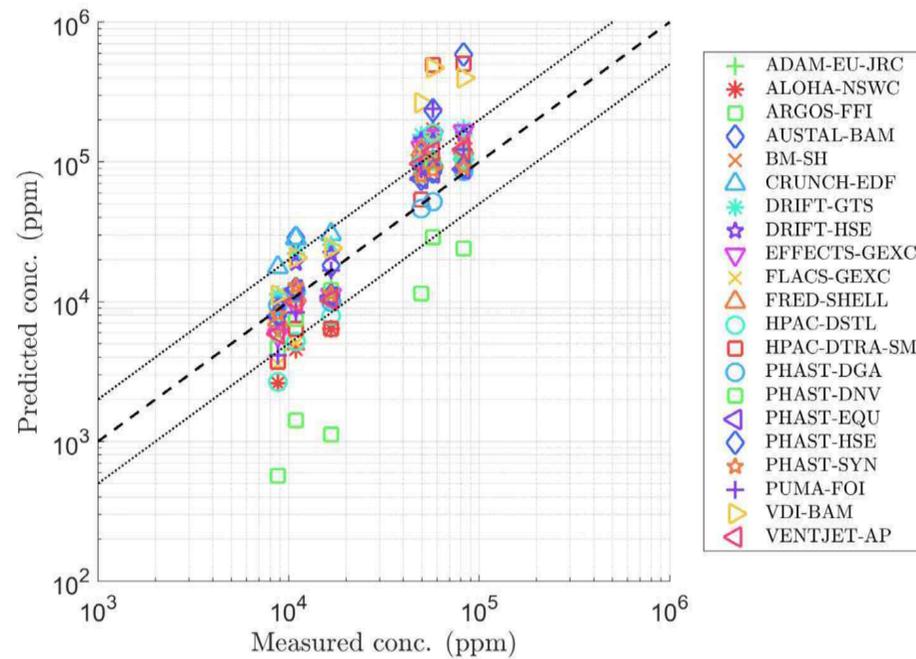


Plume widths can help to understand model behaviour, e.g., plume width over-prediction by ARGOS is consistent with it under-predicting centreline concentrations

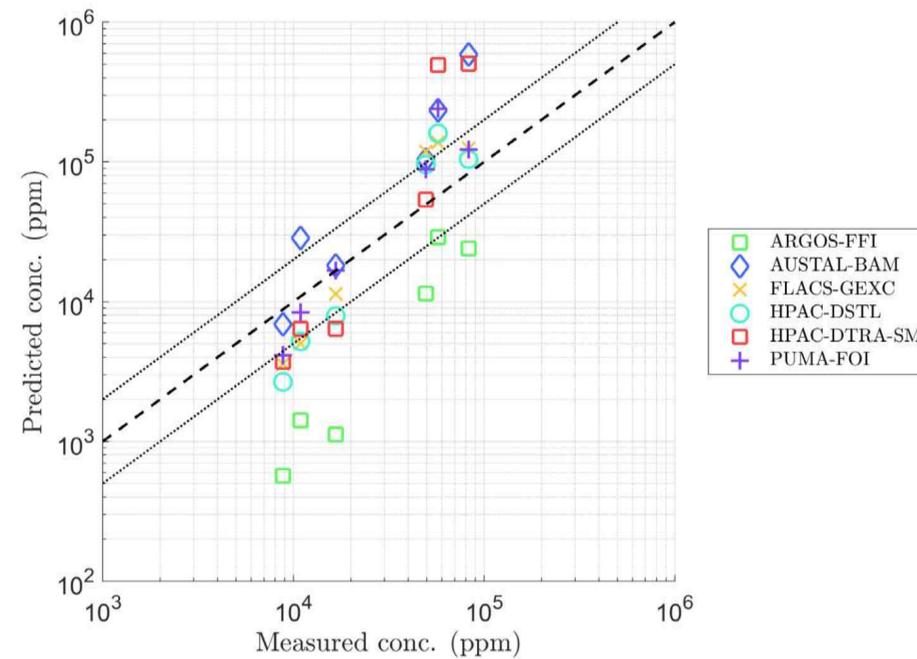


# Desert Tortoise

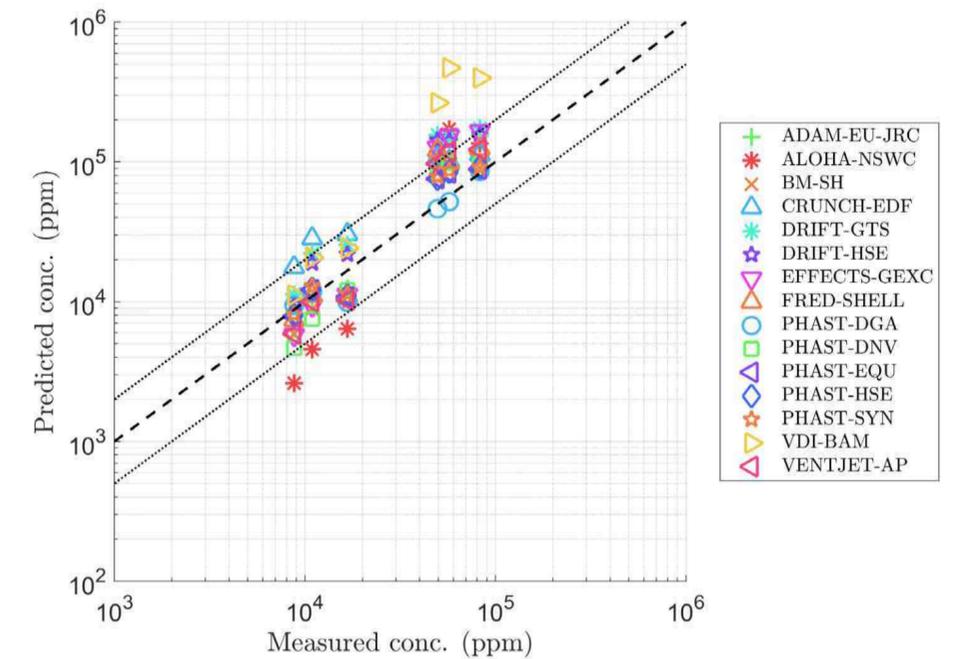
## Predicted versus Measured Centerline Concentrations



All results



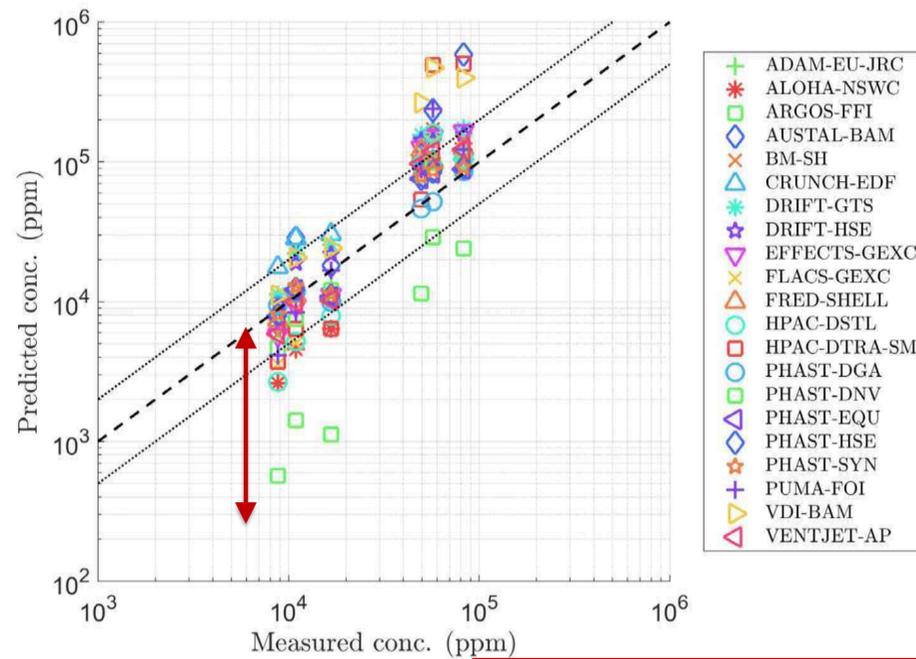
CFD, Gaussian puff,  
Lagrangian



Empirically-based  
nomograms, integral,  
Gaussian plume

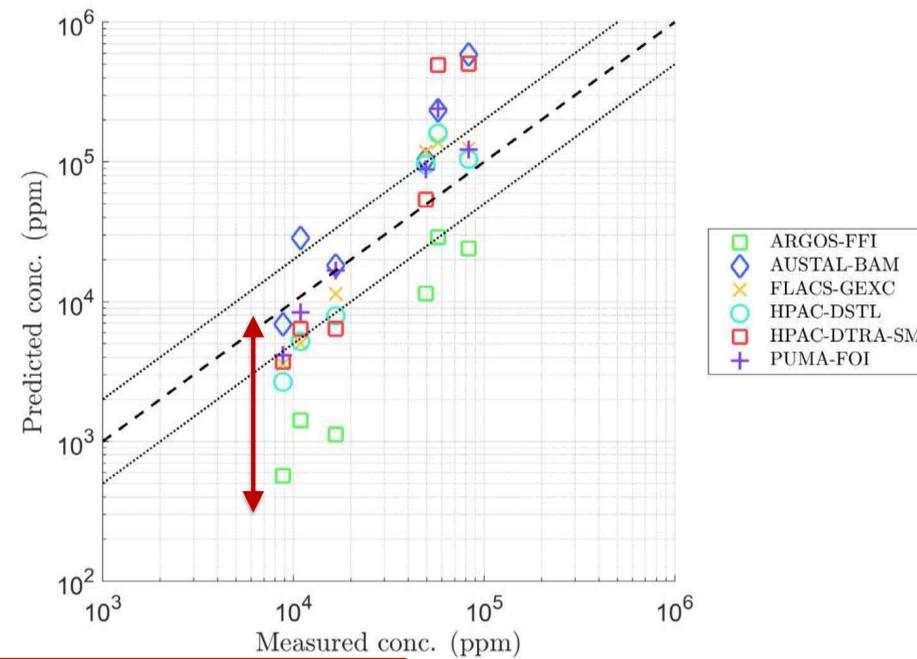
# Desert Tortoise

## Predicted versus Measured Centerline Concentrations

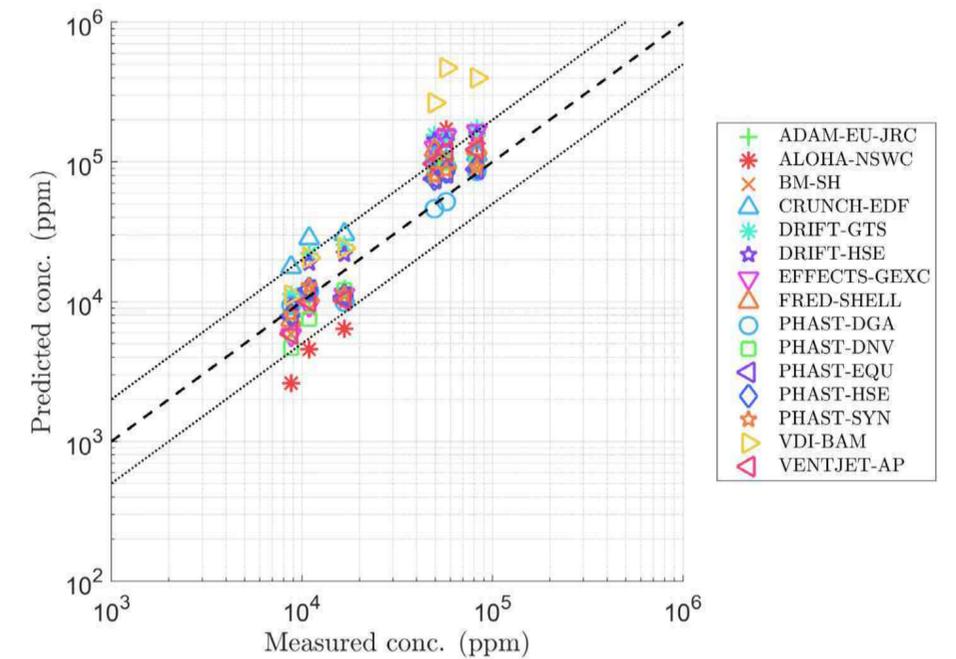


Trend towards under-predicting far field concentrations in Desert Tortoise

All results



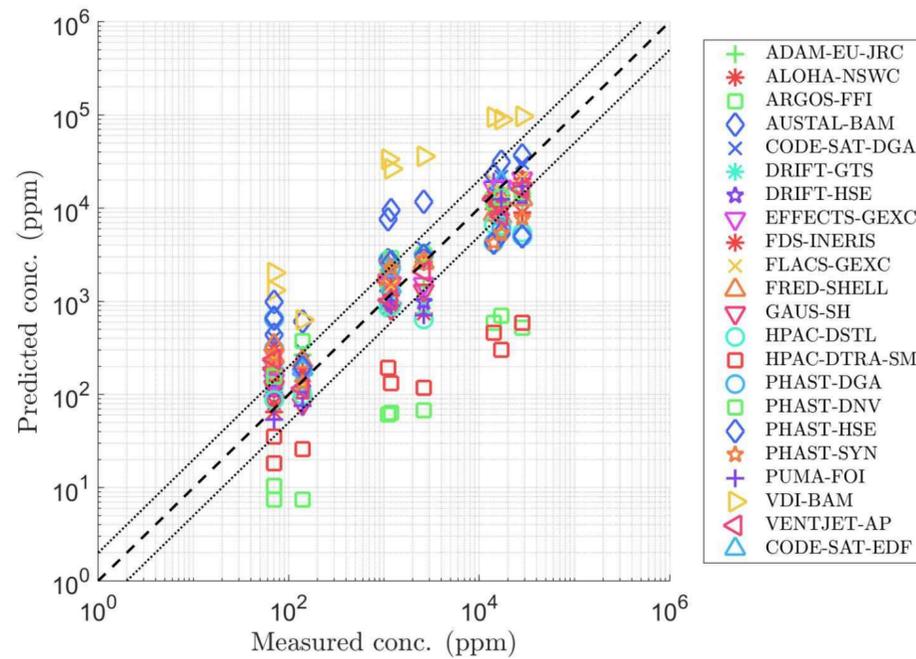
CFD, Gaussian puff,  
Lagrangian



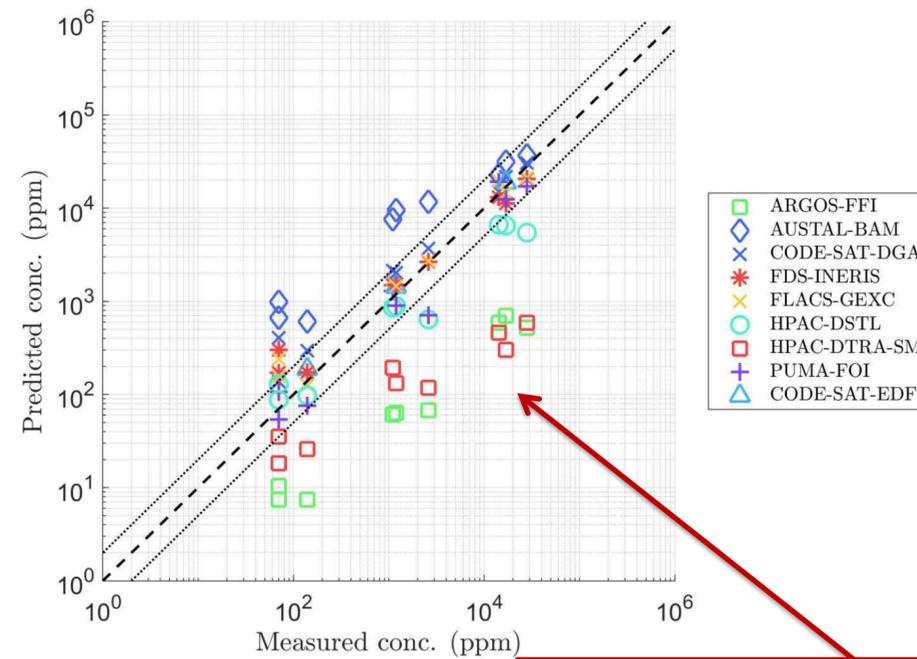
Empirically-based  
nomograms, integral,  
Gaussian plume

# FLADIS

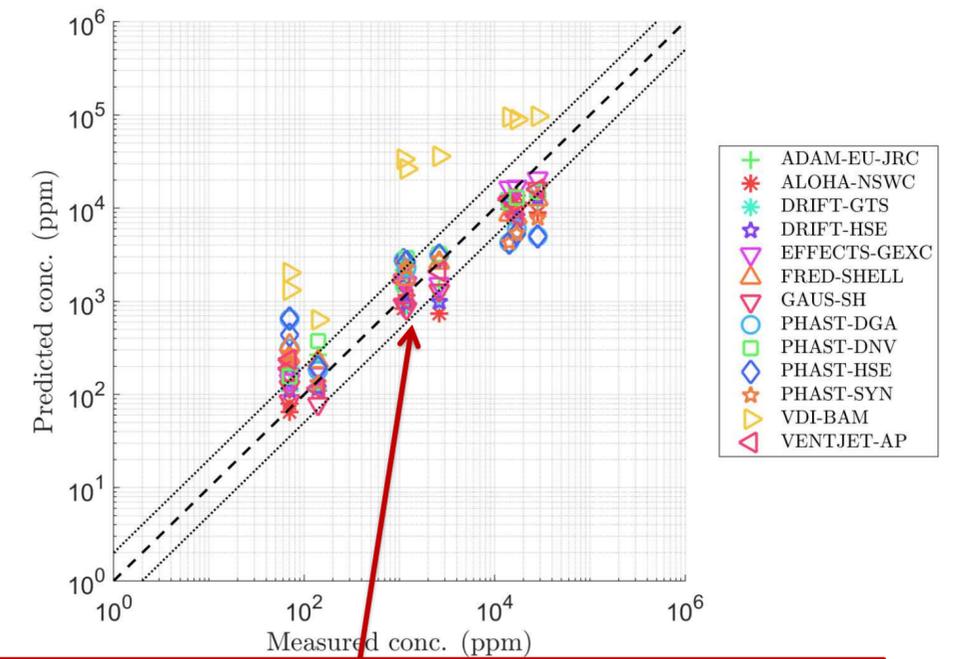
## Predicted versus Measured Centerline Concentrations



All results



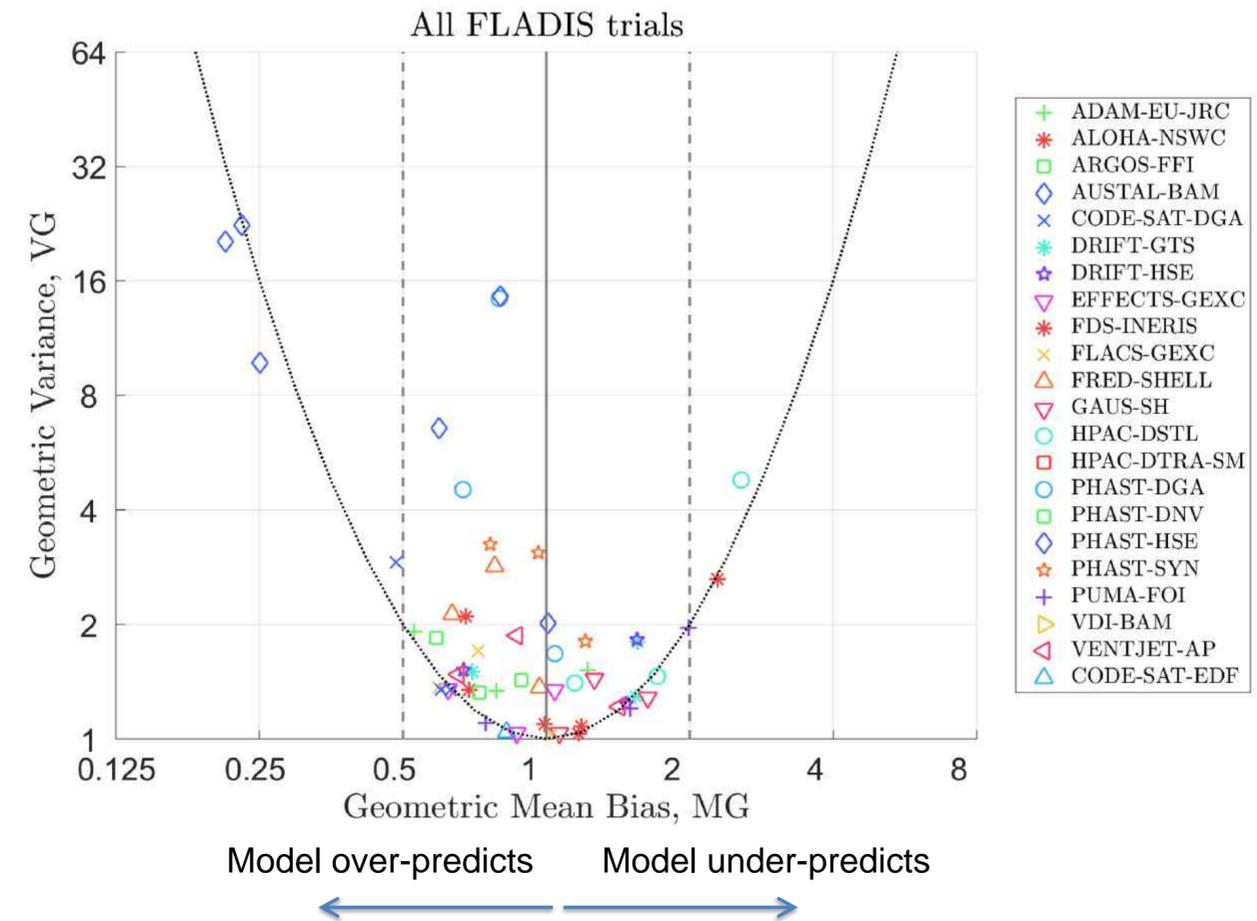
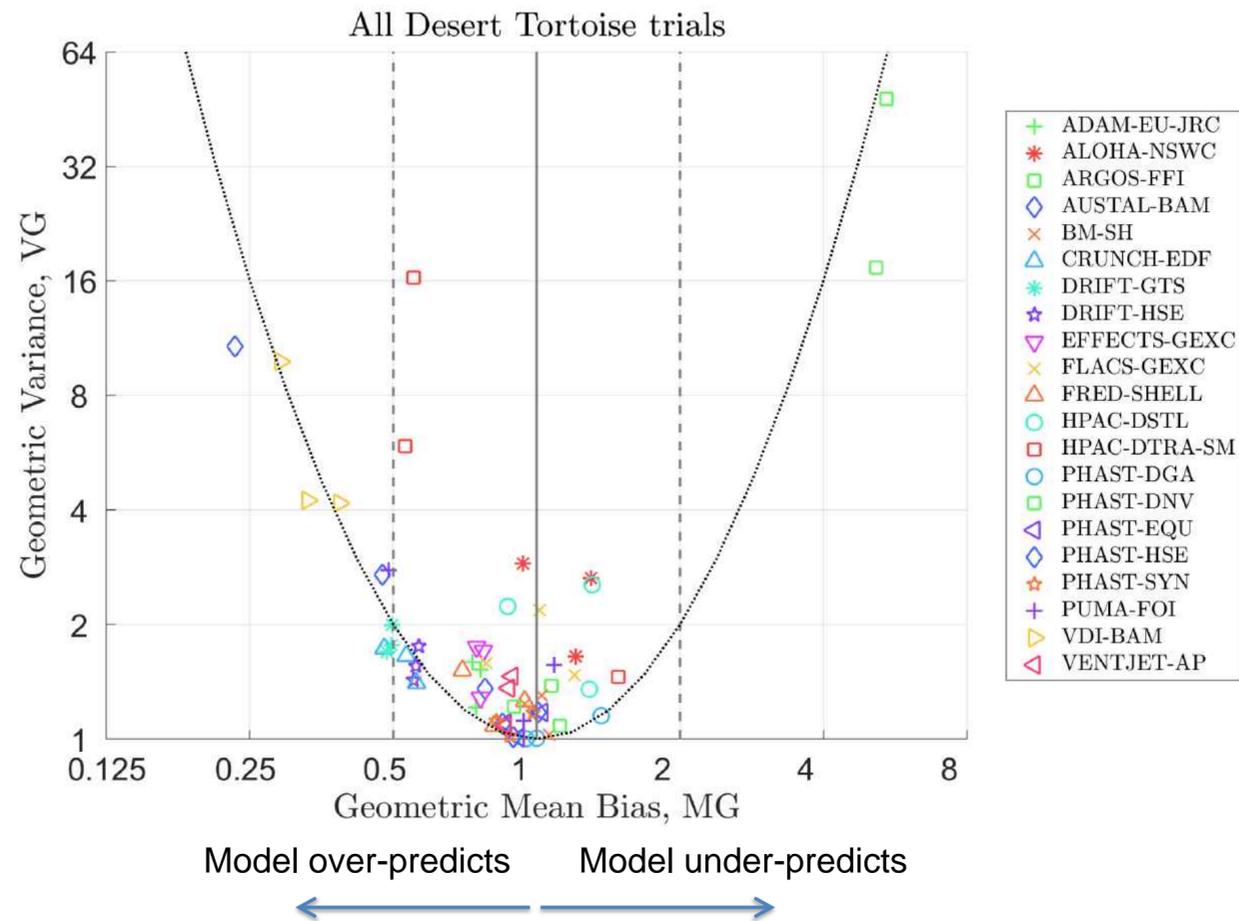
CFD, Gaussian puff,  
Lagrangian



Empirically-based  
nomograms, integral,  
Gaussian plume

Generally less scatter with nomograms/integral/Gaussian plume models, with exception of VDI model

# Geometric Mean Bias versus Geometric Variance



$$MG = \exp \left\{ \ln \left( \frac{C_m}{C_p} \right) \right\}$$

$$VG = \exp \left\{ \left[ \ln \left( \frac{C_m}{C_p} \right) \right]^2 \right\}$$

# Summary / Conclusions

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- Strong USA/UK/European support for this initial JRIII modeling exercise
  - Total of 26 sets of model predictions provided by 21 independent groups
- Agreement between model predictions and measurements varied between different models
- Useful insights gained through discussions between participants into choice of modeling approach, including discussions between different groups all using the same model
  - Experience useful for some groups in improving modeling approach going forward for JRIII
- Sensitivity tests: relatively strong impact from vapor-only source specification
  - Can we take measurements in JRIII trials to reduce this uncertainty to modeling of source conditions?
  - Further work to follow on sensitivity analysis by DSTL (including ensemble modeling)
- Modeling exercise and analysis of the Desert Tortoise and FLADIS data provided useful insights into design of the future JRIII trials, e.g.:
  - Desert Tortoise trials highlighted the need for measurements to extend further downwind to capture dense-gas/passive/buoyant(?) dispersion, i.e., full extent of hazardous cloud
  - FLADIS trials also showed that releases of this scale do not exhibit significant dense-gas effects
- Future collaborative JRIII exercise could involve modeling a previous large-scale ammonia incident

# Acknowledgements

Many thanks to all modeling groups for their valuable contributions for this exercise

## Thank you

Simon Gant<sup>1</sup>, Joseph Chang<sup>2</sup>, Sun McMasters<sup>3</sup>, Ray Jablonski<sup>3</sup>, Helen Mearns<sup>3</sup>, Shannon Fox<sup>3</sup>, Ron Meris<sup>4</sup>, Scott Bradley<sup>4</sup>, Sean Miner<sup>4</sup>, Matthew King<sup>4</sup>, Steven Hanna<sup>5</sup>, Thomas Mazzola<sup>6</sup>, Tom Spicer<sup>7</sup>, Rory Hetherington<sup>1</sup>, Alison McGillivray<sup>1</sup>, Adrian Kelsey<sup>1</sup>, Harvey Tucker<sup>1</sup>, Graham Tickle<sup>8</sup>, Oscar Björnham<sup>9</sup>, Bertrand Carissimo<sup>10</sup>, Luciano Fabbri<sup>11</sup>, Maureen Wood<sup>11</sup>, Karim Habib<sup>12</sup>, Mike Harper<sup>13</sup>, Frank Hart<sup>13</sup>, Thomas Vik<sup>14</sup>, Anders Helgeland<sup>14</sup>, Joel Howard<sup>15</sup>, Veronica Bowman<sup>15</sup>, Daniel Silk<sup>15</sup>, Lorenzo Mauri<sup>16</sup>, Shona Mackie<sup>16</sup>, Andreas Mack<sup>16</sup>, Jean-Marc Lacombe<sup>17</sup>, Stephen Puttick<sup>18</sup>, Adeel Ibrahim<sup>18</sup>, Derek Miller<sup>19</sup>, Seshu Dharmavaram<sup>19</sup>, Amy Shen<sup>19</sup>, Alyssa Cunningham<sup>20</sup>, Desiree Beverley<sup>20</sup>, Matthew O'Neal<sup>20</sup>, Laurent Verdier<sup>21</sup>, Stéphane Burkhart<sup>21</sup>, Chris Dixon<sup>22</sup>, Sandra Nilsen<sup>23</sup>

<sup>1</sup>RAND Corporation, <sup>2</sup>Health and Safety Executive (HSE), <sup>3</sup>Chemical Security Analysis Center (CSAC), Department of Homeland Security (DHS), <sup>4</sup>Defense Threat Reduction Agency (DTRA), <sup>5</sup>Hanna Consultants, Inc., <sup>6</sup>Systems Planning and Analysis, Inc. (SPA), <sup>7</sup>University of Arkansas, <sup>8</sup>GT Science and Software, <sup>9</sup>Swedish Defence Research Agency (FOI), <sup>10</sup>EDF/Ecole des Ponts, <sup>11</sup>European Joint Research Centre (JRC), <sup>12</sup>Bundesanstalt für Materialforschung und -prüfung (BAM), <sup>13</sup>DNV, Stockport, <sup>14</sup>Norwegian Defence Research Establishment (FFI), <sup>15</sup>Defence Science and Technology Laboratory (DSTL), <sup>16</sup>Gexcon, <sup>17</sup>Institut National de l'Environnement Industriel et des Risques (INERIS), <sup>18</sup>Syngenta, <sup>19</sup>Air Products, <sup>20</sup>Naval Surface Warfare Center (NSWC), <sup>21</sup>Direction Générale de l'Armement (DGA), <sup>22</sup>Shell, <sup>23</sup>Equinor

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# Predicted vs Measured Centerline Concentrations

| Baseline Model    | DT1          |             | DT2          |              | DT4          |              | FLADIS9      |             |           | FLADIS16     |             |            | FLADIS24     |             |           |
|-------------------|--------------|-------------|--------------|--------------|--------------|--------------|--------------|-------------|-----------|--------------|-------------|------------|--------------|-------------|-----------|
|                   | 100m         | 800m        | 100m         | 800m         | 100m         | 800m         | 20m          | 70m         | 238m      | 20m          | 70m         | 238m       | 20m          | 70m         | 238m      |
| ADAM-EU-JRC       | 117112       | 6384        | 154475       | 10553        | 143547       | 12351        | 14411        | 2157        | 238       | 10990        | 1996        | 267        | 14404        | 1437        | 137       |
| ALOHA-NSWC        | 98384        | 2609        | 136035       | 4569         | 171313       | 6370         | 9841         | 837         | 80        | 13690        | 1165        | 111        | 8974         | 740         | 65        |
| ARGOS-FFI         | 11447        | 569         | 23940        | 1417         | 28937        | 1123         | 587          | 61          | 7         | 702          | 63          | 7          | 517          | 68          | 10        |
| AUSTAL-BAM        | 104000       | 6886        | 586000       | 28600        | 234000       | 18100        | 22600        | 7600        | 667       | 31300        | 9470        | 608        | 36800        | 11700       | 988       |
| CODE-SAT-DGA      | -            | -           | -            | -            | -            | -            | 14989        | 2125        | 138       | 21800        | 2034        | 294        | 30558        | 3691        | 405       |
| CODE-SAT-EDF      | -            | -           | -            | -            | -            | -            | -            | -           | -         | 18765        | 1433        | 188        | -            | -           | -         |
| BM-SH             | 82865        | 5877        | 90638        | 8859         | 93336        | 9749         | -            | -           | -         | -            | -           | -          | -            | -           | -         |
| CRUNCH-EDF        | 107680       | 17672       | 112747       | 28378        | 100798       | 30313        | -            | -           | -         | -            | -           | -          | -            | -           | -         |
| DRIFT-GTS         | 155947       | 11319       | 174294       | 22120        | 152100       | 25615        | 11187        | 1443        | 199       | 7579         | 894         | 115        | 12195        | 1028        | 109       |
| DRIFT-HSE         | 142405       | 9534        | 156941       | 18926        | 141061       | 21770        | 11912        | 1508        | 202       | 8104         | 938         | 117        | 12689        | 983         | 111       |
| EFFECTS-GEXC      | 126894       | 5746        | 165882       | 9398         | 152307       | 11193        | 16658        | 1680        | 162       | 16868        | 1566        | 165        | 20835        | 1530        | 143       |
| FDS-INERIS        | -            | -           | -            | -            | -            | -            | 13144        | 1486        | 171       | 11207        | 1506        | 172        | 20700        | 2650        | 301       |
| FLACS-GEXC        | 118013       | 3584        | 125254       | 5011         | 137370       | 11323        | 19499        | 1722        | 155       | 14470        | 1453        | 126        | 21359        | 2695        | 240       |
| GAUS-SH           |              |             |              |              |              |              | 11668        | 915         | 85        | 9895         | 833         | 79         | 16169        | 1305        | 122       |
| HPAC-DSTL         | 95614        | 2657        | 104598       | 5186         | 159609       | 7915         | 6622         | 851         | 129       | 6498         | 890         | 98         | 5463         | 642         | 87        |
| HPAC-DTRA-SM      | 53559        | 3700        | 504253       | 6399         | 495409       | 6358         | 458          | 194         | 35        | 300          | 132         | 26         | 590          | 118         | 18        |
| PHAST-DGA         | 46096        | 9419        | 85734        | 11740        | 51786        | 9898         | 4256         | 2766        | 311       | 6069         | 2287        | 180        | 4967         | 3158        | 648       |
| PHAST-DNV         | 80899        | 4654        | 96505        | 7501         | 98310        | 12113        | 11592        | 1541        | 161       | 12916        | 2917        | 372        | 14947        | 3186        | 155       |
| PHAST-HSE         | 75588        | 8007        | 91726        | 12332        | 85144        | 11056        | 4268         | 2765        | 437       | 5327         | 2652        | 196        | 4959         | 3108        | 653       |
| PHAST-SYN         | 78982        | 8117        | 90870        | 12853        | 86736        | 11374        | 4266         | 2556        | 227       | 5324         | 2281        | 132        | 4962         | 2728        | 256       |
| PUMA-FOI          | 88366        | 4147        | 122102       | 8386         | 239535       | 16667        | 19252        | 1290        | 106       | 12378        | 898         | 76         | 17121        | 707         | 54        |
| VDI-BAM           | 264000       | 11100       | 400000       | 20700        | 470000       | 24200        | 94800        | 33300       | 1309      | 88900        | 26500       | 629        | 96700        | 36000       | 2030      |
| VENTJET-AP        | 96962        | 5865        | 122778       | 9952         | 118191       | 10257        | 12476        | 1657        | 189       | 8224         | 1030        | 116        | 15918        | 2092        | 238       |
| <b>Experiment</b> | <b>49490</b> | <b>8790</b> | <b>82920</b> | <b>10910</b> | <b>57300</b> | <b>16678</b> | <b>14190</b> | <b>1100</b> | <b>70</b> | <b>17010</b> | <b>1190</b> | <b>140</b> | <b>28180</b> | <b>2610</b> | <b>70</b> |

# Sensitivity Tests

- Aim: to understand potential impact of experimental uncertainties and modeling options
- Suggestions given in model exercise specification documents:

1.) Standing water at the Frenchman Flats test site in Desert Tortoise trials DT1 and DT2

|                          |                  | DT1  | DT2  |
|--------------------------|------------------|------|------|
| Relative humidity (%)    | Baseline         | 13.2 | 17.5 |
|                          | Sensitivity test | 50   | 50   |
| Monin-Obukhov length (m) | Baseline         | 92.7 | 94.7 |
|                          | Sensitivity test | -20  | -20  |
| Pasquill stability class | Baseline         | D    | D    |
|                          | Sensitivity test | C    | C    |

2.) Wind speed variability in DT4

|                               |                  | DT4  |
|-------------------------------|------------------|------|
| Site average wind speed (m/s) | Baseline         | 4.51 |
|                               | Sensitivity test | 3.0  |

3.) Ammonia liquid rainout in the Desert Tortoise trials

- For models that have the capability to simulate a fixed fraction of liquid raining out from the jet and depositing to form an evaporating pool on the ground:

|                           |                        | DT1 | DT2 | DT4 |
|---------------------------|------------------------|-----|-----|-----|
| Rainout mass fraction (%) | Baseline               | 5   | 5   | 5   |
|                           | Sensitivity test (min) | 0   | 0   | 0   |
|                           | Sensitivity test (max) | 20  | 36  | 30  |

- Tests could also be performed with rainout sub-models (if available)
- Compare predicted size of deposited ammonia pool to observed wetted area, if possible

4.) Pasquill Stability Classes in DT4, FLADIS16 and FLADIS24

- For models that use Pasquill stability class instead of Monin-Obukhov length to specify the model atmospheric boundary layer, the following tests could be undertaken:

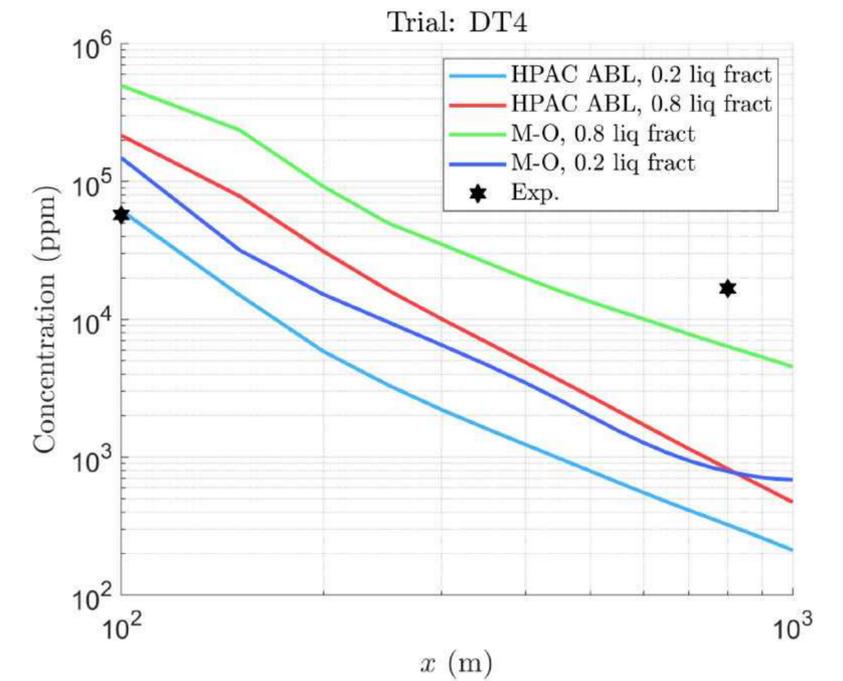
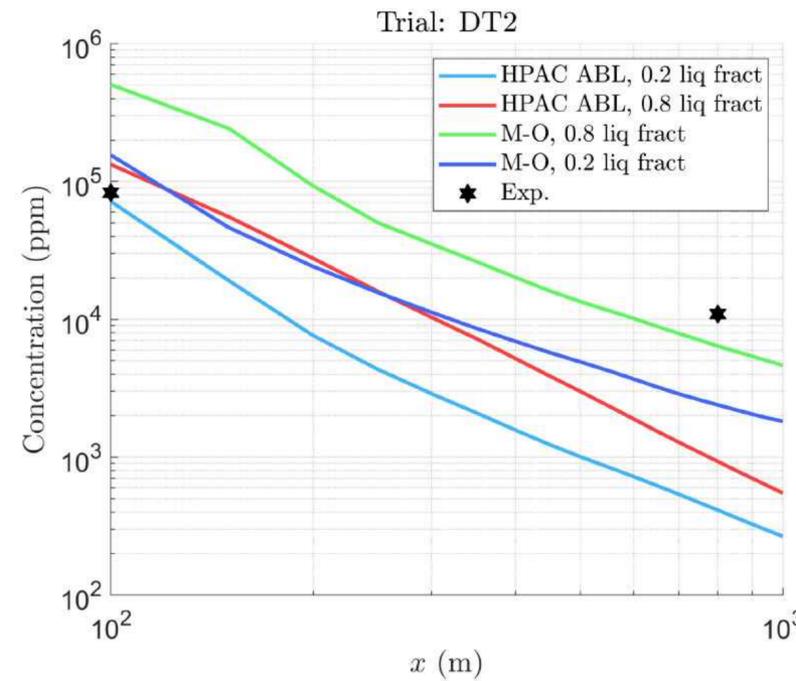
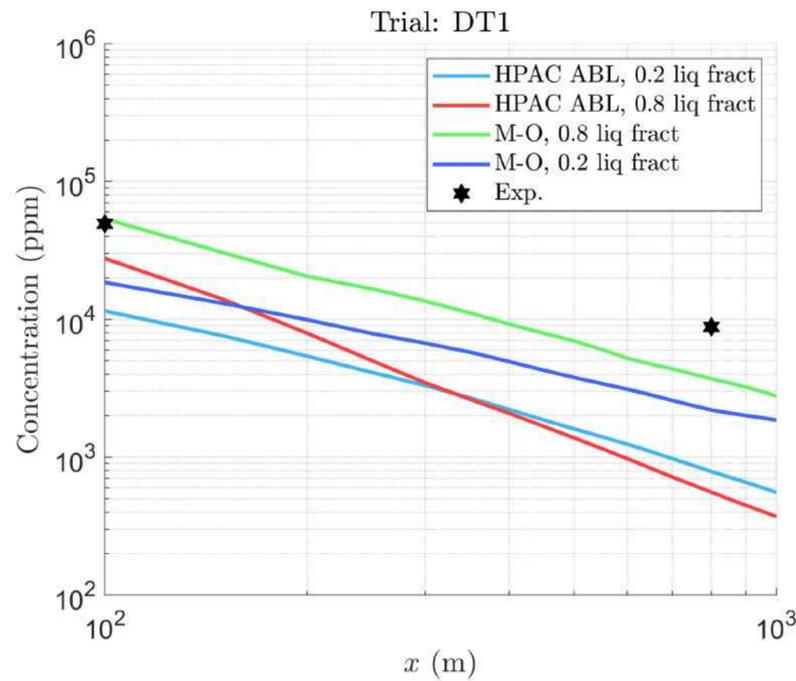
|                          |                  | DT4 | FLADIS16 | FLADIS24 |
|--------------------------|------------------|-----|----------|----------|
| Pasquill stability class | Baseline         | D   | D        | C        |
|                          | Sensitivity test | E   | E        | D        |

5.) Wind and turbulence profiles in the FLADIS trials

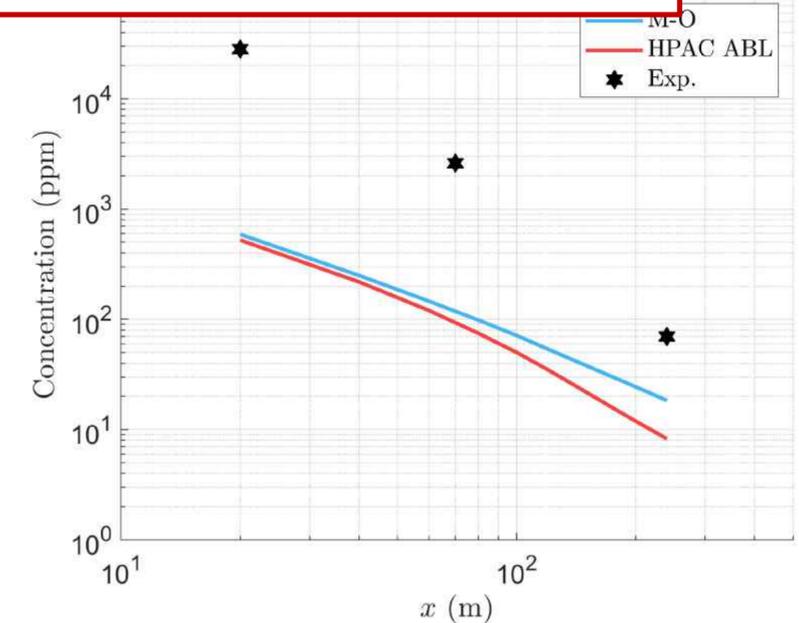
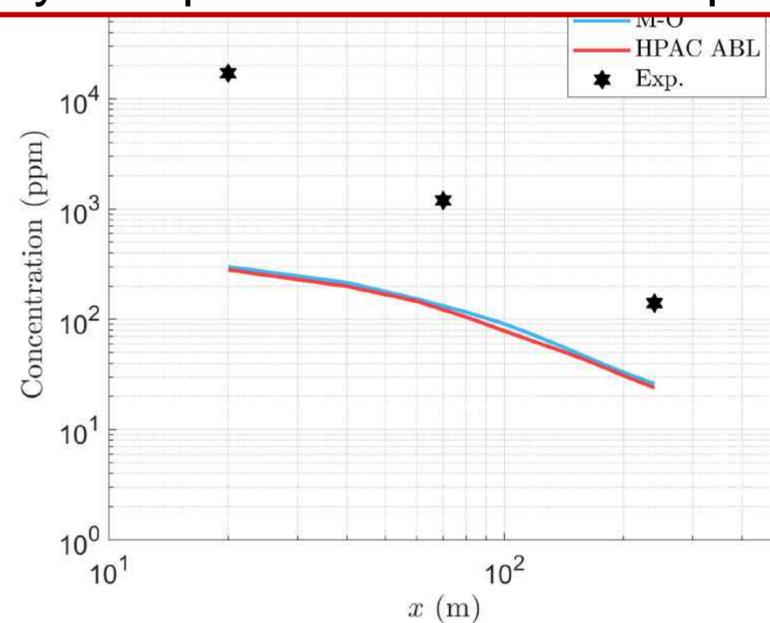
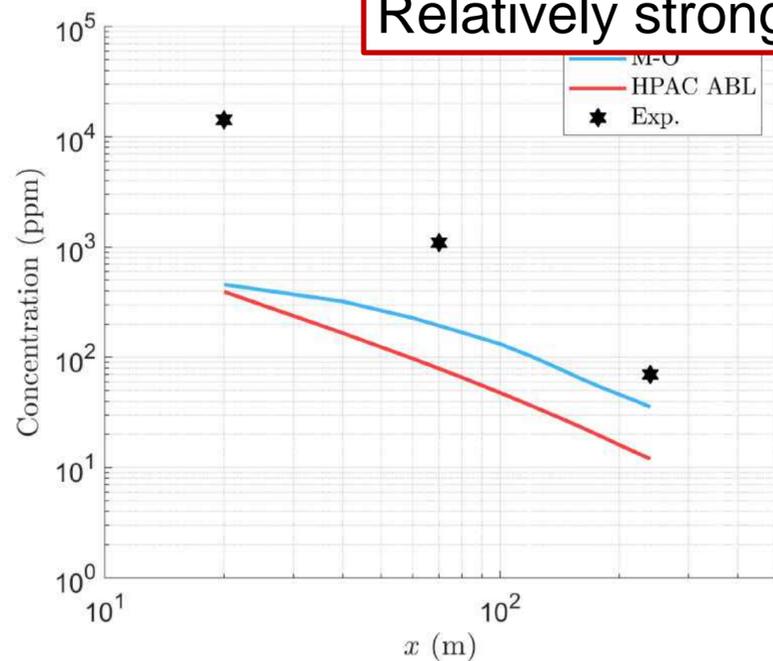
- Use wind profiles specified in the SMEDIS database and turbulence conditions specified in Table 8 or those extracted directly from the FLADIS dataset measurements (if possible).

Some modelers have examined additional factors, e.g., specification of equivalent vapor-only source conditions

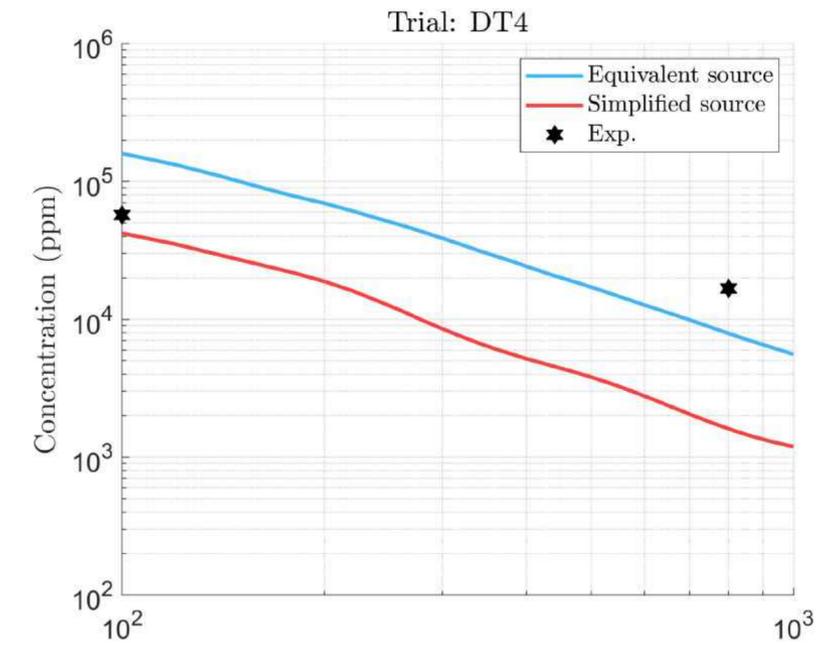
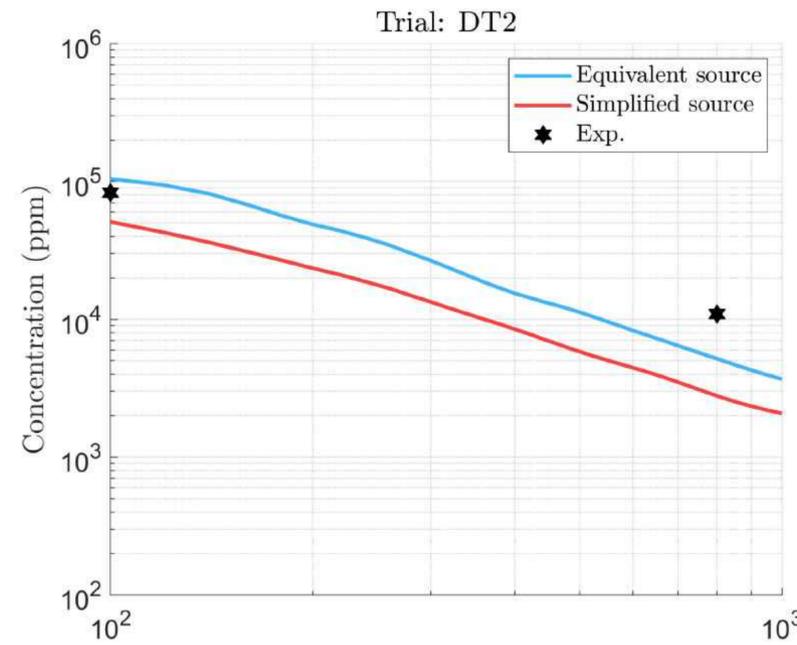
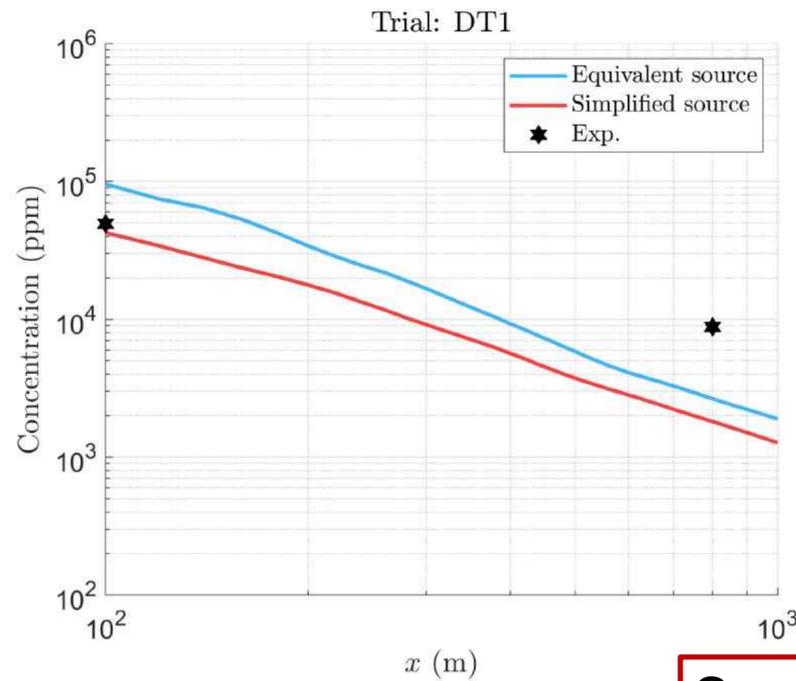
# Sensitivity Tests: DTRA Albuquerque (Sean Miner)



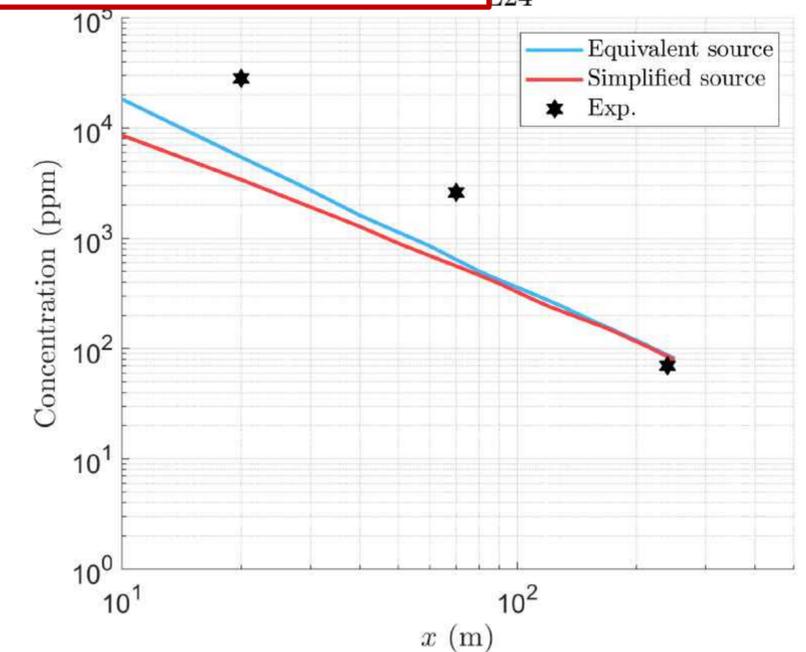
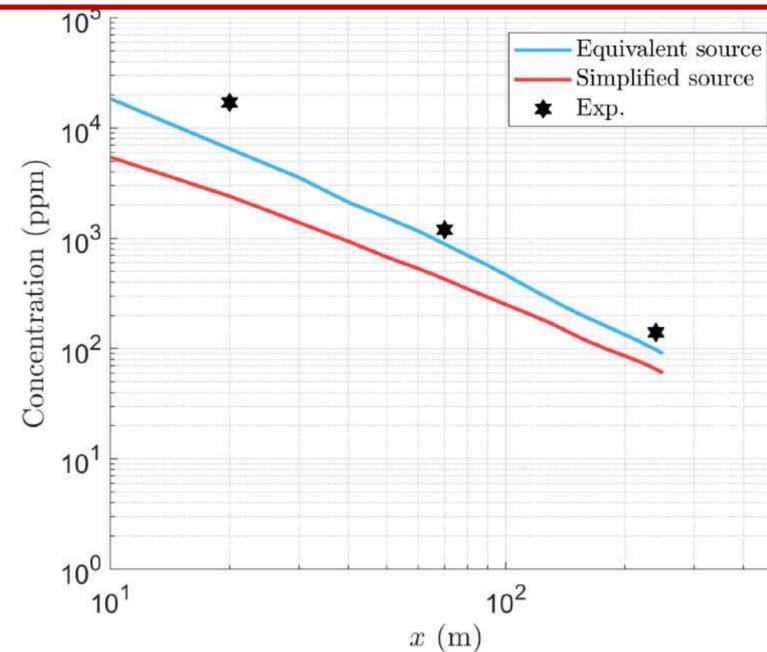
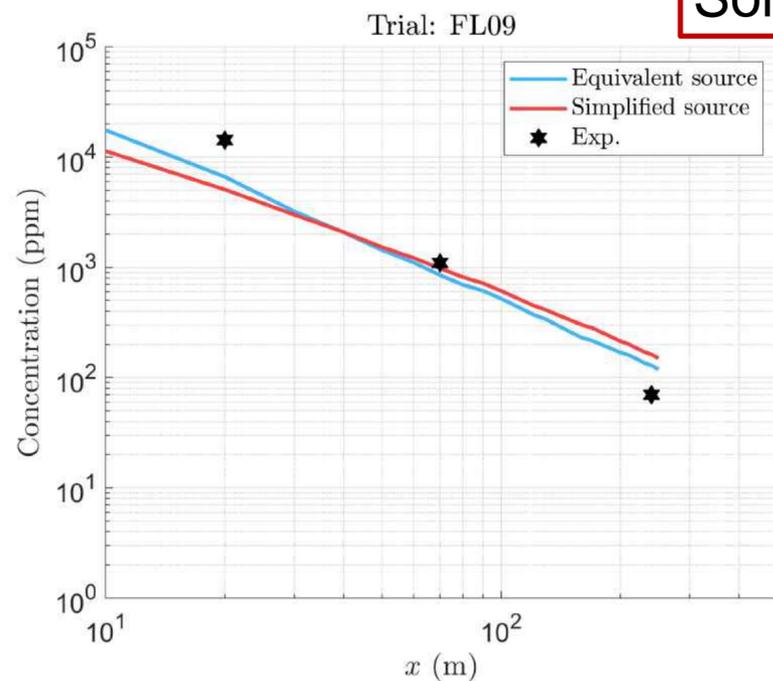
Relatively strong sensitivity to liquid fraction and ABL parameters in Desert Tortoise with HPAC



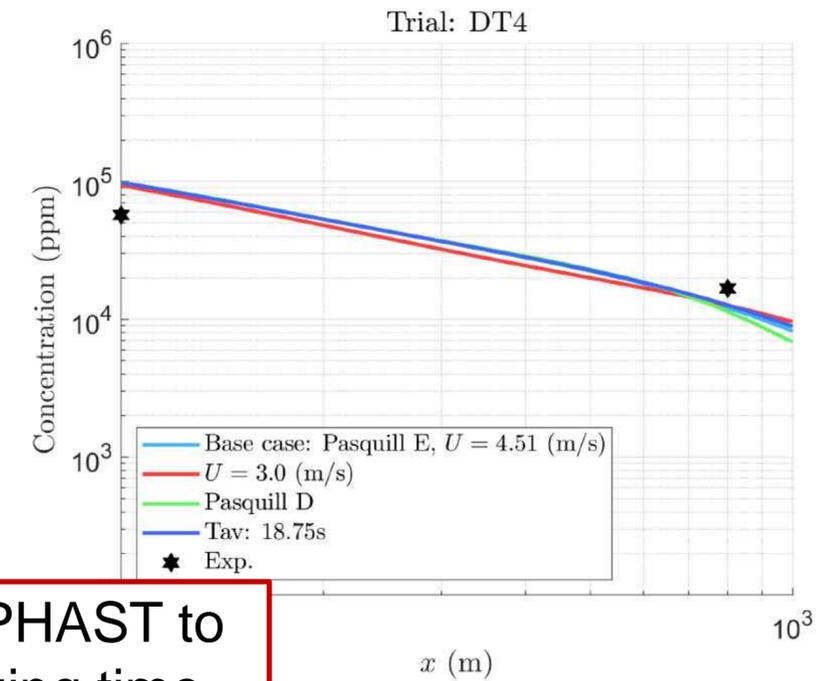
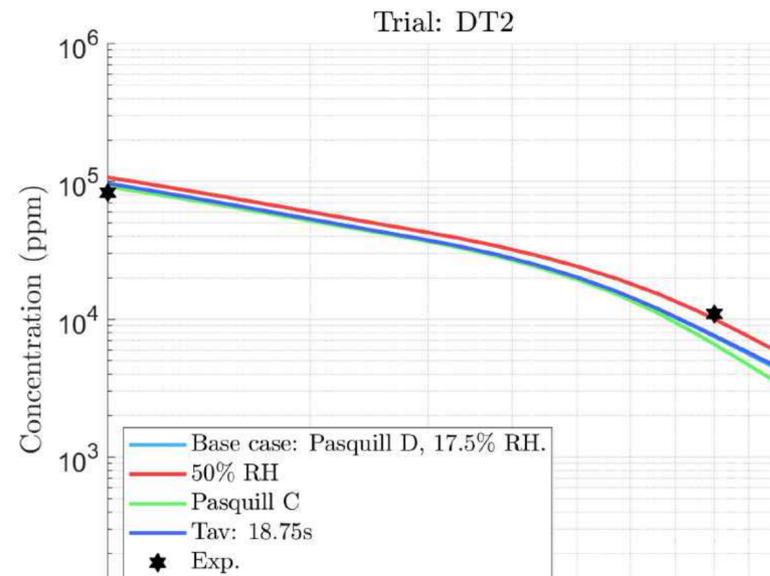
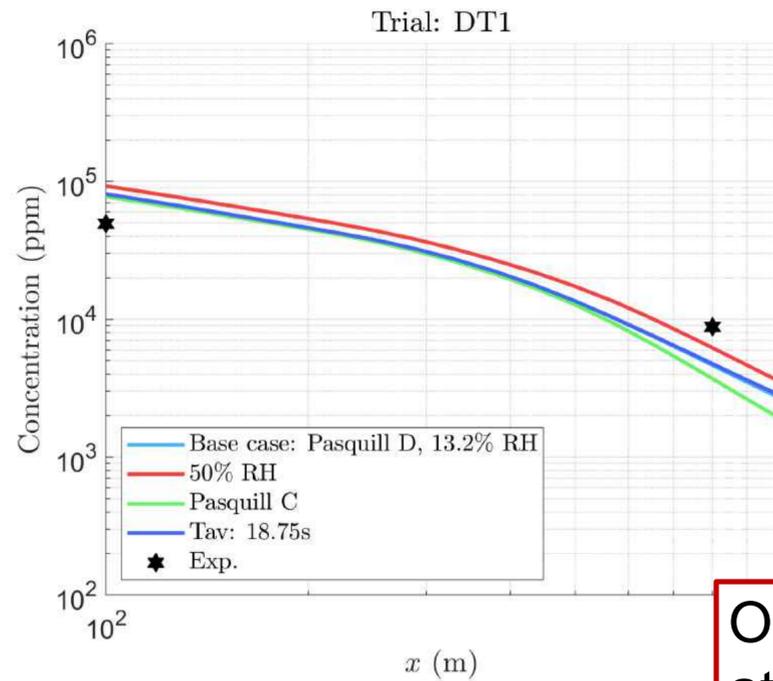
# Sensitivity Tests: Dstl (Joel Howard)



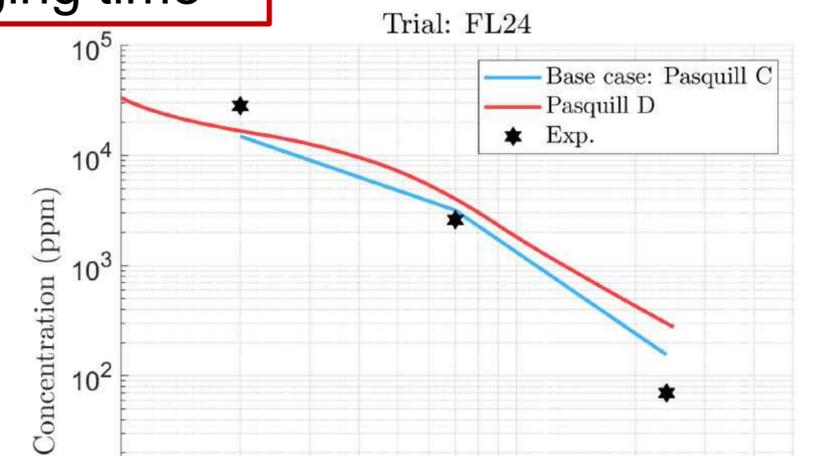
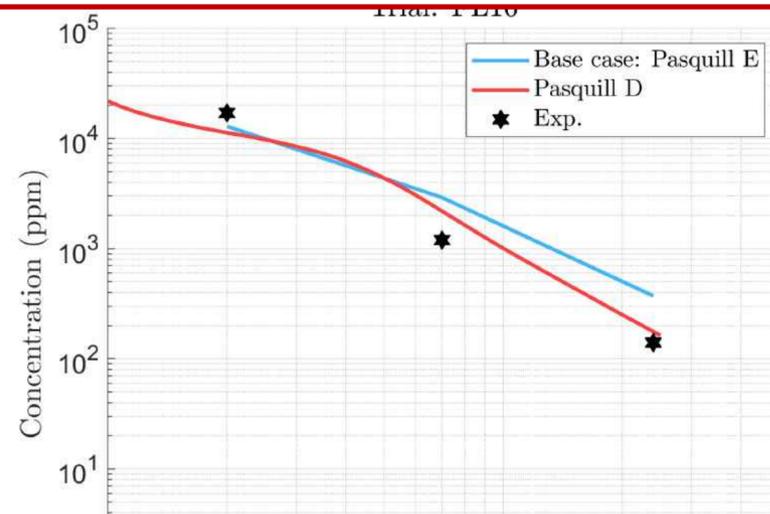
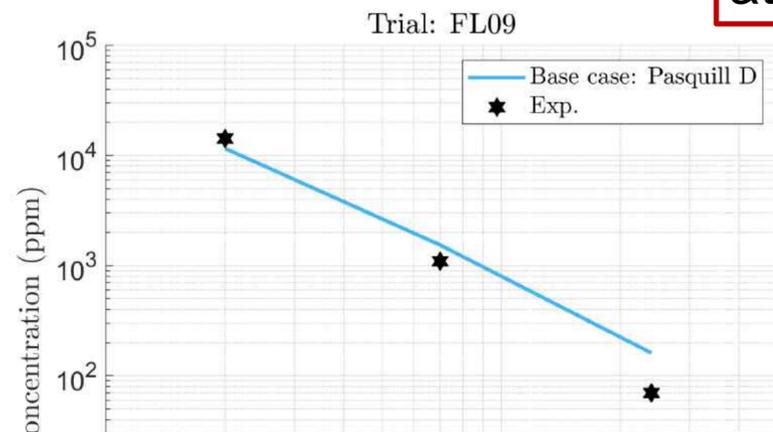
Some sensitivity to equivalent vapor-only source specification with HPAC



# Sensitivity Tests: PHAST (Frank Hart)



Only minor differences shown in sensitivity tests with PHAST to atmospheric stability, humidity, wind speed and averaging time



1.) Standing water at the Frenchman Flats test site in Desert Tortoise trials DT1 and DT2

|                          |                  | DT1  | DT2  |
|--------------------------|------------------|------|------|
| Relative humidity (%)    | Baseline         | 13.2 | 17.5 |
|                          | Sensitivity test | 50   | 50   |
| Monin-Obukhov length (m) | Baseline         | 92.7 | 94.7 |
|                          | Sensitivity test | -20  | -20  |
| Pasquill stability class | Baseline         | D    | D    |
|                          | Sensitivity test | C    | C    |

2.) Wind speed variability in DT4

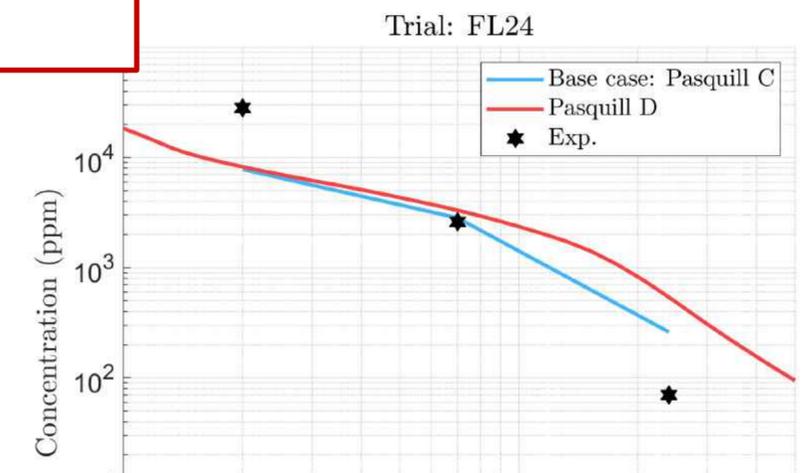
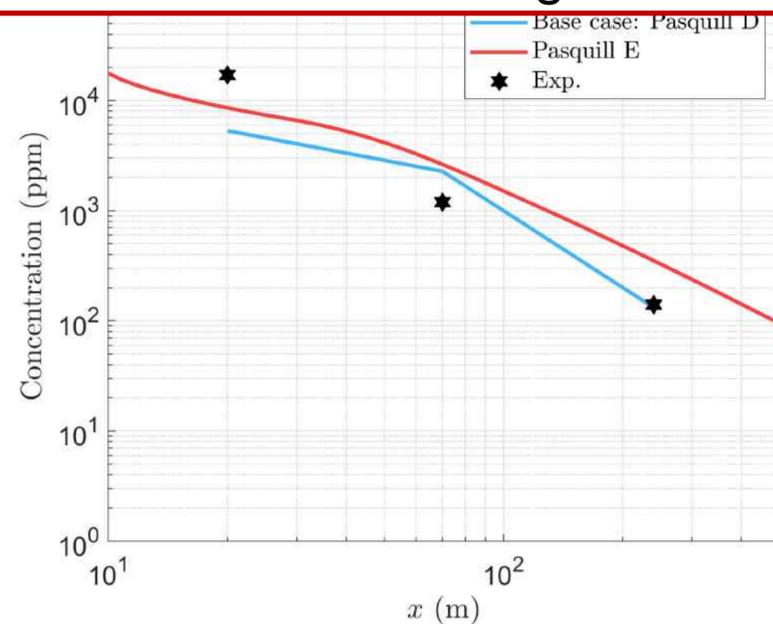
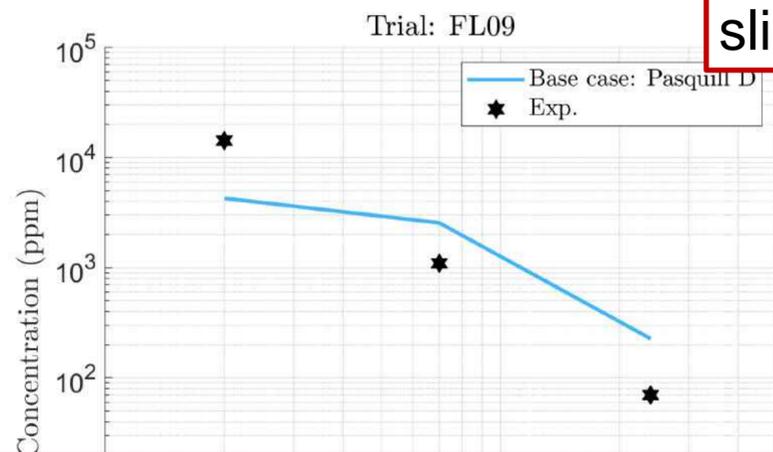
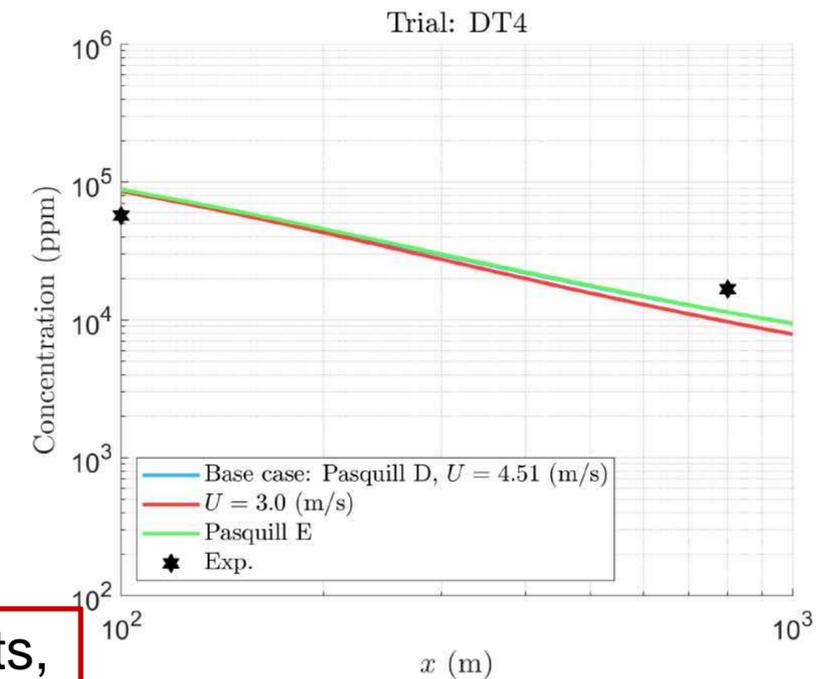
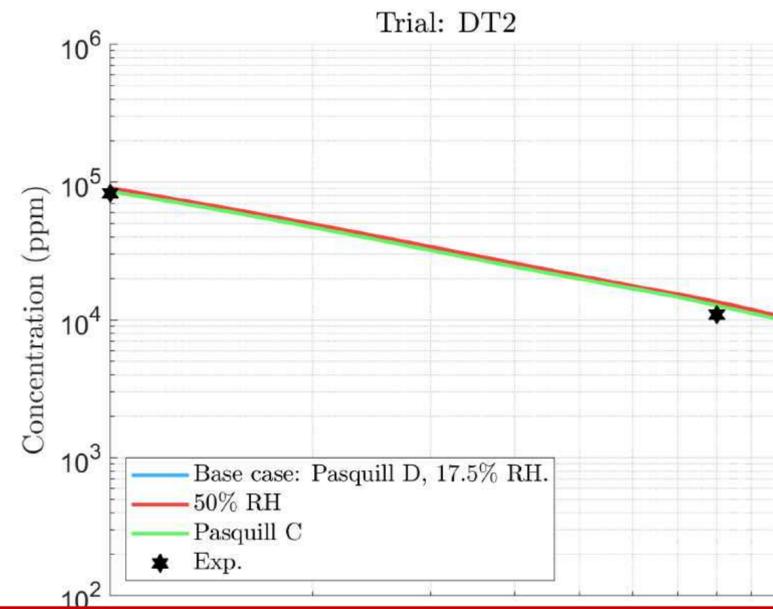
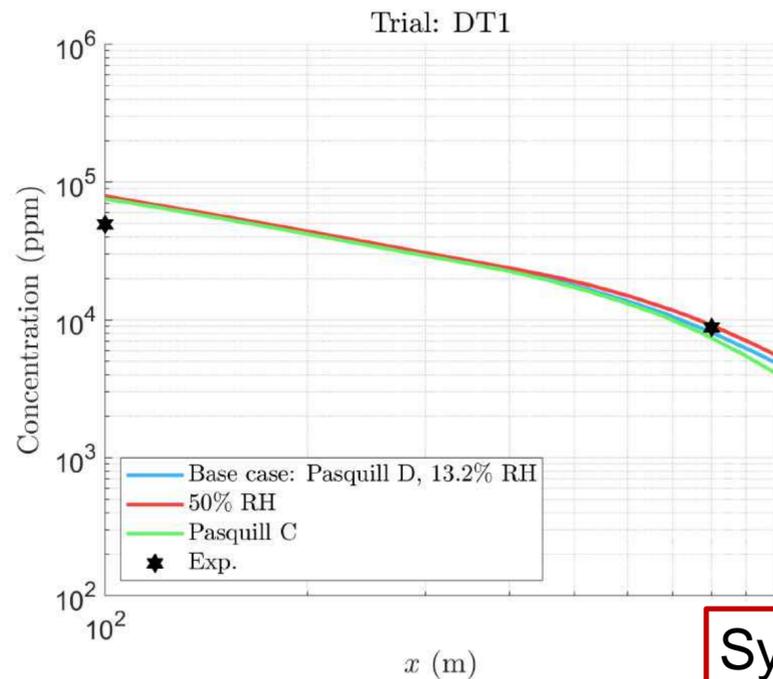
|                               |                  | DT4  |
|-------------------------------|------------------|------|
| Site average wind speed (m/s) | Baseline         | 4.51 |
|                               | Sensitivity test | 3.0  |

4.) Pasquill Stability Classes in DT4, FLADIS16 and FLADIS24

- For models that use Pasquill stability class instead of Monin-Obukhov length to specify the model atmospheric boundary layer, the following tests could be undertaken:

|                          |                  | DT4 | FLADIS16 | FLADIS24 |
|--------------------------|------------------|-----|----------|----------|
| Pasquill stability class | Baseline         | D   | D        | C        |
|                          | Sensitivity test | E   | E        | D        |

# Sensitivity Tests: PHAST-SYN (Adeel Ibrahim)



Syngenta results using Phast are similar to DNV results, slightly reduced effect from changes to humidity

1.) Standing water at the Frenchman Flats test site in Desert Tortoise trials DT1 and DT2

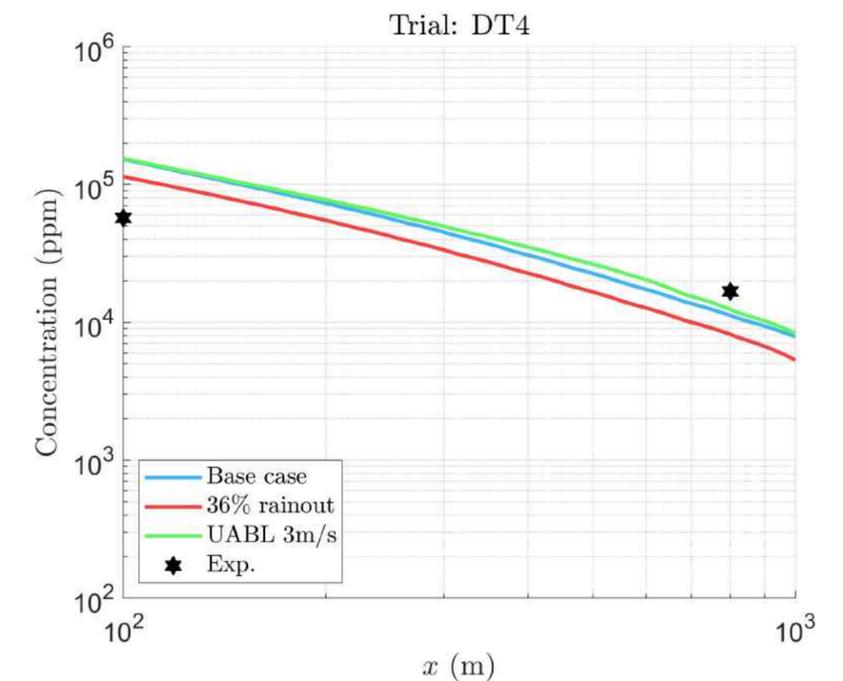
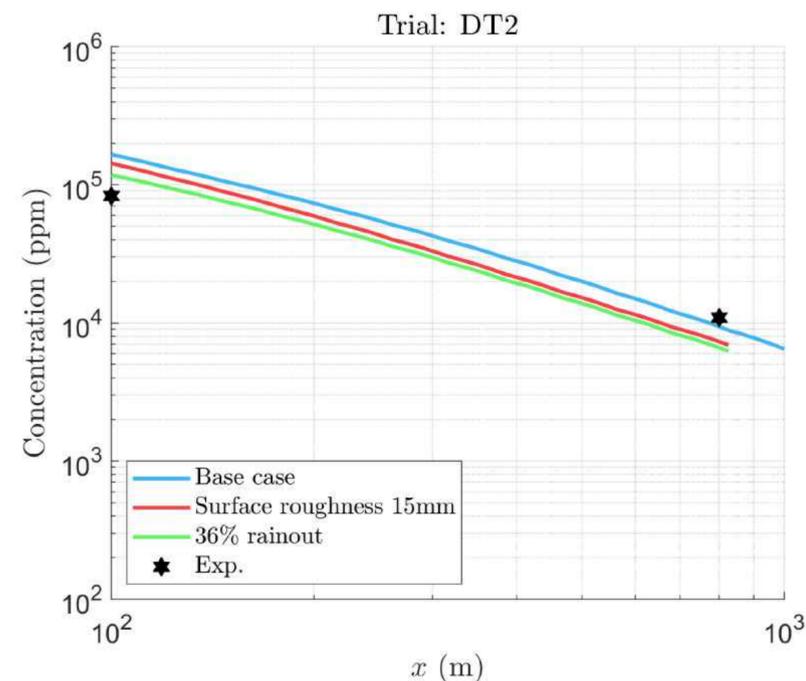
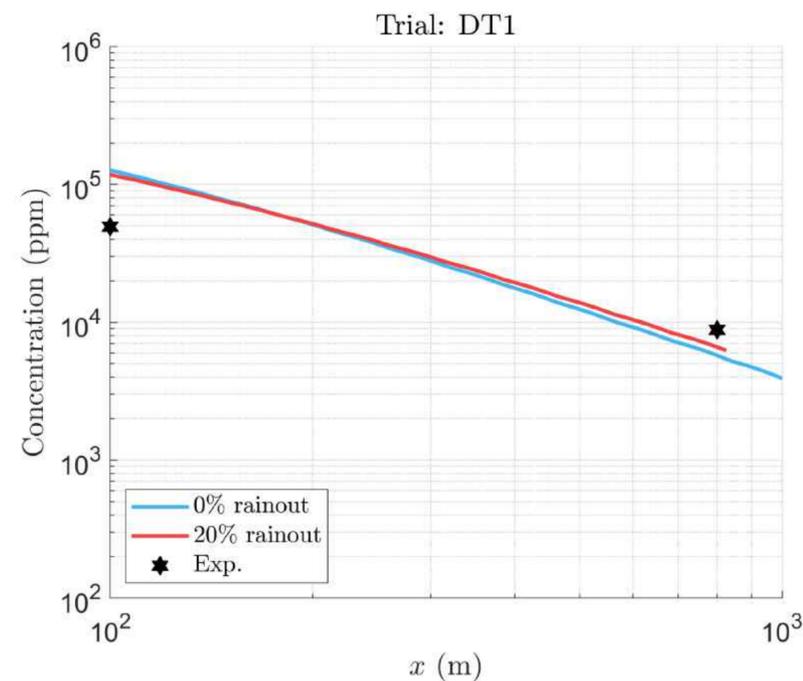
|                          |                  | DT1  | DT2  |
|--------------------------|------------------|------|------|
| Relative humidity (%)    | Baseline         | 13.2 | 17.5 |
|                          | Sensitivity test | 50   | 50   |
| Monin-Obukhov length (m) | Baseline         | 92.7 | 94.7 |
|                          | Sensitivity test | -20  | -20  |
| Pasquill stability class | Baseline         | D    | D    |
|                          | Sensitivity test | C    | C    |

4.) Pasquill Stability Classes in DT4, FLADIS16 and FLADIS24

- For models that use Pasquill stability class instead of Monin-Obukhov length to specify the model atmospheric boundary layer, the following tests could be undertaken:

|                          |                  | DT4 | FLADIS16 | FLADIS24 |
|--------------------------|------------------|-----|----------|----------|
| Pasquill stability class | Baseline         | D   | D        | C        |
|                          | Sensitivity test | E   | E        | D        |

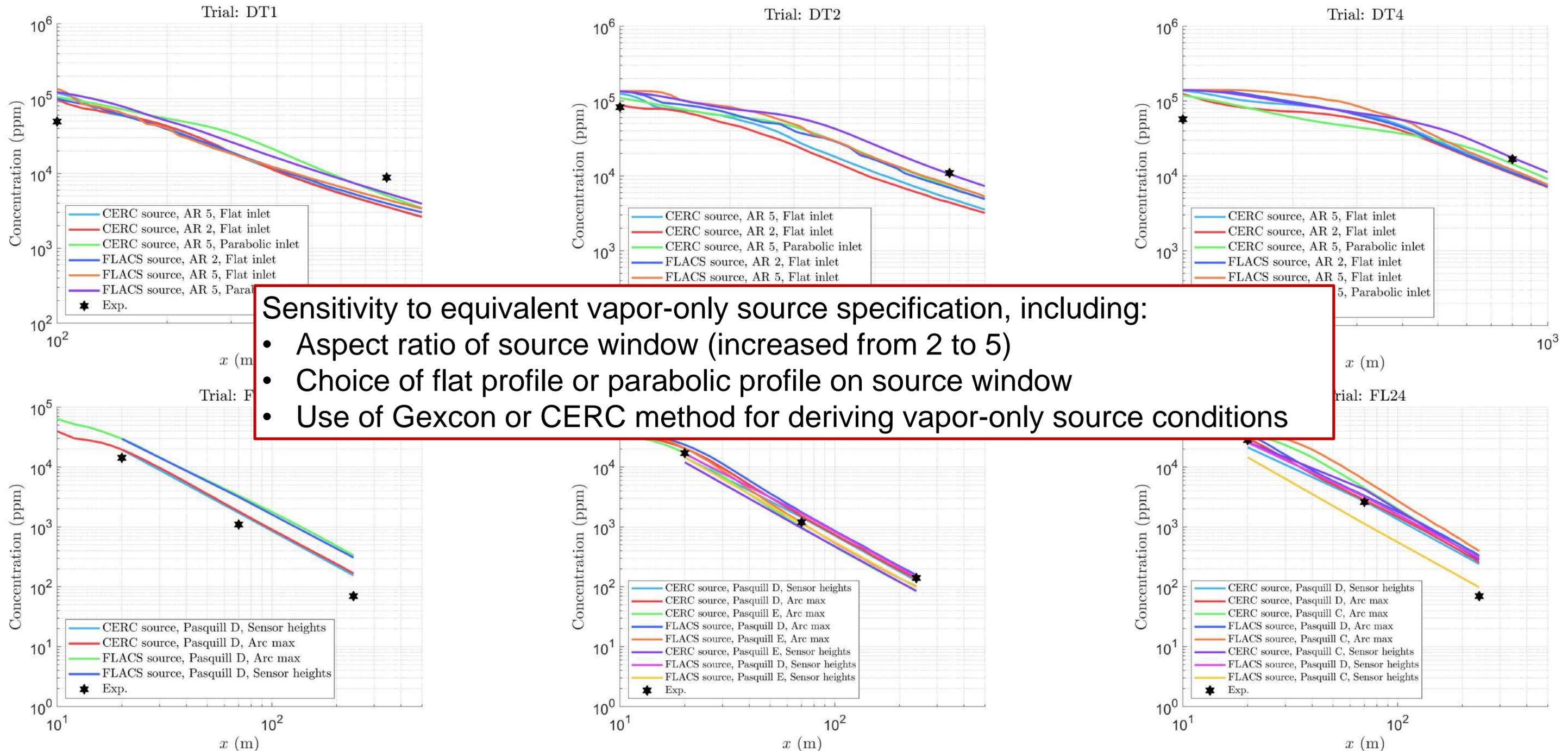
# Sensitivity Tests: EFFECTS-GEXC (Andreas Mack)



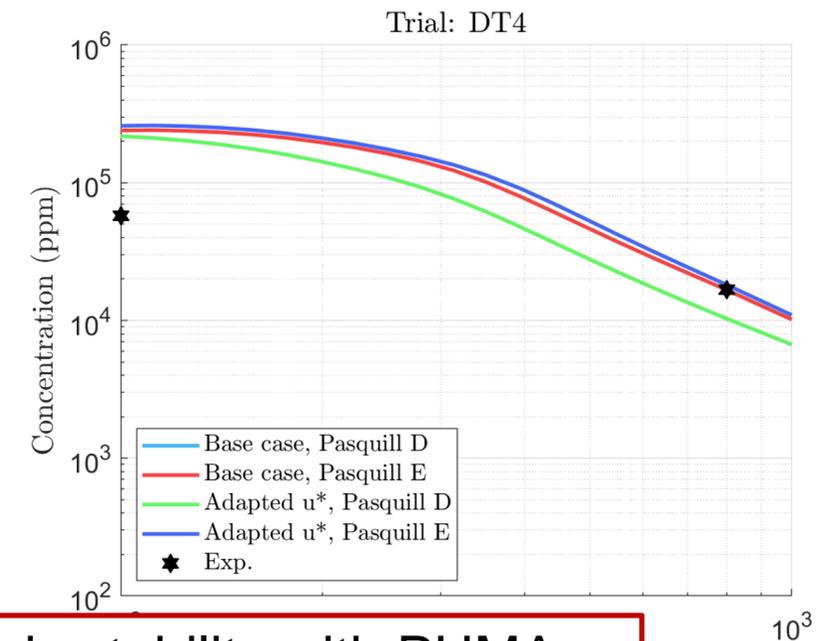
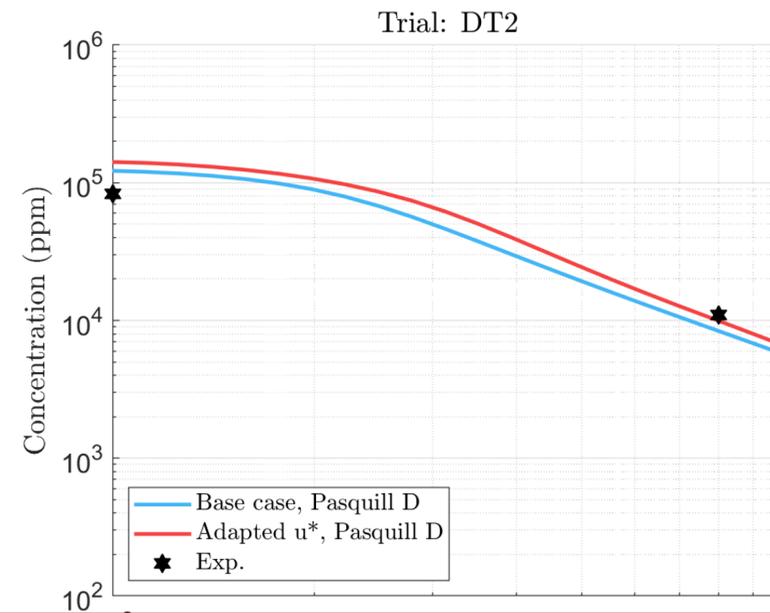
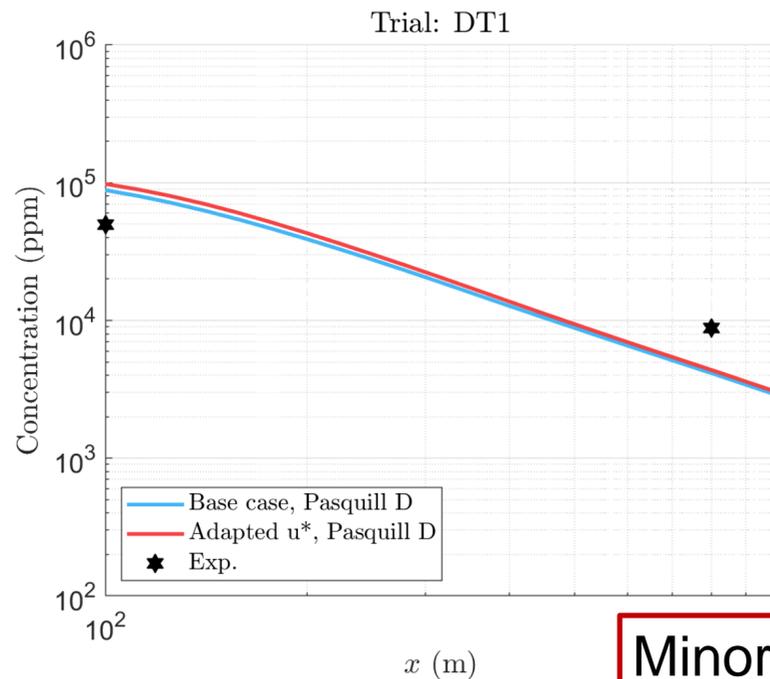
Minor sensitivity to:

- Increased liquid rainout from 0% to 20% or 36%
- Surface roughness increased from 3 mm (base case) to 15 mm
- Wind speed reduced from 4.5 m/s to 3.0 m/s in DT4

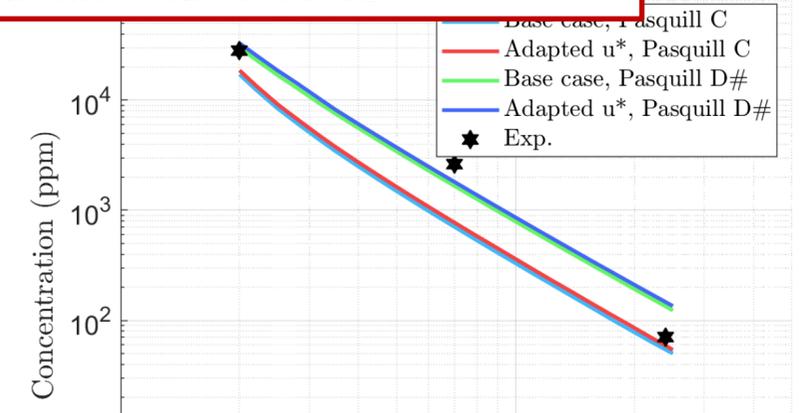
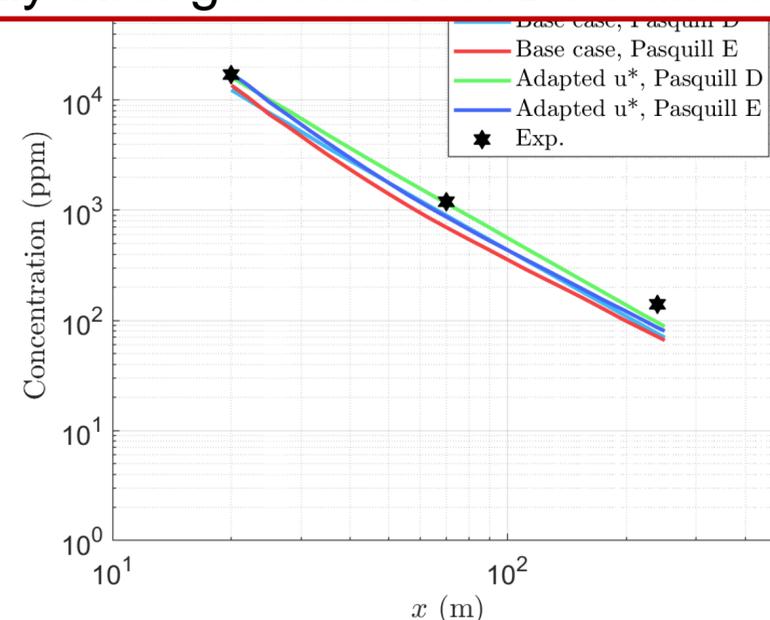
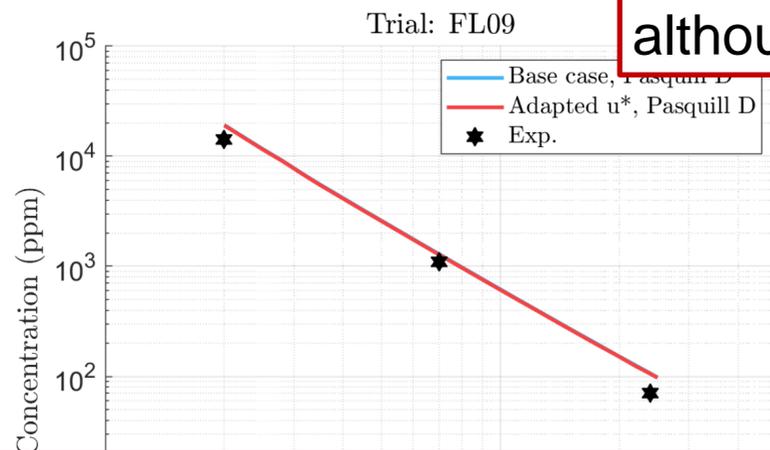
# Sensitivity Tests: FLACS-GEXC (Lorenzo Mauri)



# Sensitivity Tests: PUMA-FOI (Oscar Björnham)



Minor differences shown in sensitivity tests to atmospheric stability with PUMA, although slightly stronger effect for DT4 and FLADIS24 than with PHAST



1.) Standing water at the Frenchman Flats test site in Desert Tortoise trials DT1 and DT2

|                          |                  | DT1  | DT2  |
|--------------------------|------------------|------|------|
| Relative humidity (%)    | Baseline         | 13.2 | 17.5 |
|                          | Sensitivity test | 50   | 50   |
| Monin-Obukhov length (m) | Baseline         | 92.7 | 94.7 |
|                          | Sensitivity test | -20  | -20  |
| Pasquill stability class | Baseline         | D    | D    |
|                          | Sensitivity test | C    | C    |

4.) Pasquill Stability Classes in DT4, FLADIS16 and FLADIS24

- For models that use Pasquill stability class instead of Monin-Obukhov length to specify the model atmospheric boundary layer, the following tests could be undertaken:

|                          |                  | DT4 | FLADIS16 | FLADIS24 |
|--------------------------|------------------|-----|----------|----------|
| Pasquill stability class | Baseline         | D   | D        | C        |
|                          | Sensitivity test | E   | E        | D        |